AD-A033 605 ITT GILFILLAN INC VAN NUYS CALIF F/G 17/9
MM AND TE-APPLICATION OF RADAR TO BALLISTIC ACCEPTANCE TESTING --ETC(U)
SEP 76 C BARFIELD DAAA21-73-C-0664
UNCLASSIFIED ITTG-50598 NL

1 OF 2
AD
A033605

FC

AD ________________

REPORT NO. 5059B

MM&TE – APPLICATION OF RADAR TO BALLISTIC ACCEPTANCE TESTING OF AMMUNITION (ARBAT) PHASE B: ANTENNA DEVELOPMENT/FABRICATION

See 1473 in back

FINAL REPORT (PHASE B)

CDRL: A002

30 September 1976

SARPA-QA-A-R

PICATINNY ARSENAL
DOVER, NEW JERSEY 07801

DRCMS CODE: 4932.05.4139.1

CONTRACT NO. DAAA21-73-C-0664

ITT GILFILLAN
7821 Orion Avenue
Van Nuys, California 90406

AD ______________

REPORT NO. 5059B

MM&TE - APPLICATION OF RADAR TO BALLISTIC ACCEPTANCE TESTING OF AMMUNITION (ARBAT) PHASE B: ANTENNA DEVELOPMENT/FABRICATION

FINAL REPORT (PHASE B)

CDRL: A002

30 September 1976

SARPA-QA-A-R

PICATINNY ARSENAL
DOVER, NEW JERSEY 07801

DRCMS CODE: 4932.05.4139.1

CONTRACT NO. DAAA21-73-C-0664

Distribution of the document is unlimited.
The findings in this report are not to be construed as an official Department of Army position.
Destroy this report when no longer needed. Do not return it to the originator.

ITT GILFILLAN
7821 Orion Avenue
Van Nuys, California 90406

ABSTRACT

The ARBAT (Application of Radar to Ballistic Acceptance Testing of Ammunition) radar system is presently being developed by Picatinny Arsenal for range instrumentation purposes. This report covers the development of the antenna subsystem through range testing of a 9-element test array and assembly of the full antenna. The subject antenna is a 10 x 12 ft phase/frequency/mechanical scanning X-band planar array. Elevation scanning is by means of phase variation obtained by program controlled 4-bit diode phase shifters. In addition to the electronic scanning capability, a manual tilt capability is included to accommodate range terrain variations. Azimuth scanning is accomplished by frequency variation, and limited mechanical rotation of the array by servo control. Mechanical rotation is limited to ±170 degrees which fulfills the requirements of the application. The transmitter/receiver unit is mounted on the antenna back structure. Connections to and from the transmitter/receiver and phase shifter control electronics are made through a "windup" cable arrangement eliminating the need for slip rings. The array is made up of 167 horizontal dual-slot pair radiators fed by a vertical feed line.

The antenna incorporates a performance monitoring feature which functions as a confidence indicator and as a means for fault location down to the single horizontal array level. This feature is implemented by means of coupling each horizontal array, opposite the feed end, to a vertical combiner, or performance monitor line. Residual RF energy in the radiating sections is combined and detected to monitor array performance. Simple diagnostic phase shifter exercising programs facilitate fault location.

FOREWORD

ARBAT PHASE B (FABRICATION AND TESTING OF A PHASED ARRAY FREQUENCY SCAN RADAR ANTENNA)

The subject report covers the second phase (antenna fabrication and testing) of a multiple phase program to develop and deliver an X-band phase/frequency/mechanical scanning radar for ballistic ammunition testing applications.

Related data contained in this report concerns the intermediate steps of test element and test array fabrication, and testing of those components individually, then as a nine element test array on the test range.

In addition to the detailed specific requirements placed on the antenna design/implementation, there is an obvious requirement for complete compatibility with the other radar group elements to insure achievement of the overall radar system performance specifications when the subject antenna is assembled into the system.

Where useful in describing the development of the antenna, non-scale sketches have been used in some instances to clarify the text only. Photographs of the assembled antenna are included.

The report presents data collected during the course of the Phase B design and fabrication, and data pertinent to the testing program through the nine element test array range pattern measurement activities.

TABLE OF CONTENTS

LIST OF ILLUSTRATIONS

LIST OF ILLUSTRATIONS (Continued)

ARBAT ANTENNA

1. DEVELOPMENT APPROACH

The ARBAT system required the development of an antenna to meet the unique performance requirements of ballistic ammunition testing. The approach followed for this development was standard in antenna design; a paper design was first generated by means of computer analyses. Input data for these analyses were based on proven design parameters generated for similar antennas produced for other programs. An iterative process, in which a single element followed by multiple horizontal array elements were fabricated, tested and modified as necessary to optimize configuration, was followed. A detailed illustration of the development/fabrication sequence followed with the ARBAT antenna is shown in Figure 1.

1.1 Overall Characteristics

1.1.1 General Description. - The antenna is a planar array design with an aperture of 10 ft x 12 ft. Beam scanning is accomplished by a combination of electronic and mechanical means. The beam is scanned in elevation by four-bit diode phase shifters (GFE), whereas azimuth scanning is by frequency variation and mechanical rotation of the array. The mechanical rotation capability is limited to a maximum of ±170 degrees which fulfills the requirements in ammunition testing applications. Provisions are included in the antenna back structure design for a mechnical adjustment (tilt) of 0 to 25 degrees in elevation. The back structure is designed to support the microwave assembly, phase shifter power supplies and logic, and the transmitter/receiver unit. In view of the less than 360 degree rotation required (±170°), a cable "windup" scheme is used for power and all input/output lines to and from the antenna which obviates the need for slip rings. The artists sketch in Figure 2 illustrates the overall system configuration concept. A more detailed view illustrating the back structure concept is shown in Figure 3. The array contains 167 dual slot horizontal radiators which are fed by a single vertical feed line via 90-degree waveguide twist and offset sections followed by 4-bit diode phase shifters. The arrays terminate at a vertical performance monitor line at the end opposite the feed line. The performance monitor line is a part of the performance monitor and fault location feature incorporated in the system design. Antenna performance determination is accomplished by the measurement of residual RF energy at the extreme ends of the horizontal arrays (opposite the feed ends). Coupling from the vertical feed line to the arrays and from the arrays to the performance monitor line is by 4-port coupler

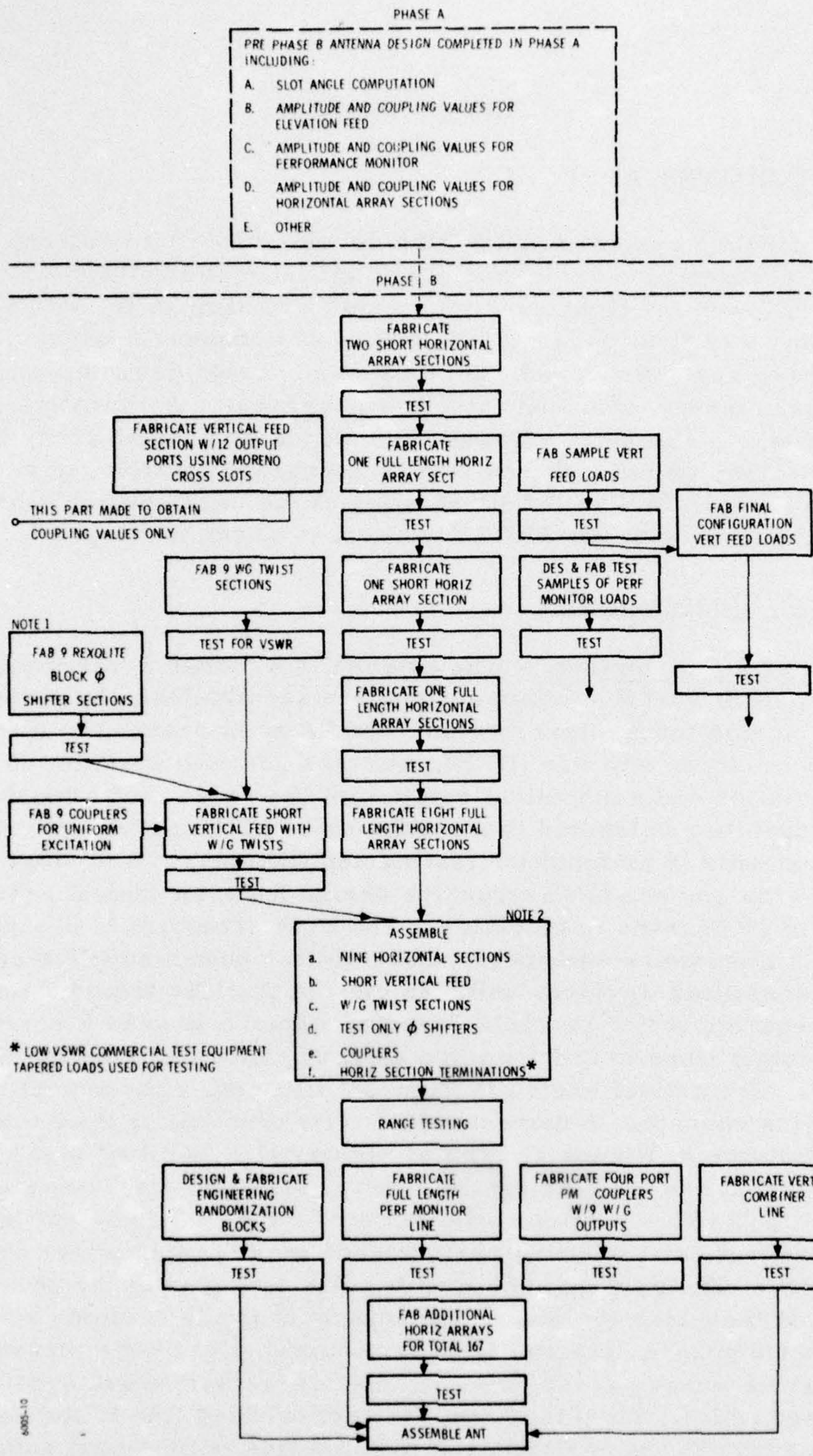


Figure 1. ARBAT Phase Antenna Development Sequence

NOTES TO FIGURE 1

NOTE 1:

Fabrication of "dummy" phase shifter waveguide sections with Rexolite phase shifting block inserts for substitution in place of the diode phase shifters which were not available at the time the tests were required. The Rexolite blocks provide a step transformer with a maximum VSWR of 1.1:5. The phase shift increments of the Rexolite block/waveguide section units were adjusted to ± 3 degrees by the application of dielectric tape directly to the side of the block; phase shift was then measured at center frequency.

NOTE 2:

A nine element test array was assembled using the array elements, short feed, waveguide twist sections, dummy phase shifter blocks and couplers prepared earlier. These elements were assembled into a test support to simulate the final full array configuration except with a reduced number of array elements. This test assembly was then moved to the test range for the tests described later in this report.

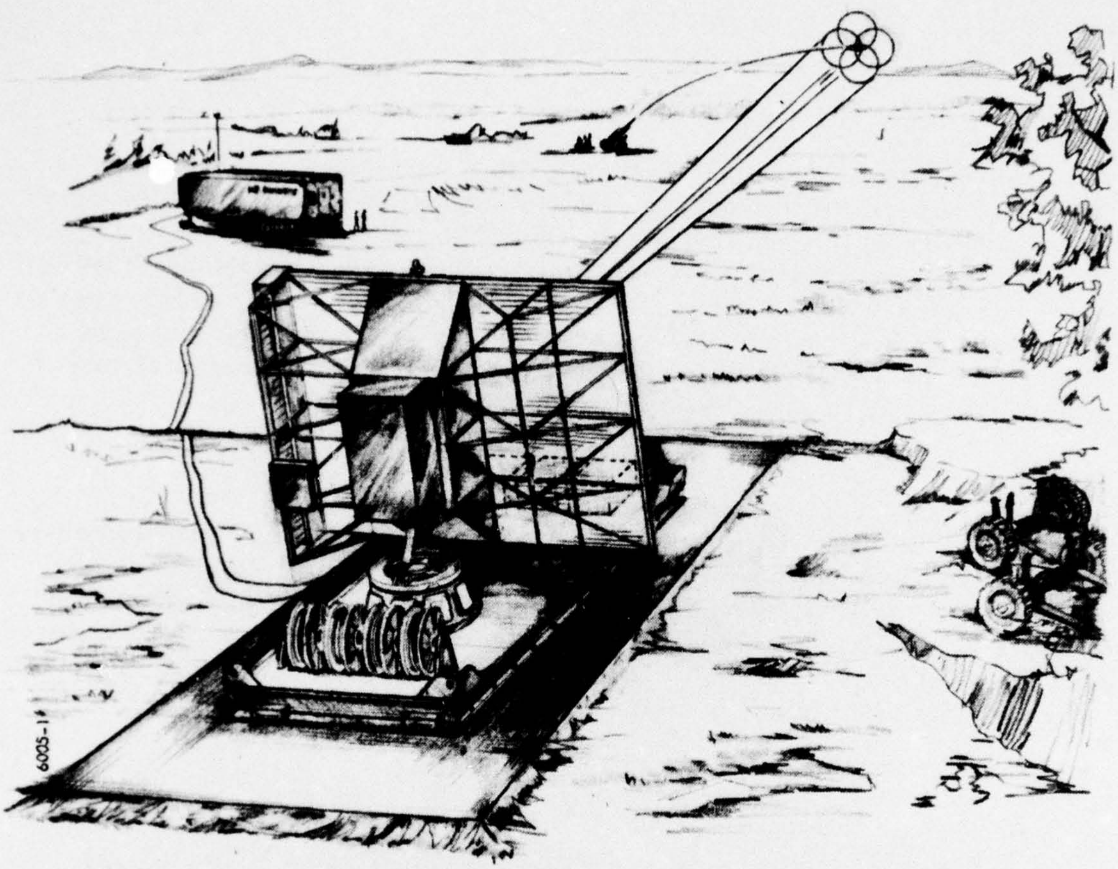


Figure 2. System Configuration Concept

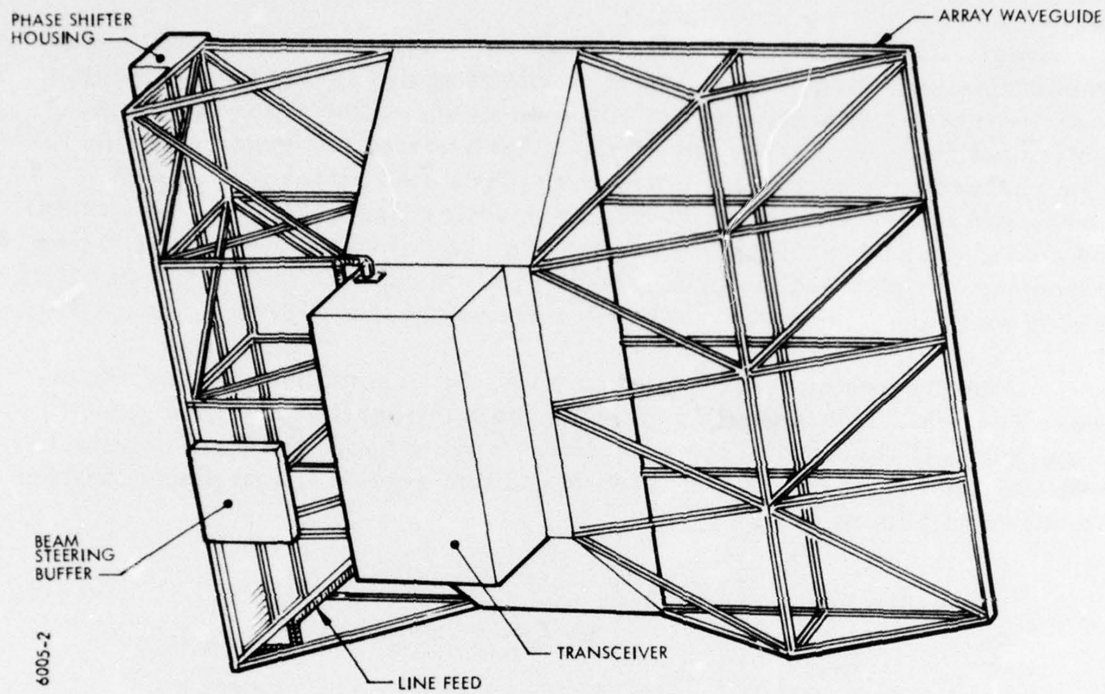


Figure 3. Back Structure/Transceiver Mounting

sections. Coupling sections at the feed end contain end loads and phase randomization blocks. The 4-port couplers at the performance monitor line section are designed with a common flange which mates with the individual flanges at the output ends of each horizontal array element. The performance monitor feature is implemented by terminating the lower end of the vertical performance monitor line section with a crystal video detector whose output is routed via coaxial cable to the monitoring circuitry. A pictorial drawing showing microwave element configuration and signal flow illustrates the basic antenna physical design, Figure 4.

The two photographs following show the assembled antenna microwave section. The front side showing the horizontal array elements, Figure 5; and the rear of the assembly showing back structure details, vertical feed line, 90 degree twist waveguide sections, and phase shifters is shown in Figure 6.

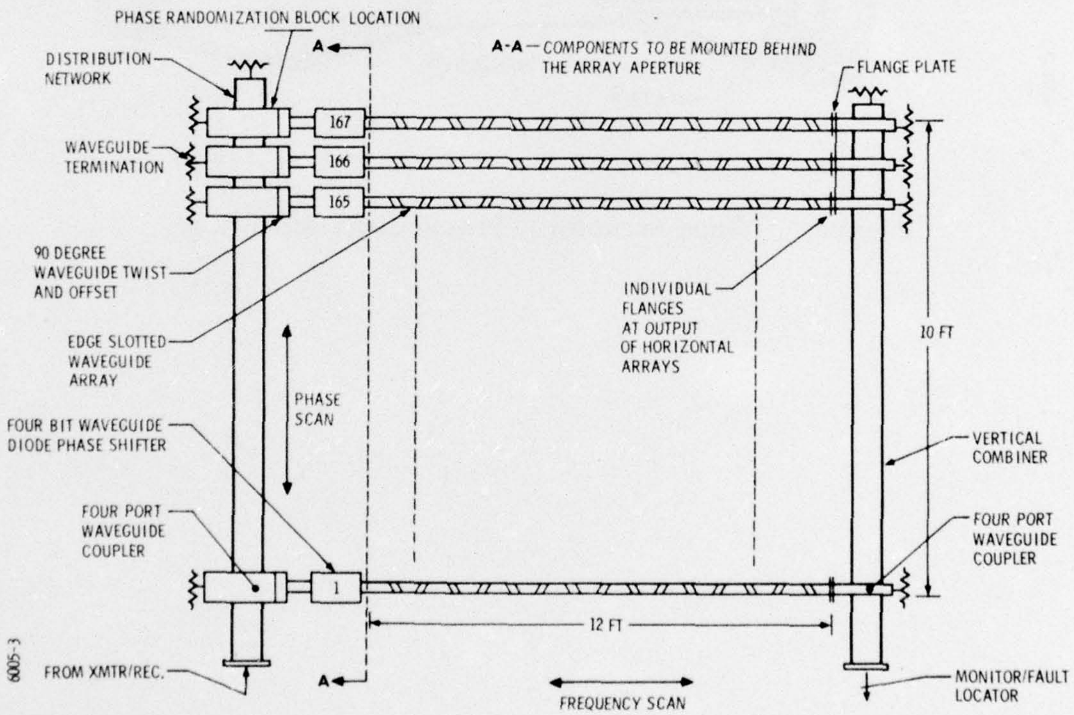
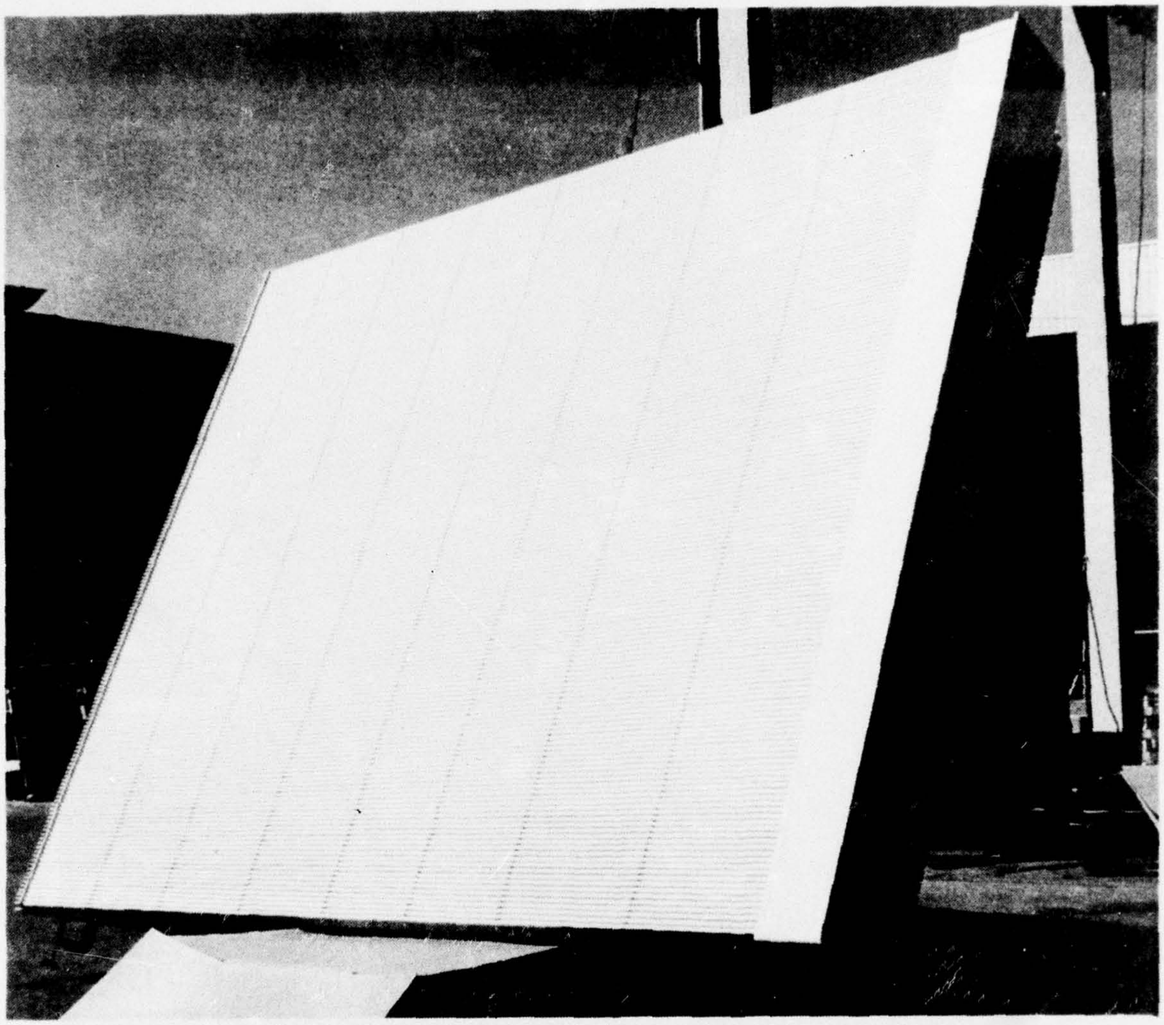
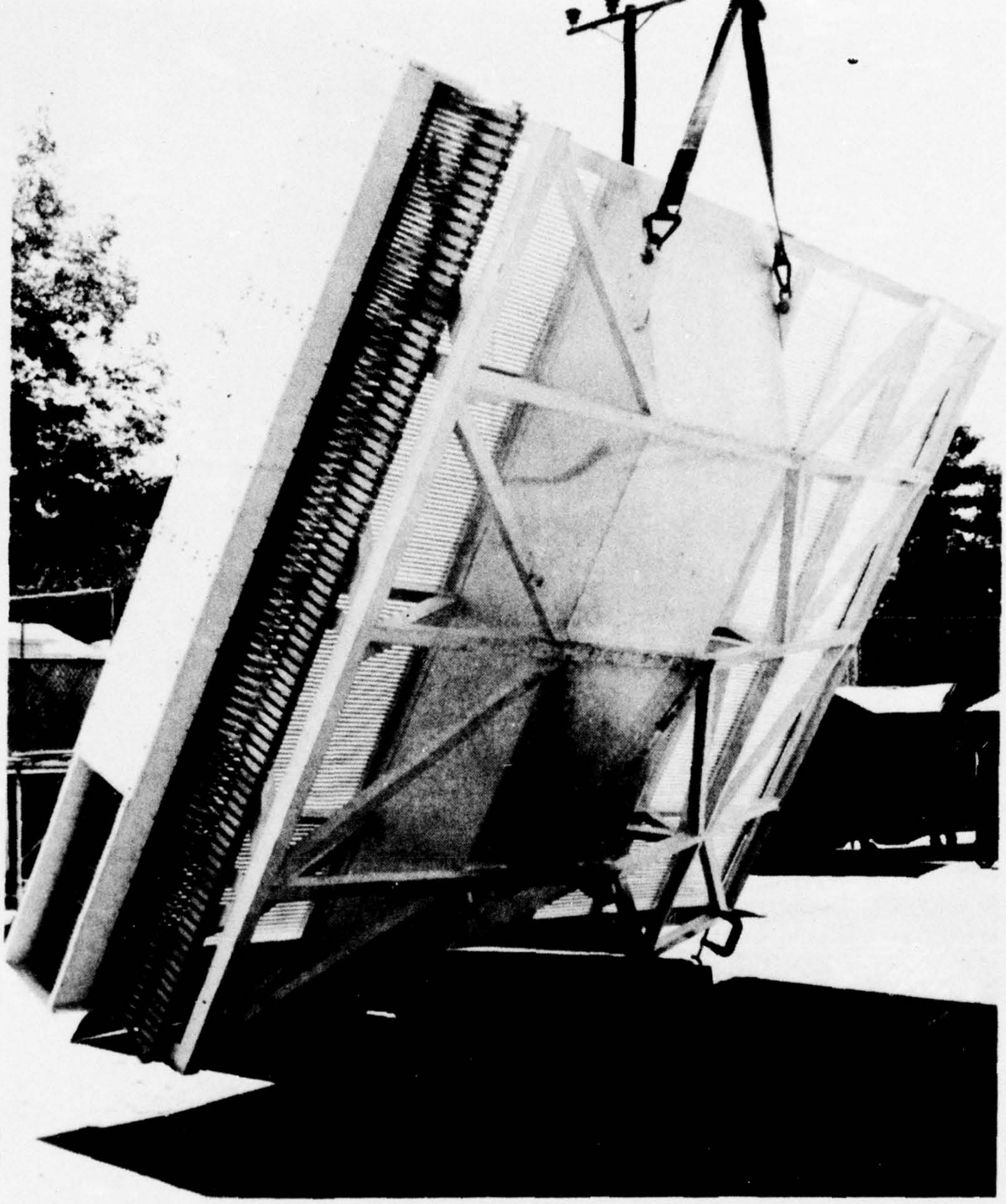


Figure 4. Antenna Signal Flow Graphic Schematic



P12929-4

Figure 5. Antenna Assembly Front Array View



P12929-1

Figure 6. Antenna Assembly Rear View

1.2 Detailed Requirements

The following extracts from Appendix A of the contract Statement of Work, include the basic performance requirements placed on the antenna to be achieved when mounted on a suitable pedestal with servo control and when coupled to the modified GFE transmitter for which the antenna has been designed. Pedestal assembly and transceiver modifications are parts of forthcoming program phases.

1.0 Beam Steering

1.1 Electrical

1.1.1 Azimuth: 7.7 degrees minimum

1.1.2 Elevation: ±35 degrees minimum

1.2 Mechanical

1.2.1 Azimuth: ±170 degrees rotation minimum at 40 degrees/sec^2 while maintaining pointing accuracy during rotation.

The electrical beam motion shall be accomplished with diode phase shifters in elevation and with frequency scanned slotted waveguide radiators in azimuth. The antenna shall be designed for electrical sequential lobing. Provision shall be made for a mechanical adjustment capability in elevation. The angle between the horizontal position and the beam normal of the antenna shall have an adjustable range of 0 to 25^{o}.

2.0 Electrical Requirements

2.1 Detailed Specification

2.1.1 Frequency Band - X

2.1.2 Center Frequency - See Note 1

2.1.3 Bandwidth for Frequency Scan - See Note 1

2.1.4 Azimuth Scan (Electrical): 7.7°

2.1.5 Elevation Scan (Electrical): $\pm 35^{\circ}$

2.1.6 Bandwidth, 3 dB (Note 2)

Azimuth	for 0° elevation	$.55^{\circ}$
	for $\pm 35^{\circ}$ elevation	$.67^{\circ}$
Elevation	for 0° elevation	$.66^{\circ}$
	for $\pm 35^{\circ}$ elevation	$.81^{\circ}$

2.1.7 Beam Pointing Error, Electrical

Elevation	.37 mrad

2.1.8 Electronic Beam Switching Time in Elevation — 1.0 MHz

2.1.9 Polarization — Horizontal

NOTE 1: As stated in antenna design specification. (Contract DAAA21-72-C-0725)

2.1.10 Sidelobe Level (Note 2)

Azimuth	at 0° elev. scan	-25 dB
	at $\pm 35^{\circ}$ elev. scan	-23 dB
Elevation	at 0° elev. scan	-25 dB
	at $\pm 35^{\circ}$ elev. scan	-23 dB

2.1.11 Terminal Gain at 0° Elev. scan at Center Frequency — 46.0 minimum (Note 3)

Terminal Gain at $\pm 35^{\circ}$ Elev. scan at Center Frequency — 45.0 dB (Note 3)

2.1.12 Power Capability — peak 30 kw; average 300 w

2.2 Major Subassemblies

2.2.1 For description and characteristics of GFE phase shifters see Picatinny Arsenal Document Technical Description TDPA-QAAR-2340.

2.3 Techniques Used

2.3.1 Wideband Operation for Frequency Scan

Appropriate techniques shall be applied to suppress the grating lobes and improve the radiation pattern while operating over the maximum bandwidth necessary for the frequency scan in azimuth.

2.3.2 Phase Randomization

To avoid the quantization error of the 4-bit phase shifter and the associated increase in sidelobe level, an appropriate phase randomization technique shall be used for each element of the horizontal array. The antenna buffer shall be able to compensate for this additional insertion phase.

NOTE 2: These parameters will be achieved at the center frequency.

NOTE 3: Based on an average phase shifter insertion loss of 2.5 dB.

2.3.3 Signal Coupling

To generate an optimum pencil beam with the most efficient low sidelobe pattern, proper weighting (30 dB Taylor excitation (N=4)) shall be applied by specifying appropriate coupling apertures from the vertical feed to the horizontal arrays and in establishing the slots in the horizontal elements.

2.3.4 CW Mode

The requirements for a CW mode of operation, to be added in the future, should be considered during the fabrication and design modifications of the antenna.

2.3 Mechanical Requirements

2.3.1 General Mechanical Requirements

2.3.1.1 The antenna array and its supporting structure shall be of sufficient rigidity and strength to minimize the deflection when subjected to the required acceleration and wind loading. When assembled on an appropriate servo mount pedestal (AN/SPS-48 or equivalent) and when subjected simultaneously to $40^{o}/sec^{2}$ acceleration in azimuth and 20 mph wind load, the antenna system shall exhibit no more than the following maximum deflection of the beam:

	BASIC ANTENNA (PHASE B)	ANTENNA + PEDESTAL + VEHICLE (PHASE C)
a. Azimuth	.377 mrad max.	.660 mrad max.
b. Elevation	.184 mrad max.	.690 mrad max.

2.3.1.2 The antenna shall be properly designed, fabricated and assembled to permit electrical and mechanical operation in accordance with this and the complete ARBAT radar system specifications when subjected to the environmental conditions specified in paragraph 2.8.

In a non-operative state, the antenna system shall be sufficiently rugged to withstand, without damage, vibration and shock during transportation per paragraphs 2.7 and 2.8, and wind loads and precipitation per paragraph 2.8.

2.3.2 Detailed Mechanical Specifications

2.3.2.1	Antenna Aperture Size: Height	- 120 ins.
	Width	- 144 ins.
2.3.2.2	Total Antenna Width	- 154 ins. (ref)
2.3.2.3	Adjustable Elevation Tilt	0 to 25^{o}
2.3.2.4	Mechanical Pointing Accuracy (deflection error due to all loading, see para 2.3.1.1) az	- .377 mrad max.
	el	- .184 mrad max.
2.3.2.5	Maximum Weight (Antenna, transceiver, buffer, power supplies, cables) without pedestal	1700 lbs. max

2.3.3 Antenna Microwave Hardware

The antenna shall include, but not be limited to, the following microwave hardware:

2.3.3.1 Vertical Feed Line

2.3.3.2 90^{o} Waveguide Twist (167)

2.3.3.3 Diode Phase Shifters (167)

2.3.3.4 Mounting Plate(s) for Phase Shifters

2.3.3.5 Horizontal Slotted Array Element (167)

2.3.3.6 Required coupling Elements, straight and angular (167 each)

2.3.4 Mechanical Mounting Structure

The microwave elements shall be securely mounted to a back structure.

2.3.5 Protective Enclosures

2.3.5.1 A protective enclosure (cover) shall be provided for the phase shifters.

2.3.5.2 Weather-resistant, electrically non-interfering plastic tape (tedlar-mylar or equivalent) shall cover the antenna radiating slots and prevent entrance and accumulation of water, sand and dust in the microwave elements.

2.3.5.3 The contractor shall supply a waterproof, soft plastic or coated or impregnated cloth hood to protect the antenna while not operated or while in storage.

2.3.6 Protective Finishes

The exterior surfaces of the antenna system (wave-guides, mounting structure, enclosures, transceiver) shall be covered with protective coating. The color shall be silver or white, to minimize the heating due to solar radiation. The interior surfaces shall have appropriate corrosion-resistant finish.

2.3.7 Material Compatibility

Different materials in contact with each other shall be chosen with careful regard to the electrochemical series so that they are compatible and will not corrode because of electrical potential differences.

2.4 Testing

The contractor shall perform the following tests:

2.4.1 Laboratory tests for microwave components (vertical feed, horizontal array elements, etc).

2.4.2 Laboratory and range tests for the 9-element test array.

2.5 Calibration

All instrumentation used for laboratory and range testing shall be properly calibrated with standards traceable to the National Bureau of Standards.

2.6 Maintenance

For ease of maintenance, electrical and microwave components shall be mounted so as to permit field testing and replacement by qualified personnel.

2.7 Mobility/Transportability

2.7.1 In the next phase (C), the antenna system will be mounted on a servo pedestal located on an antenna vehicle. The vehicle will be transported by public highways and/or railroads between proving grounds. Within the proving grounds, graded, light duty, hard surface roads will be used. However, the system shall be capable of being moved at low speeds (5 mph) on unimproved dirt roads. The antenna system shall be able to withstand, without damage, the above transportation requirements.

2.7.2 During transportation within the proving grounds the overall system height shall be less than 16 feet, 12 feet desired. If it is necessary to lower the antenna to meet this requirement, the lowering mechanism shall be self-contained and hydraulically or hand operated. The width of the system during transportation shall not exceed 8 feet. When moving from site to site within the proving grounds, a maximum set-up time of 8 hours is required, four hours desired.

2.7.3 For transportation between proving grounds, it shall be possible to deploy the system into a configuration transportable over public roads and compatible with applicable federal, state and local regulations. If necessary, subsystem may be removed or lowered from the main assembly with the aid of a crane (to be provided by Proving Grounds).

2.8 Environmental Requirements

2.8.1 Temperature

The antenna system shall be capable of operating in an ambient air temperature range of $-65^{o}F$ to $+165^{o}F$ and maintaining the accuracy requirements specified in section 2 for an ambient air temperature range of $-20^{o}F$ to $+120^{o}F$.

2.8.2 Wind

The antenna system shall be capable of operating and maintaining the accuracy requirements specified in section 2 in winds up to 30 mph. In addition, when the antenna is secured and not operating, it shall be capable of withstanding winds up to 75 mph.

2.8.3 Precipitation (Rain, Snow, Hail, Ice)

The antenna system shall be properly designed and fabricated to prevent limitation in accuracy and operational capability caused by internal leakage and accumulation of precipitation. The effects of external accumulation should be kept as low as possible by proper design.

2.8.4 Humidity

The antenna system shall be properly designed and fabricated to prevent deterioration of system performance due to humidity encountered in the continental United States.

2.8.5 Sand and Dust

The antenna system shall be properly designed and fabricated to prevent sand and dust particles from entering the interior of the system, accumulating there and causing electrical and/or mechanical interference.

2.8.6 Solar Radiation

The antenna system shall be designed to operate under extreme environmental conditions with a solar load of 360 BTU per square foot per hour taken at the worst orientation of the sun relative to the equipment. To limit the heating effect, the antenna system shall have an exterior reflective color of silver or white.

2.8.7 Shock

The antenna system, when properly mounted on servo pedestal and antenna vehicle, shall be able to withstand the effects of a 10g shock environment (any direction)

during transit by truck. The equipment shall be designed to withstand humping loads common to rail transportation.

2.9 Reliability

The reliability of the antenna system shall be sufficiently high to permit achievement of the desired objective:

MTBF for the <u>entire radar system</u> - 200 hours.

2. DESIGN DESCRIPTIONS

The following sub-sections provide brief descriptions of the major components in the ARBAT antenna design. Detailed physical descriptions are generally not included in this section, except that in some instances basic dimensions are included on sketches to provide the reader with sufficient information to facilitate visualization of the component described.

Test results for critical parameters are included for those components where such tests are applicable.

Drawings for the antenna are packaged separately from this report (3 copies supplied to Picatinny Arsenal and requests for copies should be made there).

The following drawings are available at Picatinny Arsenal.

	Drawing	Component/Assembly
1.	140300-1	Antenna Assy, ARBAT
2.	140301-1	Back Structure, Antenna
3.	140311-1	Twist, 90°, W/G
4.	140309-2	Array Assy, W/G
5.	140309-2	Parts List
6.	140312-1	Flange
7.	140312-2	Flange
8.	140307-1	Feed Line
9.	140313-1	Load Assy
10.	140310-1	Comb
11.	140310-2	Comb
12.	140317-1	Comb
13.	140317-2	Comb
14.	140315-1	Structure
15.	140328-1	Bracket
16.	140328-2	Bracket

	Drawing	Component/Assembly
17.	140316-1	Panel
18.	140318-1	Bracket
19.	140319-1	Block
20.	140320-1	Retainer
21.	140308-1	Monitor
22.	140325-1	Load
23.	140321-1	Cover
24.	140322-1	Cover
25.	140323-1	Cover
26.	140324-1	Angle
27.	140302-1	Support
28.	140303-1	Support
29.	140304-1	Support
30.	140304-2	Support
31.	140305-1	Base
32.	140306-1	Clevis
33.	140326-1	Rod End
34.	140327-1	Clevis

2.1 Back Structure

The antenna back structure is a rigid welded aluminum (6061-T6) structure designed to support the microwave elements of the antenna with the associated phase shifter drive electronics and the transmitter/receiver. The structure is designed for mounting on a rotating pedestal which will provide the mechanical portion of the required beam scanning capability. A non-scalar structural schematic sketch is used for clarity in Figure 7 to illustrate the basic construction of the back support.

A full view, artists sketch, of the backside of the antenna with the transmitter/receiver mounted shows the position of the transceiver/ mounting, Figure 8.

The measured weight of the completed back structure is 722.0 pounds which includes the array positioning combs.

The obvious prime requirement for the back structure is rigidity and desirably the rigidity should be achieved with reasonably light-weight. Computer defelection analysis results are shown in Figure 9.

The mechanical structure analysis for the total antenna structure is contained in Appendix A.

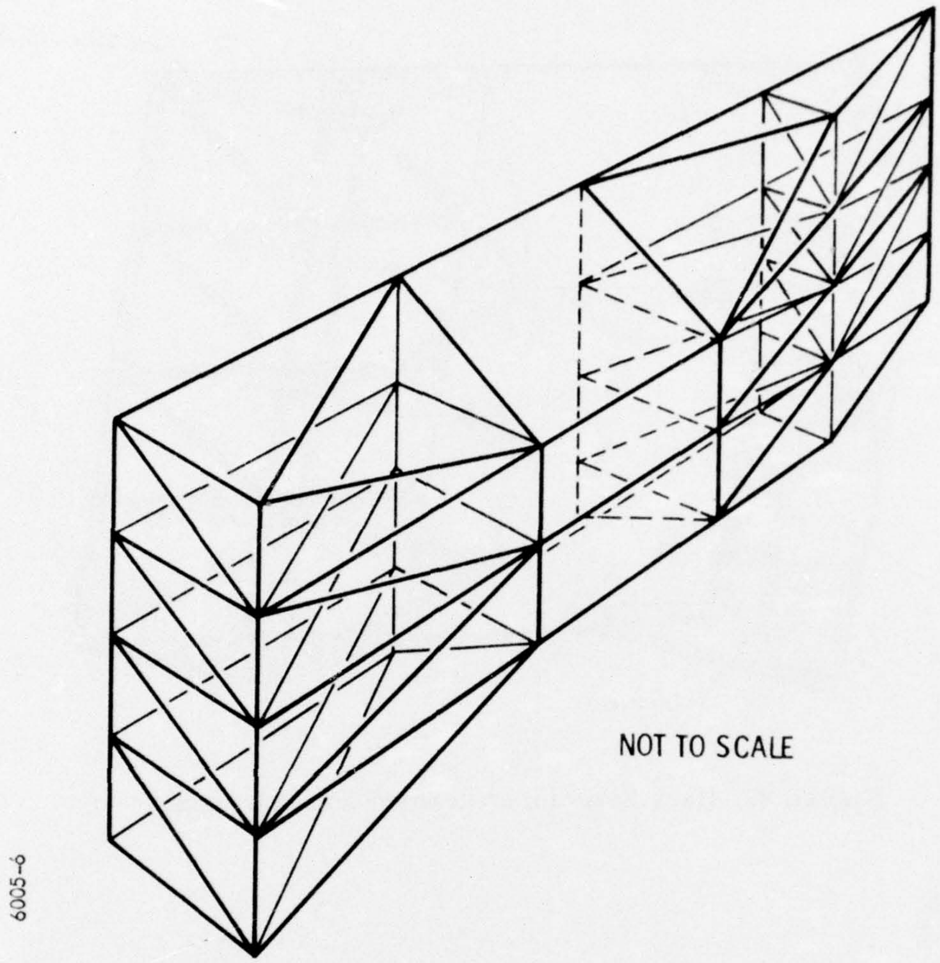


Figure 7. Back Structure Truss Elements

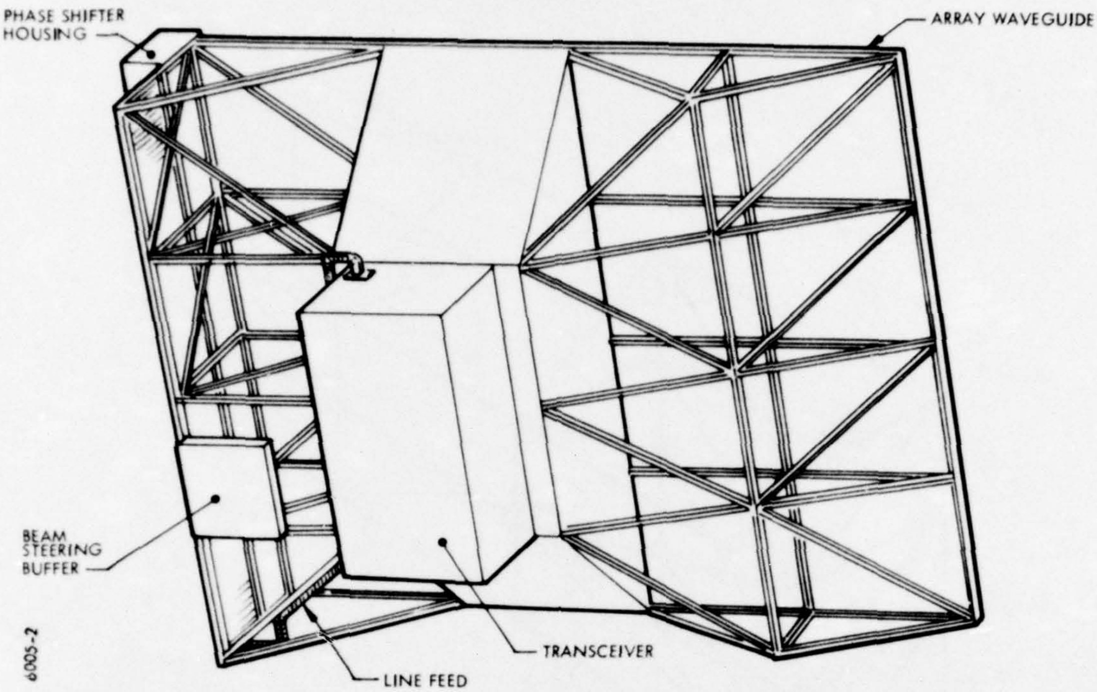
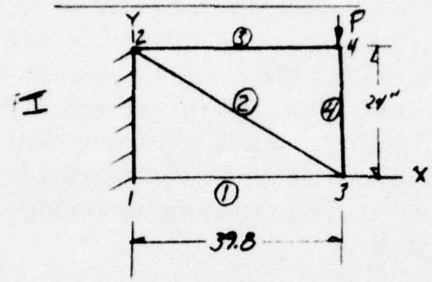


Figure 8. Back Structure/Transceiver Mounting

	NAME	DATE	ITT Gilfillan Inc.	SHEET 13 OF
PREPARED	S. Coe	7/25/73	TITLE COMPUTER MODEL FOR STRUPAK ANALYSIS	SKETCH NO. PHASE B
CHECKED				
APPROVED				

COMPUTER MODELS STRUPAK PROGRAM 2DTSAP

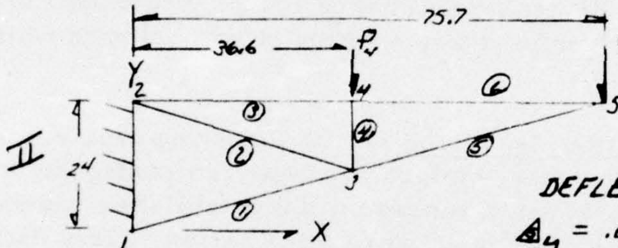


$P_4 = 16.5 + 13.6 = \underline{30.1 \text{ lb}}$

DEFLECTION RESULTS

$\Delta_y = .000979$ IN

$\epsilon_{H_2} = \frac{.000979}{39.8} \times 1000 = \underline{.025 \text{ mr}}$



$P_4 = 33 + 5.4 = \underline{38.4 \text{ lb}}$

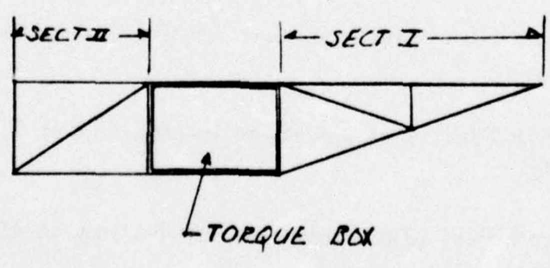
$P_5 = 16.5 + 3.6 = \underline{20.1 \text{ lb}}$

DEFLECTION RESULTS

$\Delta_y = .004122$ IN

$\epsilon_{H_5} = \frac{.004122(1000)}{75.7} = \underline{.054 \text{ mr}}$

ASSUME CENTER SECTION TORQUE BOX TO BE RIGID & DEFLECTIONS ARE DUE TO BENDING OF TRUSS STRUCTURE ONLY



6005-8

Figure 9. Computer Deflection Analysis

2.2 Horizontal Array Waveguide Sections

The radiating elements in the ARBAT antenna are horizontal array waveguide sections. Radiation is via dual pairs of slots milled in the narrow dimension side. Array waveguide sections are fabricated from thin wall precision waveguide made from 6061-T6 aluminum alloy conforming to MIL-W-85/6 requirements. This waveguide is 0.400 by 0.750 inches inside and 0.476 by 0.826 inches outside. Each array section is 145.86 inches in length and contain 161 dual slot pairs (322 milled slots) in the narrow dimension radiating edge. Each individual array section is fitted with a flange at each end for mating with a diode phase shifter at the feed end and with a coupler flange plate at the opposite or performance monitor end. The flanges are welded at each corner to the mating waveguide and the remaining area of contact is then sealed.

Before assembly of the horizontal array sections, the slotted side is covered with a multi-layer RF transparent tape (G. T. Schjeldahl Co., Type G.133500-014) and all surfaces are eventually painted with white epoxy paint.

Horizontal Array Section Test Data. - The following data represents the individual element test results obtained for finalized configurations. Consequently, the results presented represent the established requirements for which the production samples were later tested. This data is generally presented in one of two forms, tabular or graphic and in all instances the data is self explanatory. The following specific data is contained in this section:

a. Insertion Phase Measurement/Comparison Test Set up (Figure 10)

b. Insertion Phase Plot (after etching process) (Figure 11)

c. Phase Error Plot (2nd aperture excitation at 9.3 GHz) (Figure 12)

d. Phase Error Plot (2nd aperture excitation at 9.65 GHz) (Figure 13)

e. Phase Error Plot (2nd aperture excitation at 10 GHz) (Figure 14)

f. Amplitude Plot (1st aperture excitation at 9.65 GHz) (Figure 15)

g. Amplitude Plot (2nd aperture excitation at 9.3 GHz) (Figure 16)

h. Amplitude Plot (3rd aperture excitation at 10 GHz) (Figure 17)

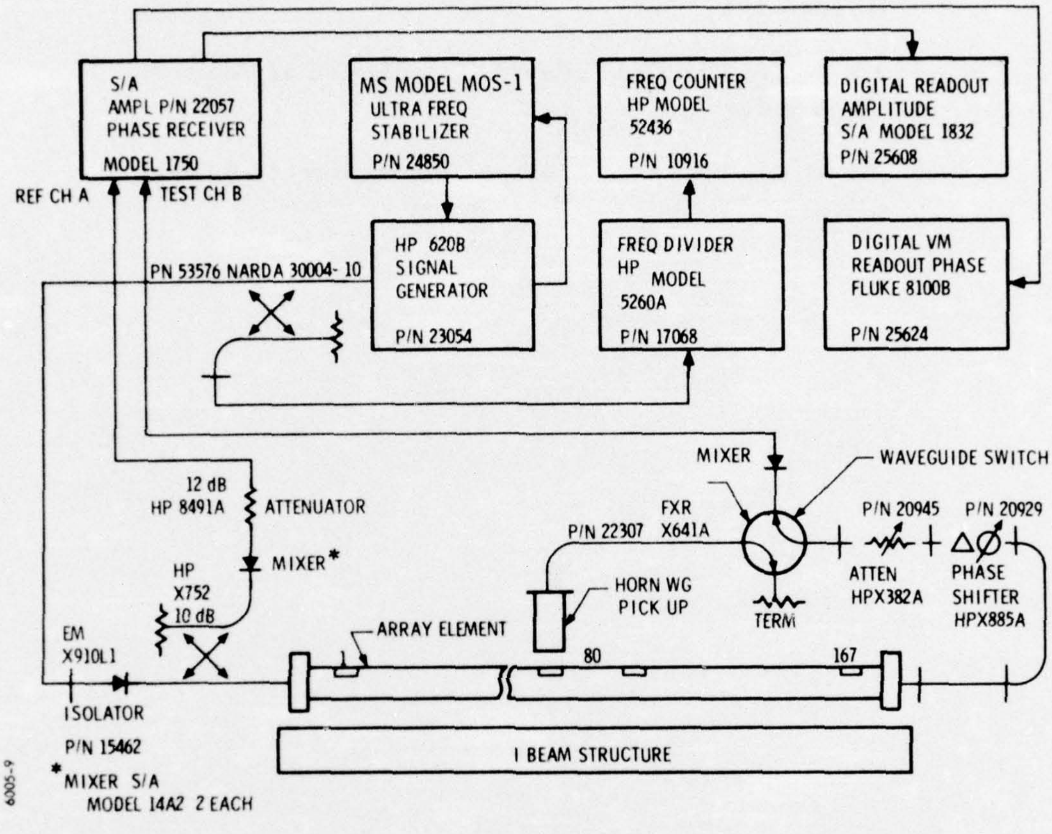
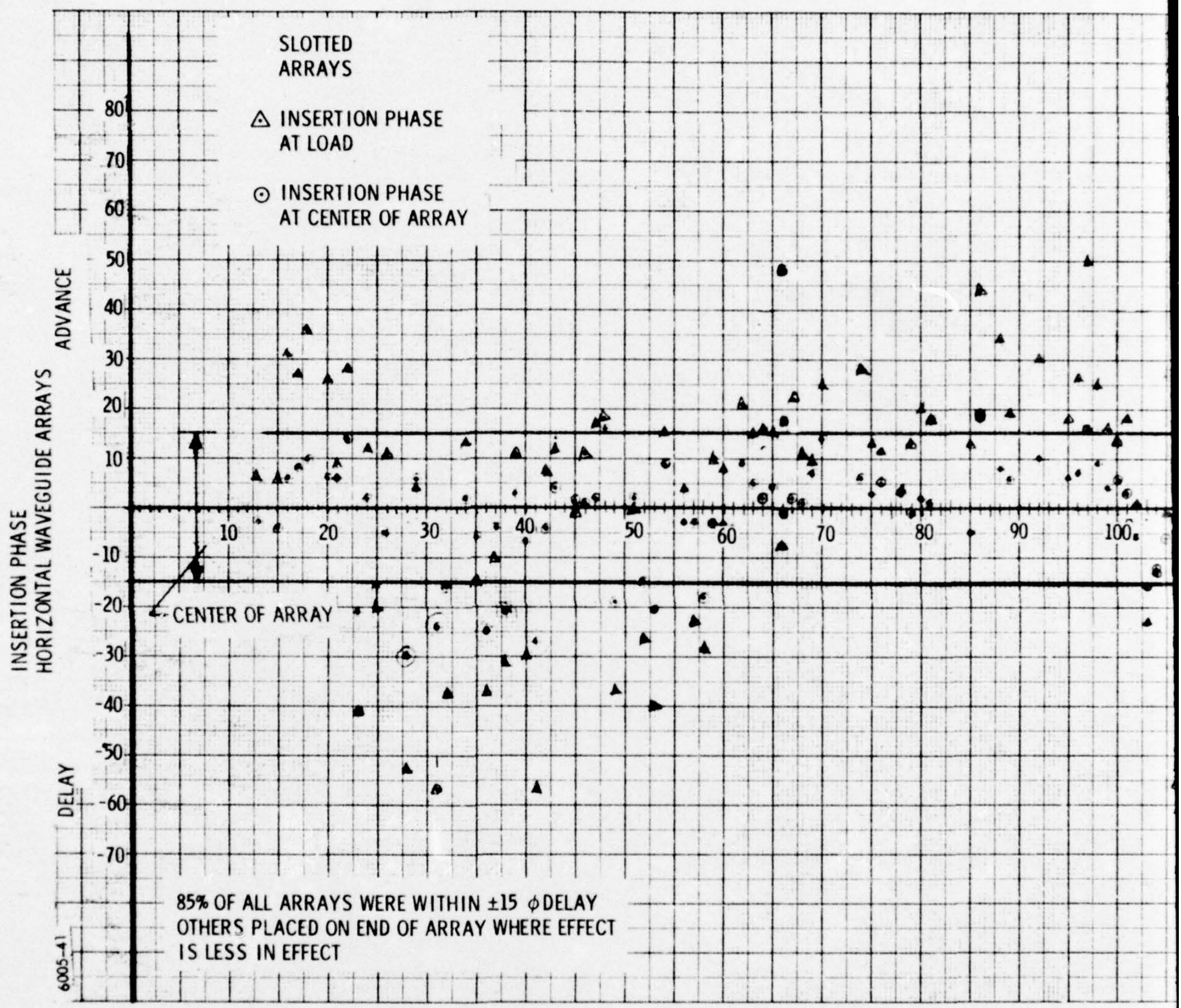


Figure 10. Insertion Phase Measurement/Comparison Test Setup


SLOTTED
ARRAYS
INSERTION PHASE
AT LOAD
INSERTION PHASE
AT CENTER OF ARRAY
INSERTION PHASE
HORIZONTAL WAVEGUIDE ARRAYS
ADVANCE
DELAY
80
70
60
50
40
30
20
10
-10
-20
-30
-40
-50
-60
-70
10
20
30
40
50
60
70
80
90
100
CENTER OF ARRAY
85% OF ALL ARRAYS WERE WITHIN ±15 φ DELAY
OTHERS PLACED ON END OF ARRAY WHERE EFFECT
IS LESS IN EFFECT
6005-41

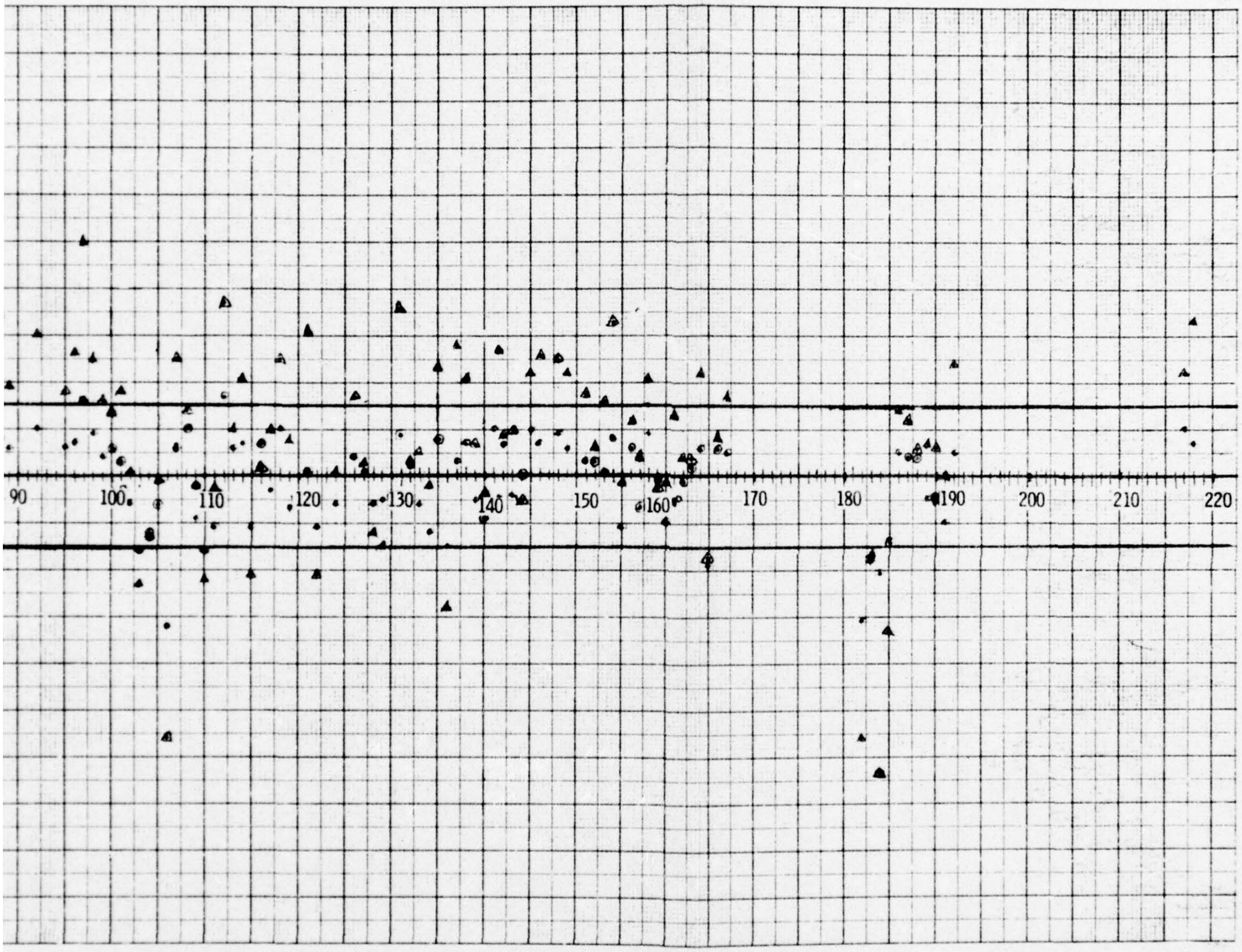


Figure 11. Insertion Phase Plot (After Etching Process)

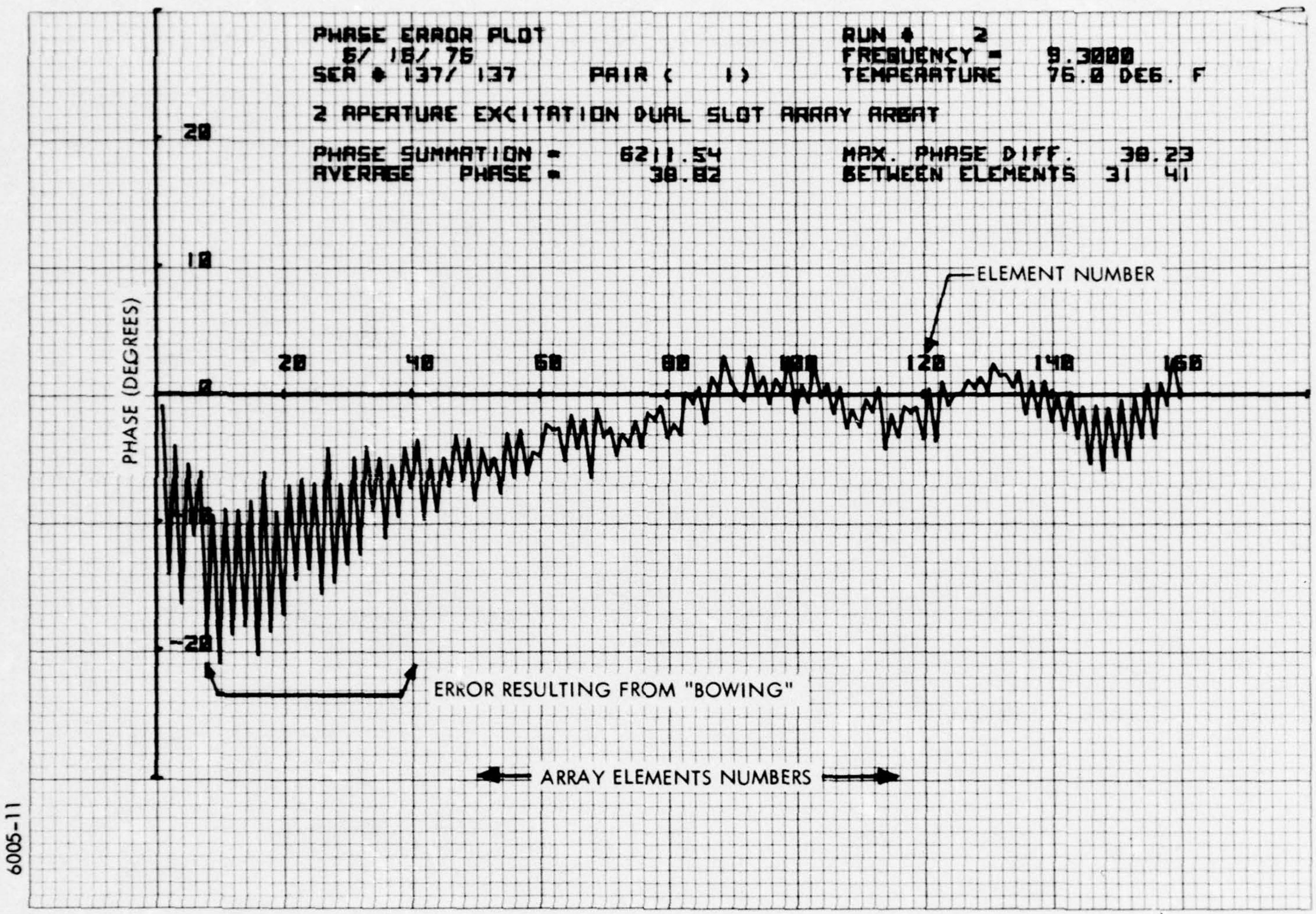


Figure 12. Phase Error Plot (2nd Aperture Excitation at 9.3 GHz)

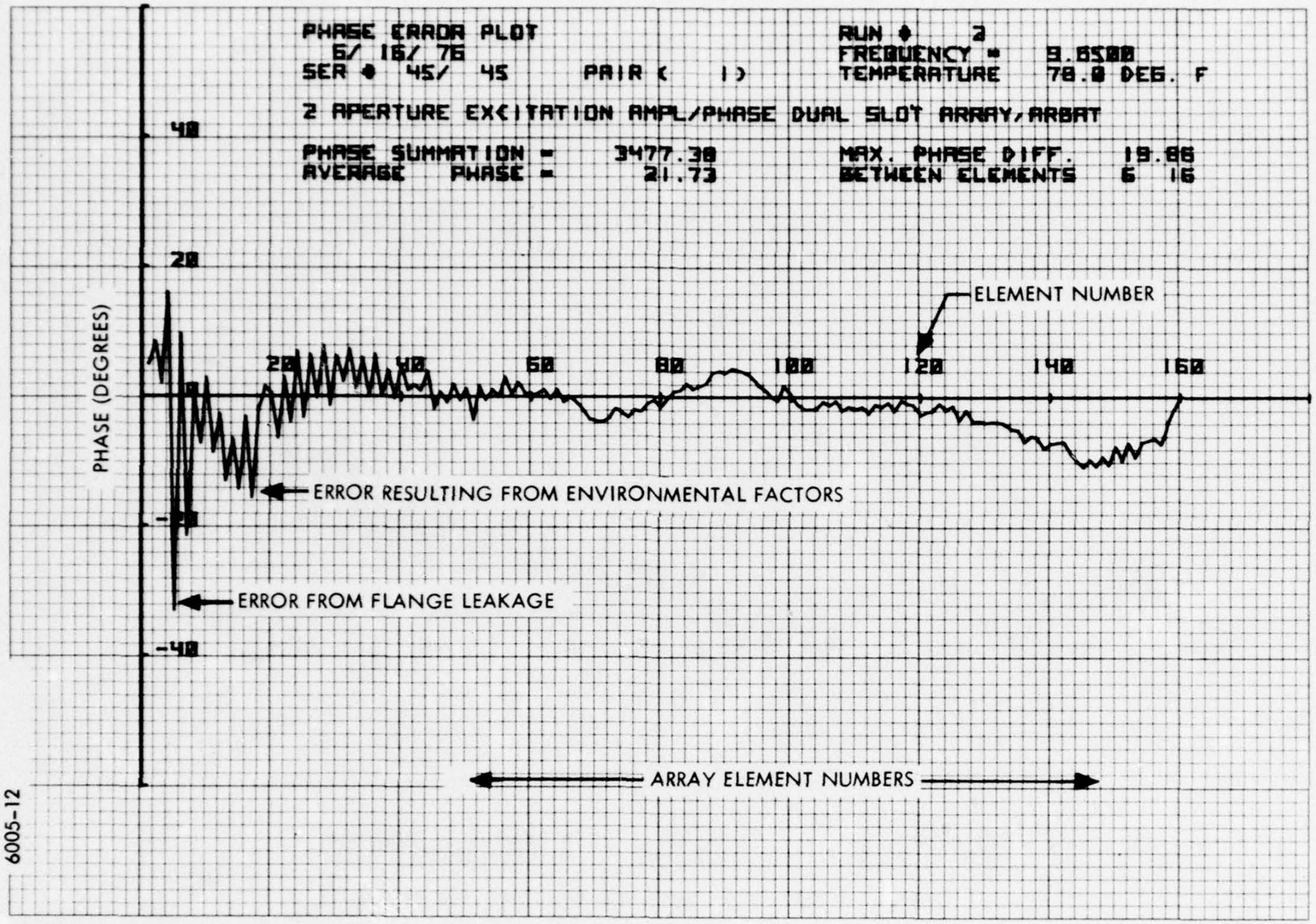
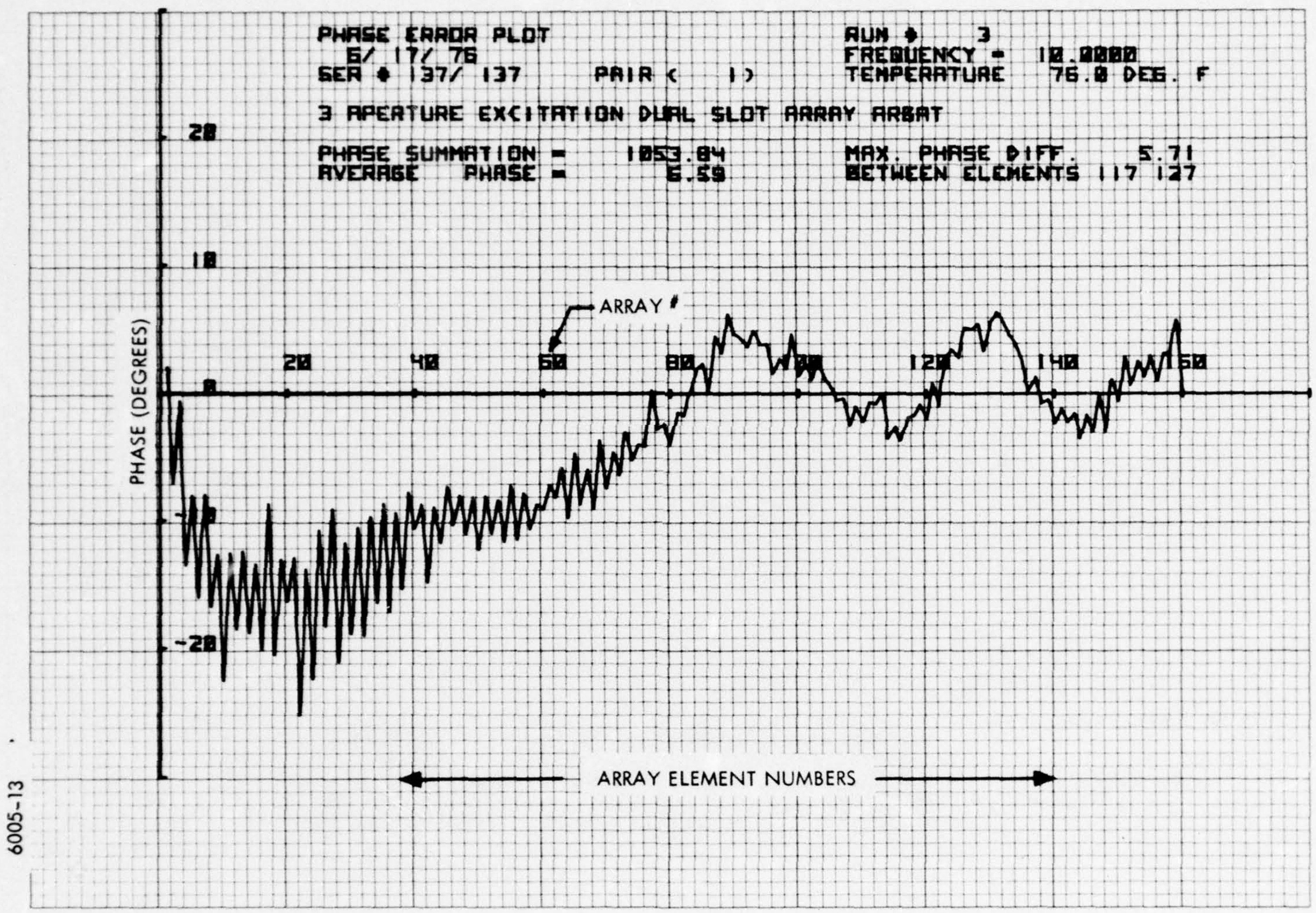
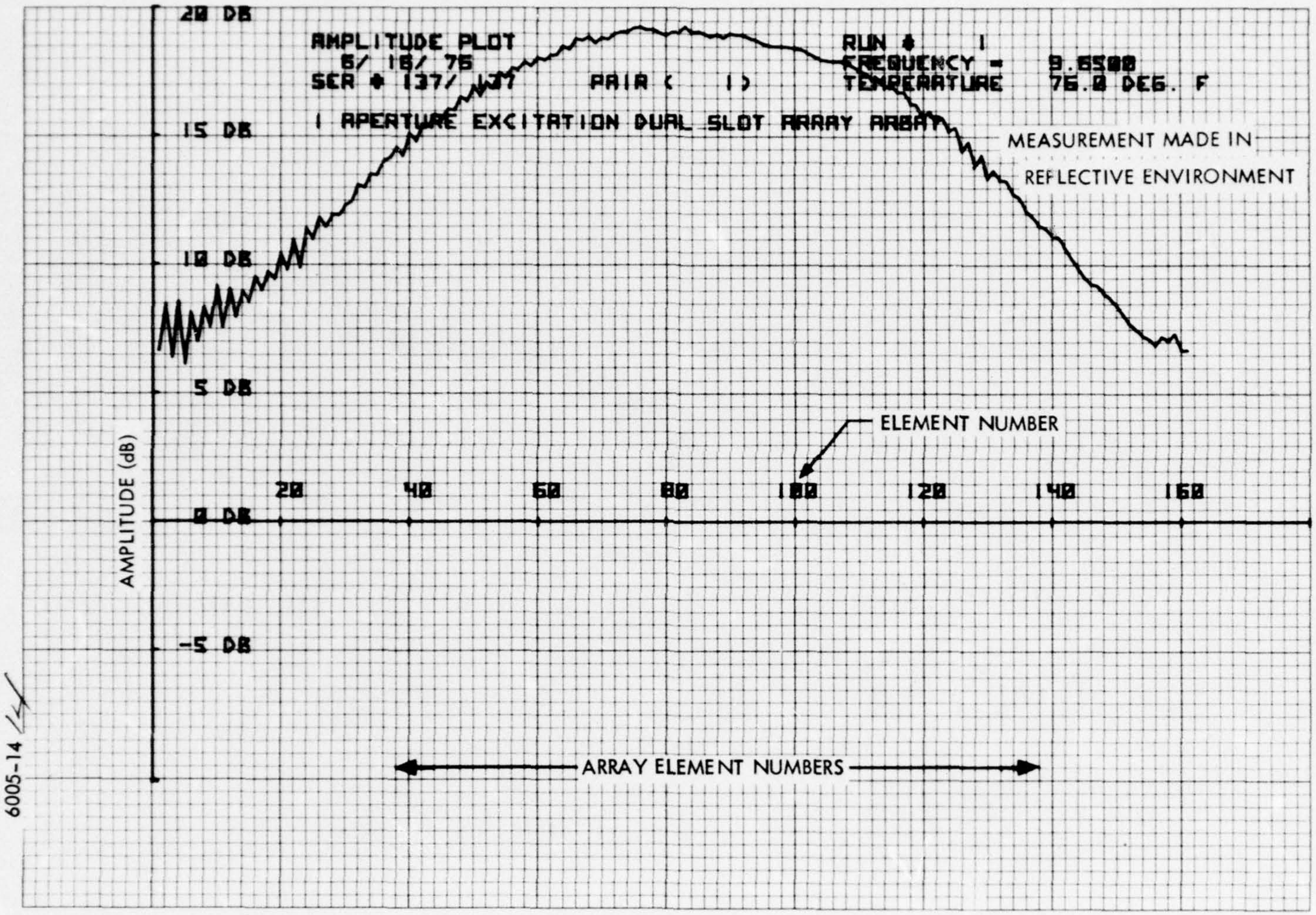


Figure 13. Phase Error Plot (2nd Aperture Excitation at 9.65 GHz)



6005-13

Figure 14. Phase Error Plot (3rd Aperture Excitation at 10 GHz)



6005-14

Figure 15. Amplitude Plot (1st Aperture Excitation at 9.65 GHz)

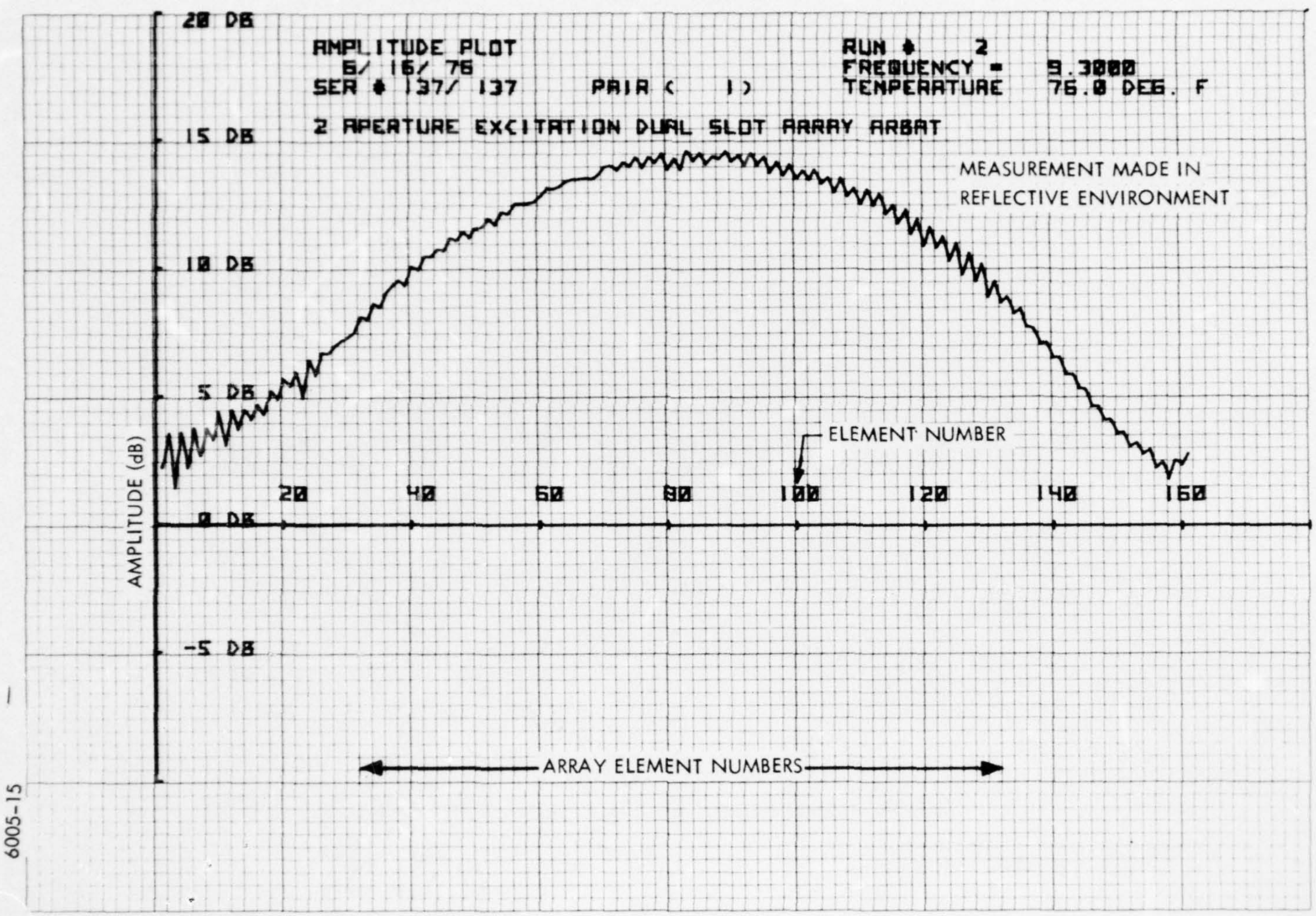


Figure 16. Amplitude Plot (2nd Aperture Excitation at 9.3 GHz)

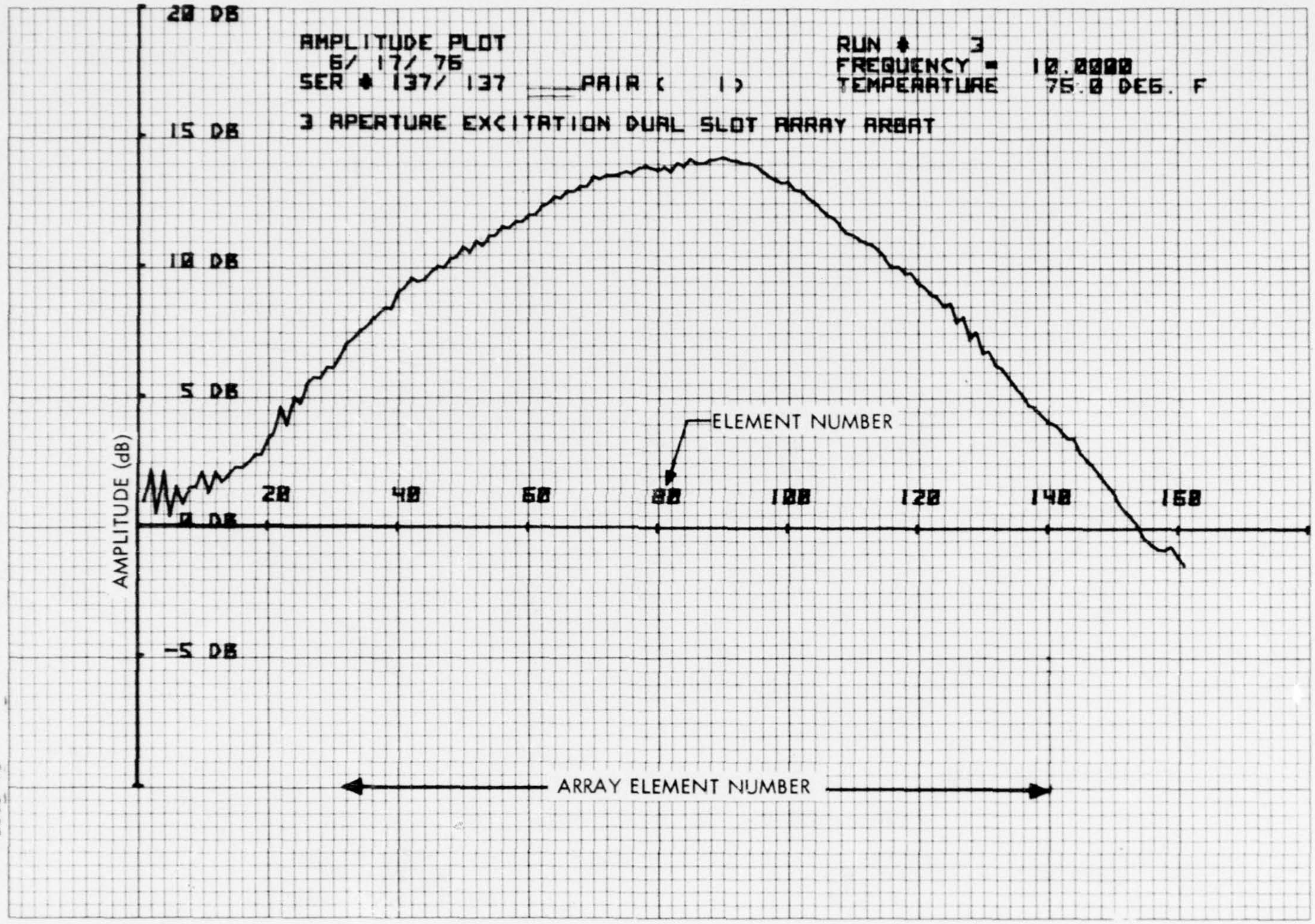


Figure 17. Amplitude Plot 3rd Aperture Excitation at 10 GHz)

2.3 Vertical Feed Line

The vertical feed line provides the single RF connection between the transmitter/receiver and the antenna. The RF input/output connection is at the lower end of the vertical feed waveguide section. Connection to the feed line is made with a short section of flexible waveguide. The vertical feed distributes the input to individual horizontal arrays by way of four-port coupling apertures into 90 degree twist sections that distribute energy to and from the 167 horizontal array sections via the diode phase shifters. The 90 degree twist sections are attached to the vertical feed line by dip brazing. The feed line and its position in the antenna assembly are shown in the photograph, Figure 18.

Vertical Feed Line Configuration. - The feed line is 120.52 inches long and is fabricated in three separate sections from precision waveguide (aluminum) per MIL-W-85/1. Waveguide dimensions are 0.400 x 0.900 inside by 0.500 x 1.00 inch outisde. See drawing 140307 for design details (available at Picatinny Arsenal).

Vertical Feed Tests. - After finalization of design detail, tests to determine actual insertion loss and VSWR were run. The results of the tests are shown graphically in Figure 19 Insertion Loss, Figure 20 VSWR (Elements 113 to 167), and Figure 21 VSWR (Expanded Figure 20).

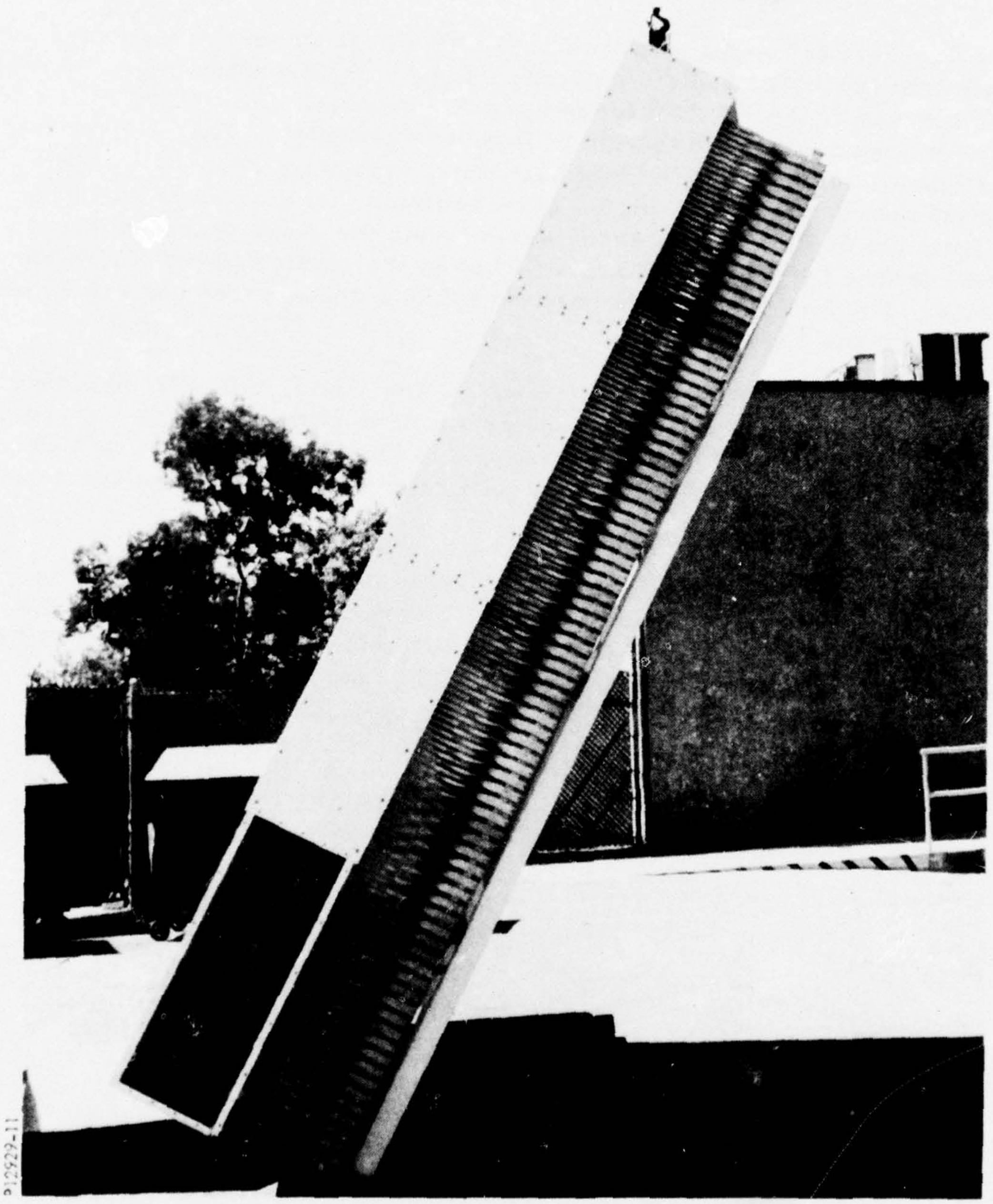


Figure 18. Vertical Line Feed in Assembled Antenna

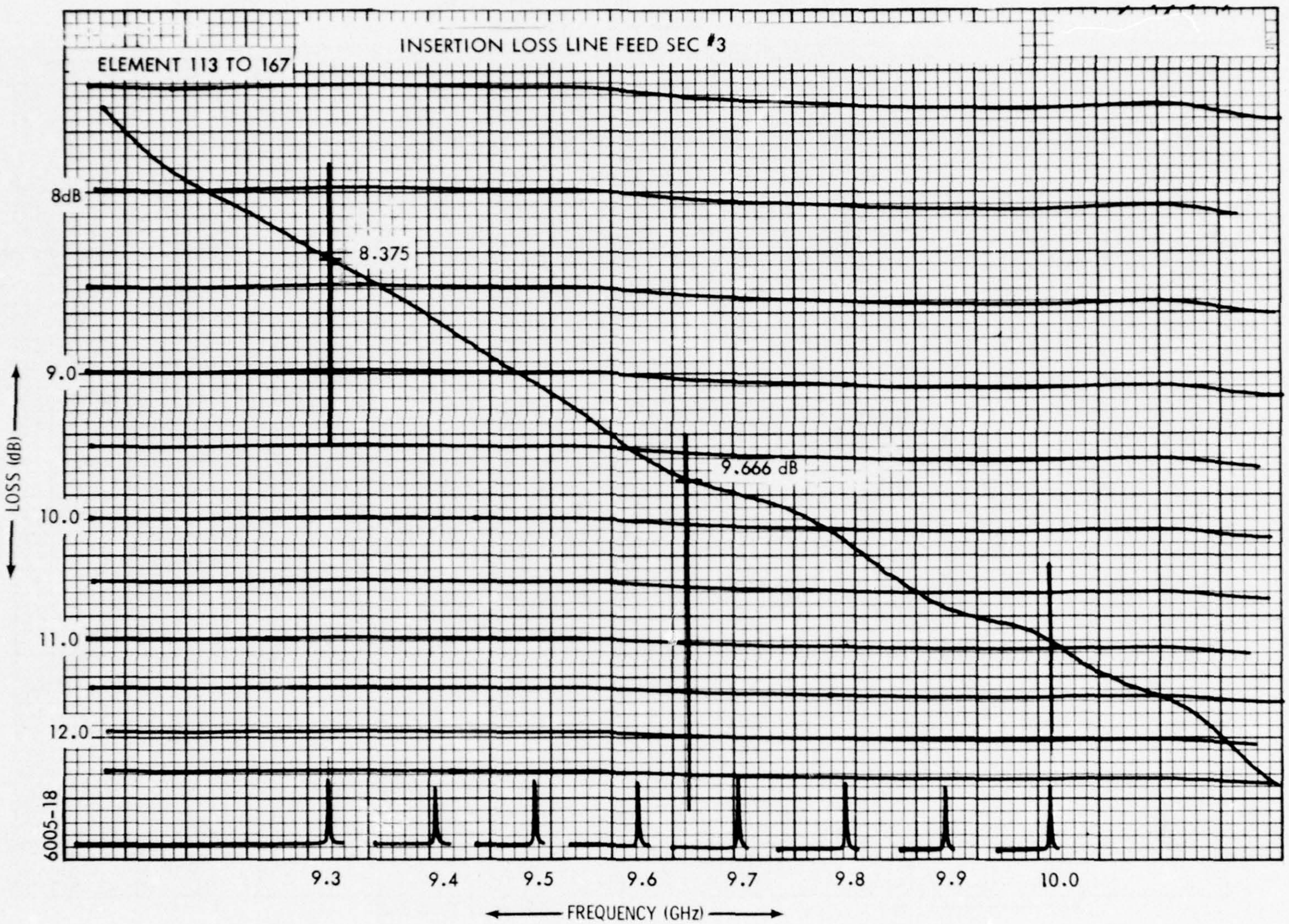


Figure 19. Vertical Line Feed Insertion Loss vs Frequency

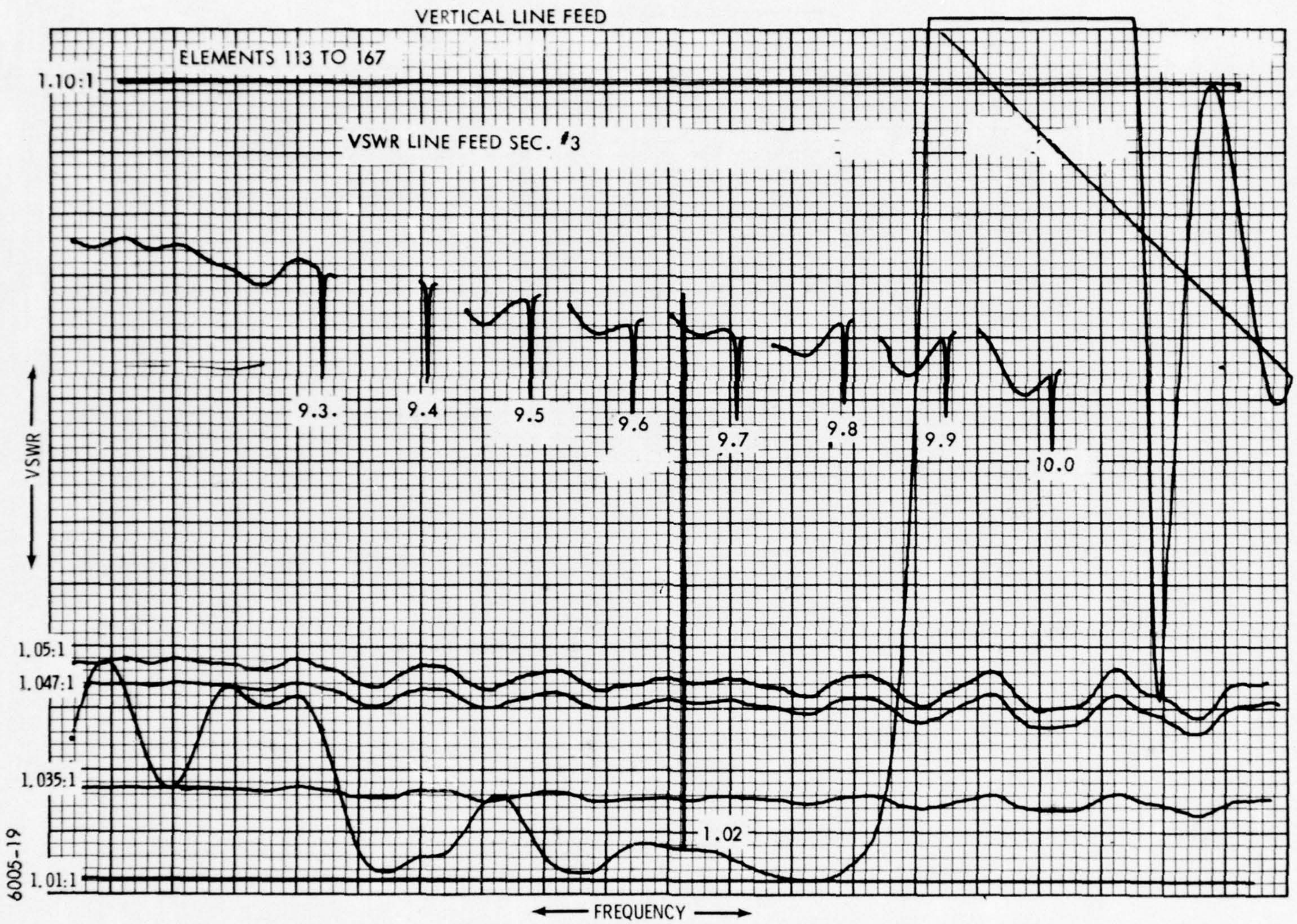


Figure 20. VSWR vs Frequency: Line Feed Section #3

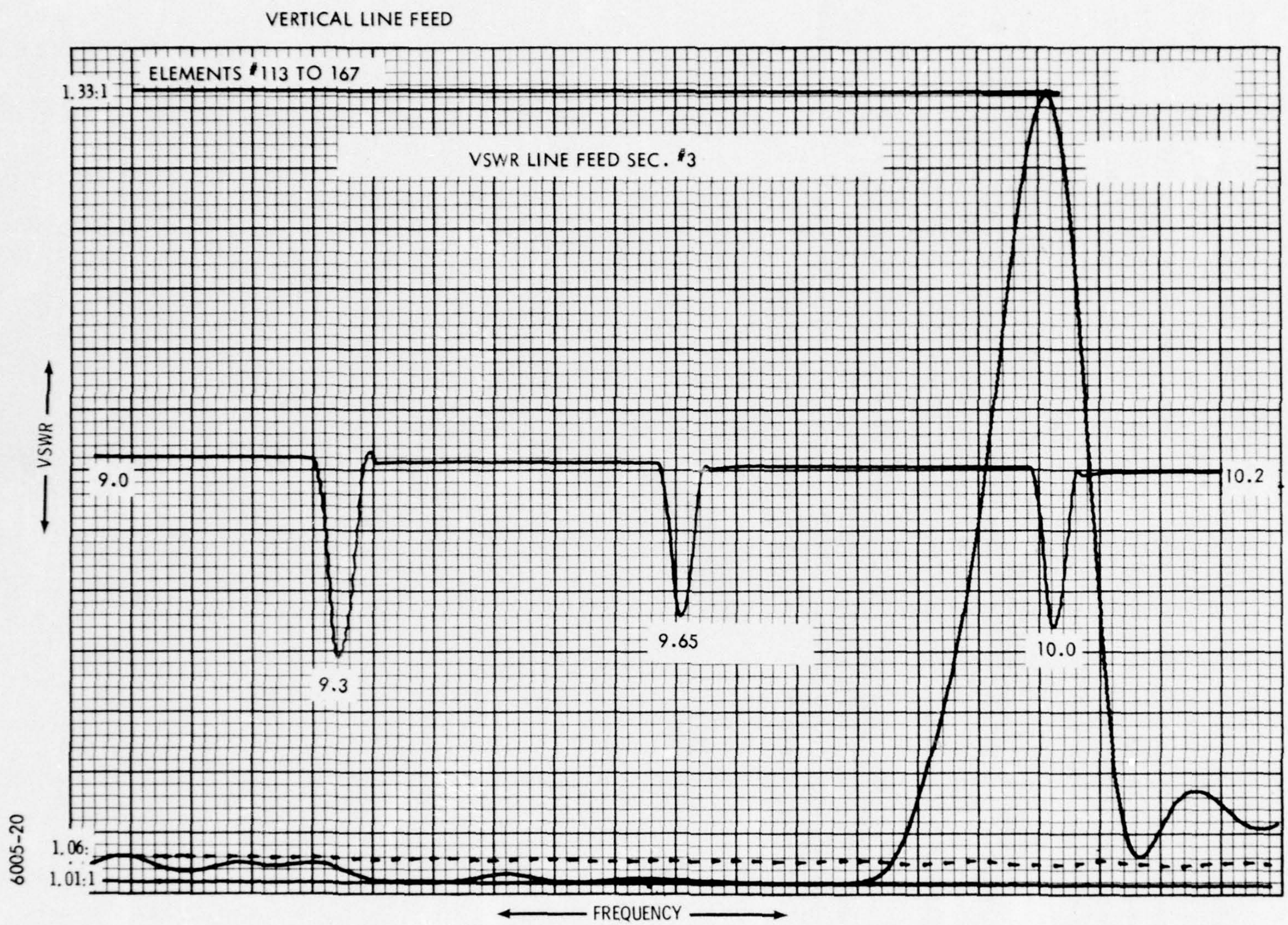


Figure 21. VSWR vs Frequency: Line Feed Section #3 (Expanded Scale)

2.4 90 Degree Twist Crossguide Coupler Section

Horizontal array sections are coupled to the vertical feed line (via diode phase shifters) by a 90° twist waveguide section with four port coupling apertures. A loading block is inserted in the closed end of each coupler section opposite the feed line. Four port coupling slots match apertures in the vertical feed line. Attachment of coupling sections to the feed line is by dip brazing. The physical configuration of the production section is shown in the photograph, Figure 22.

Physical Configuration. - The crosscouplers are fabricated from precision waveguide (6061-F aluminum alloy in accordance with MIL-W-85/1). Figure 23 illustrates the configuration of the part. (See drawing 140311 for dimensions, available at Picatinny Arsenal.)

Coupler Testing. - Testing this element was relatively simple because of its configuration and previous tests for terminating loads and coupling slot dimensions. VSWR tests were conducted on a sample quantity of coupling sections with results shown in Figure 24.

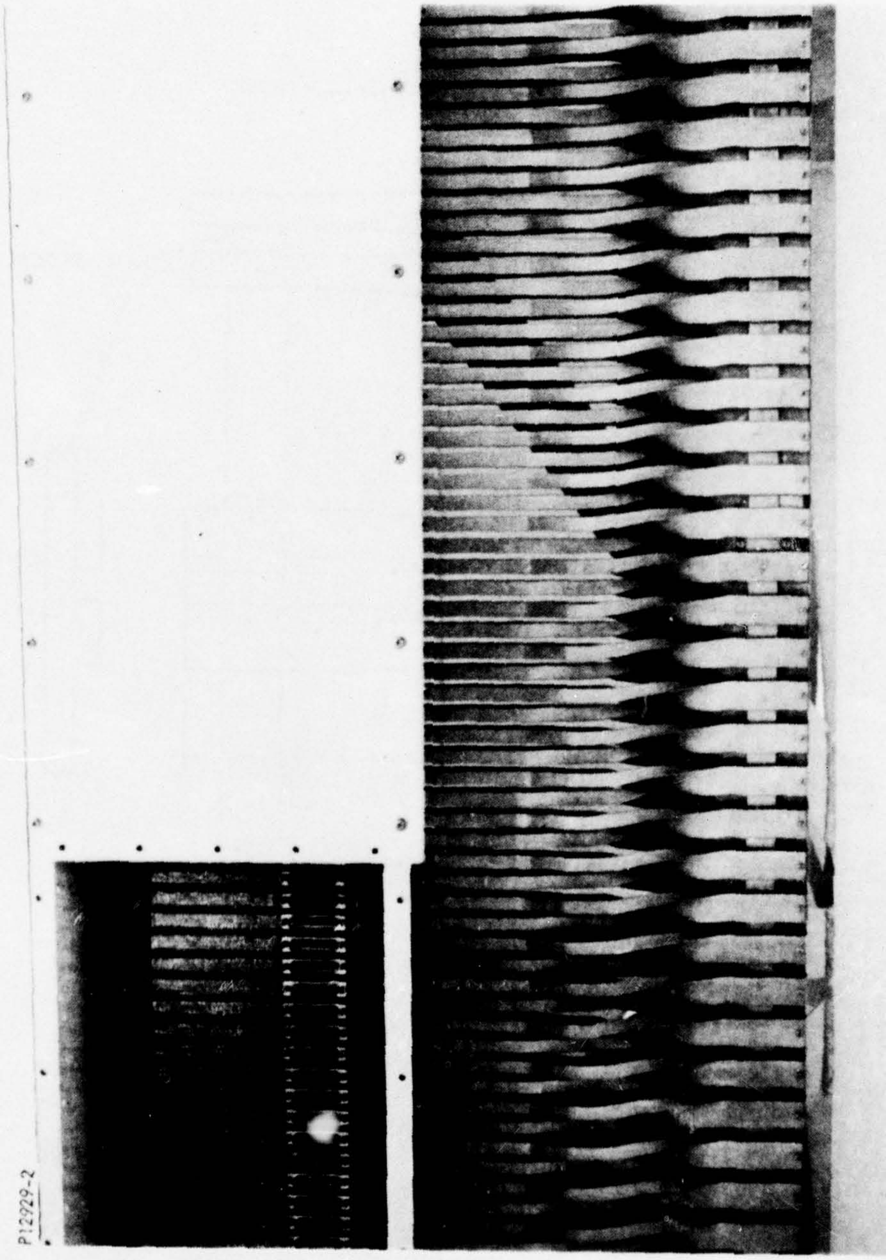


Figure 22. Ninety Degree Twist Crossguide Coupler in Assembled Antenna

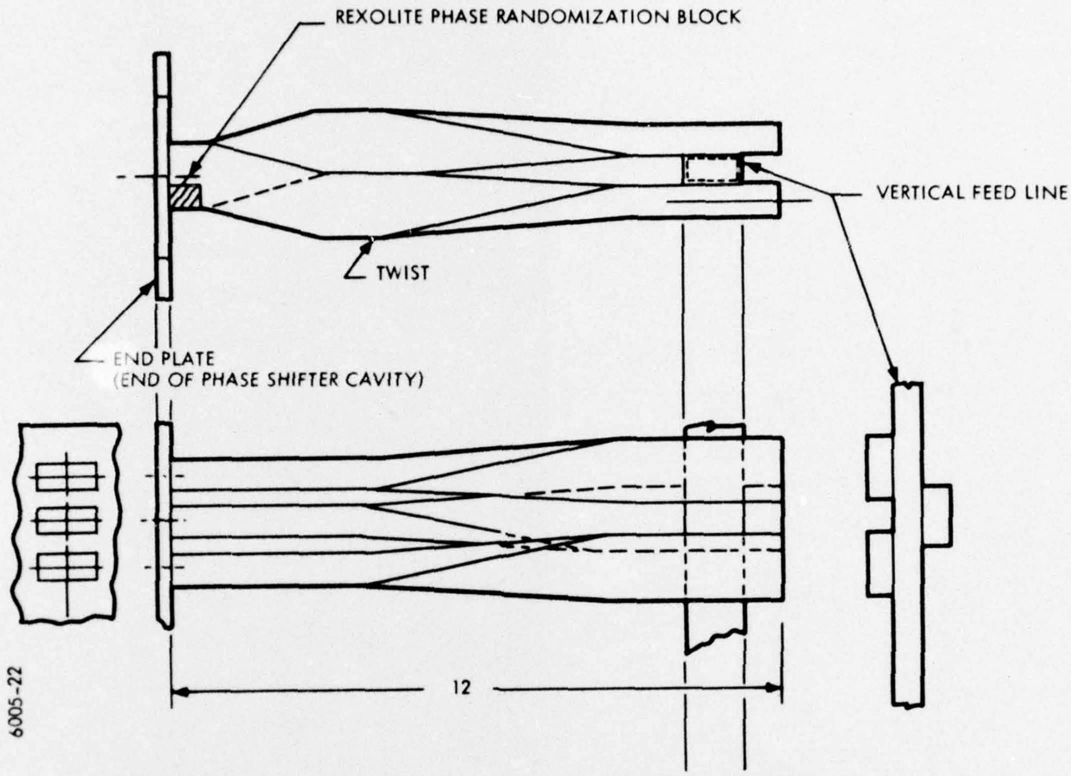


Figure 23. Ninety Degree Twist Crossguide Section

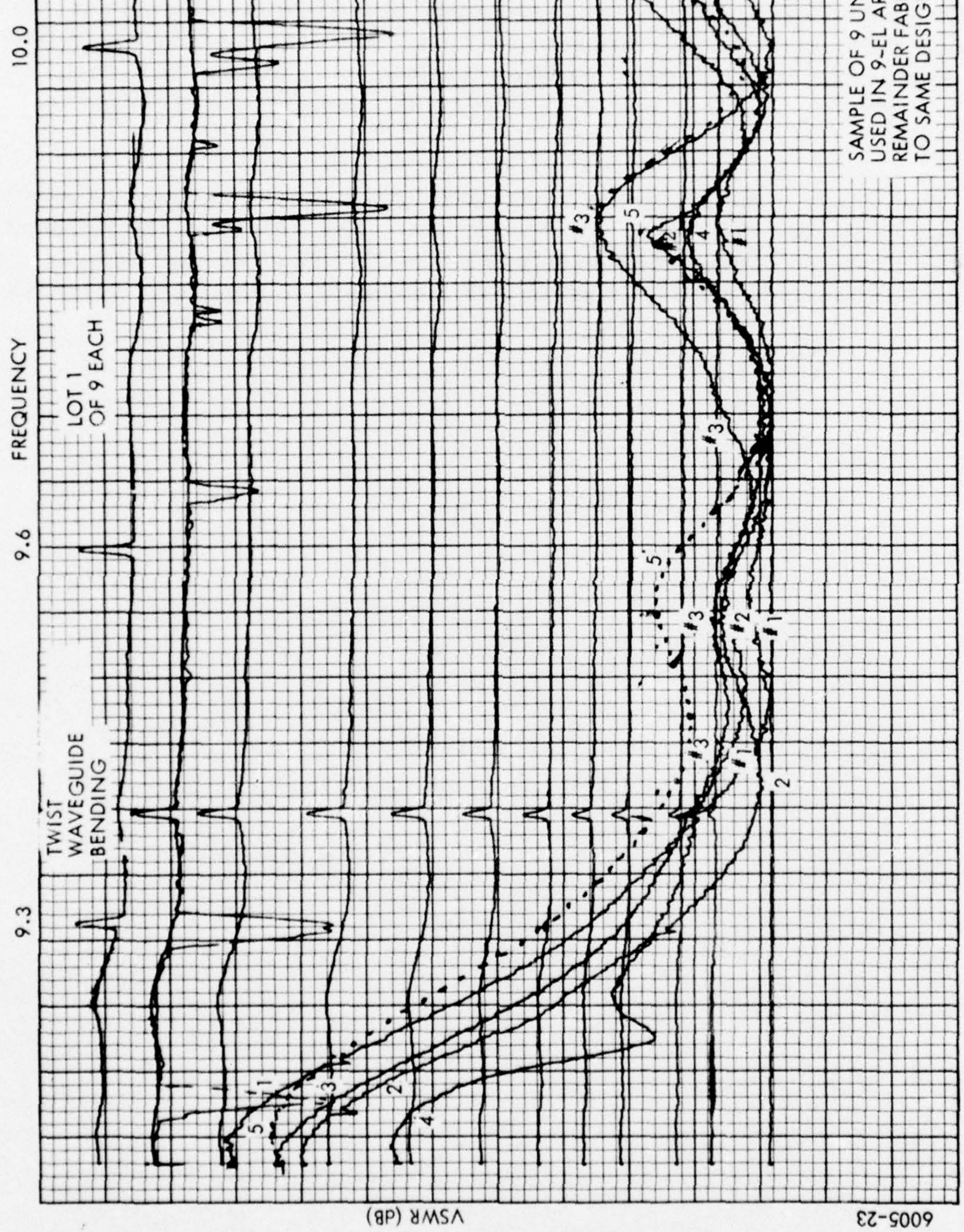


Figure 24. Ninety Degree Twist Section VSWR Plot

2.4.1 Load: Termination (Vertical Feed Coupler). - Equalizing termination loads are required for each coupler section at the vertical feed line. The loads used in the ARBAT antenna are fabricated from ECCOSORB 17 Compound, which is molded and then machined to final dimensions. The load element is then cemented to a waveguide cap plug and the assembly is installed in the ends of each coupling section. The load element is drilled for a 4-40 screw which further secures the load/plug assembly in the coupling section. All load elements in the 167 couplers are of uniform dimensions.

Load Test. - Sample loads were tested over the operating frequency range to insure acceptable return loss values. The VSWR values obtained from the finalized design are shown in Figure 25. For detailed design including dimensions see Drawing 140313 (available at Picatinny Arsenal).

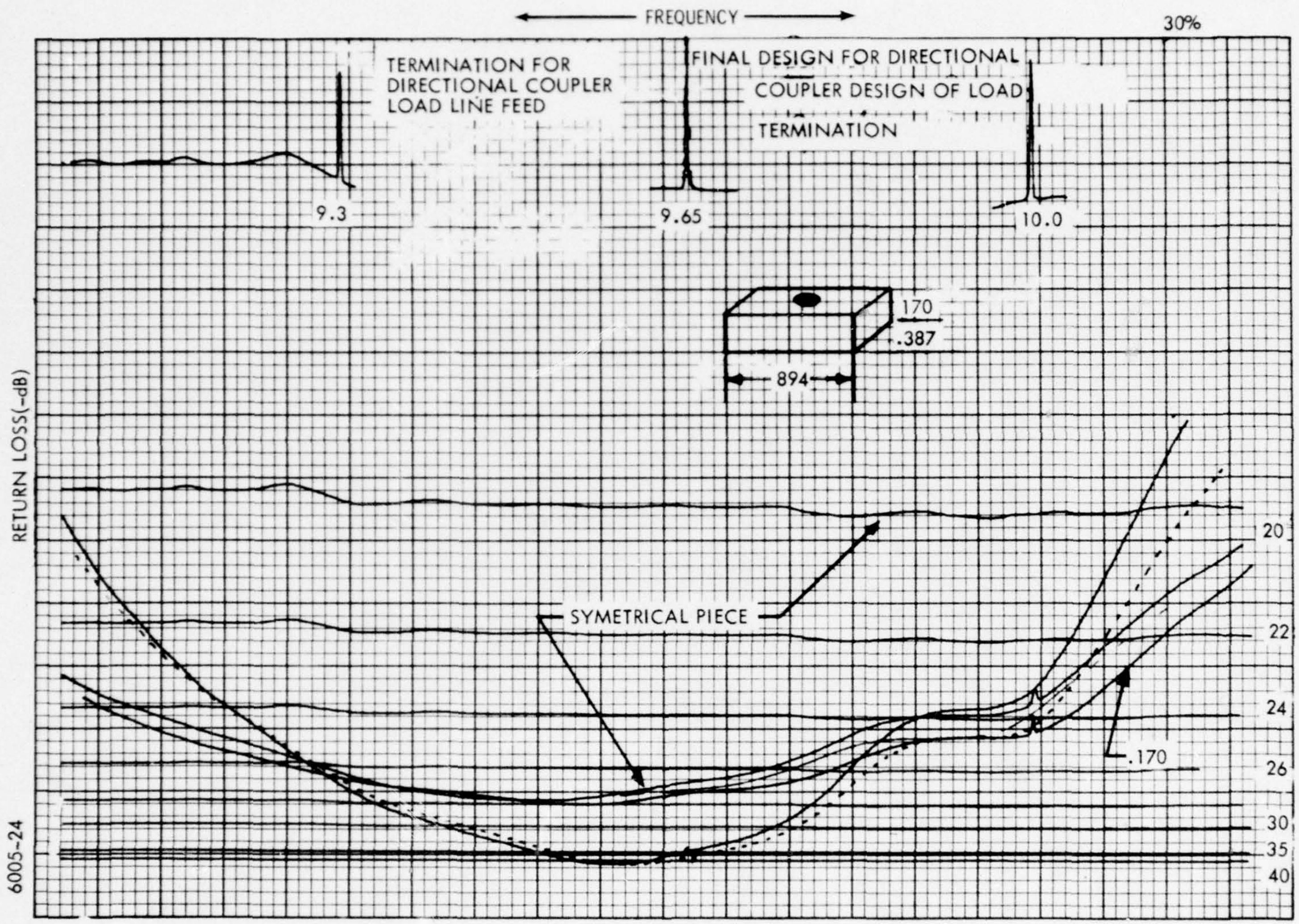


Figure 25. Load: Vertical Feed Coupler VSWR Plot

2.4.2 Phase Randomization Blocks. - Phase randomization blocks are used in the beam scanning path to reduce the degree of phase quantization effect which may occur with digital phase shifters producing relatively large phase shift increments.

The method of overcoming the possible occurrence of phase quantization effects in the ARBAT antenna is through the installation of a dielectric material block in each 90 degree twist section. The blocks are fabricated from Rexolite material in a single width ($\frac{.390}{.400}$ inch) and six lengths (0.216; 0.207; 0.170; 0.709; 0.722; and 0.769 inch). The phase randomization blocks are installed in the narrow dimensions of each twist section at the end adjacent to the phase shifter. Each block is held in place by a single screw and epoxy adhesive. The position of the block in the 90 degree twist section is shown in Figure 26. The configuration and dimensions for the series of blocks is shown in Figure 27.

Phase Randomization Block Tests. - The parameters of significance in the phase randomization block design are insertion phase over the radar bandwidth and return loss over the operating frequency range. The results of tests using samples of each block configuration are shown in Figure 28, Phase Randomization Block Insertion Phase vs Frequency and Figure 29, Phase Randomization Block Return Loss vs Frequency

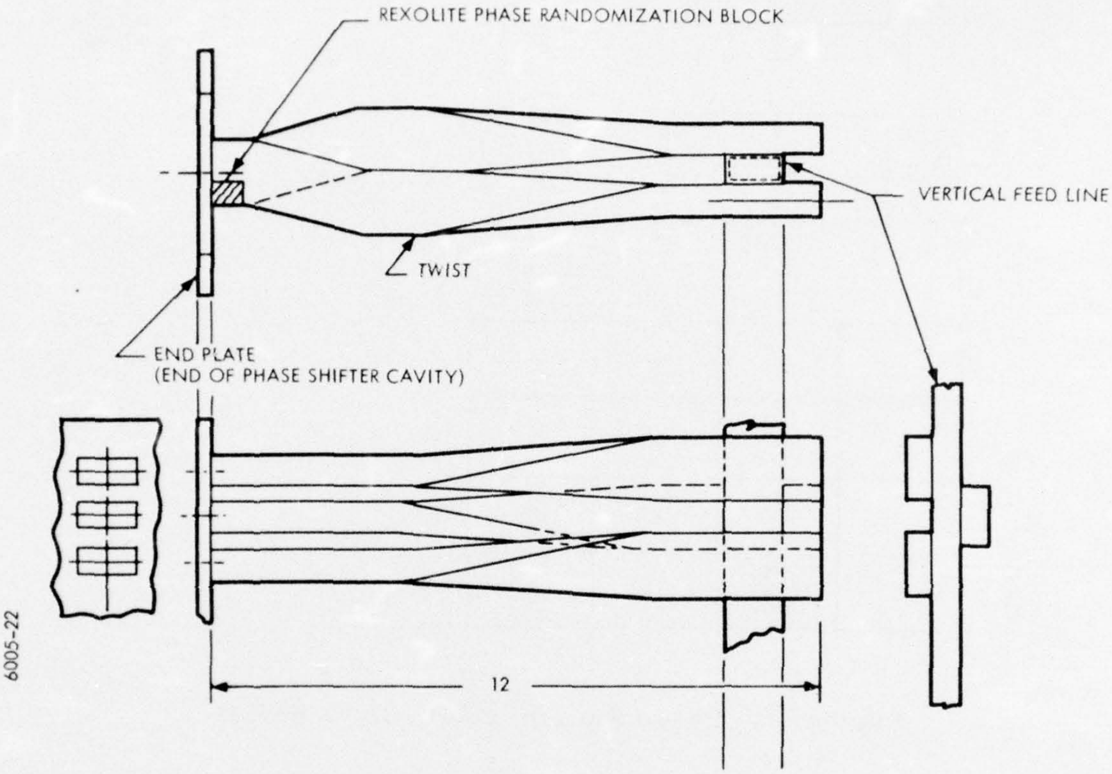
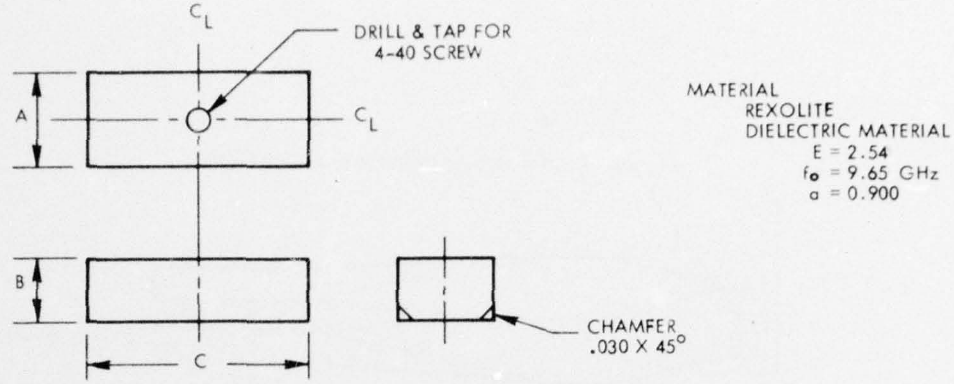


Figure 26. Phase Randomization Block Location in Coupler



DASH	A	B	C	
-1	.390 / .400	.216	.709	BLK
-2	.390 / .400	.207	.722	BLUE
-3	.390 / .400	.170	.769	GR

6005-25

Figure 27. Phase Randomization Block Series

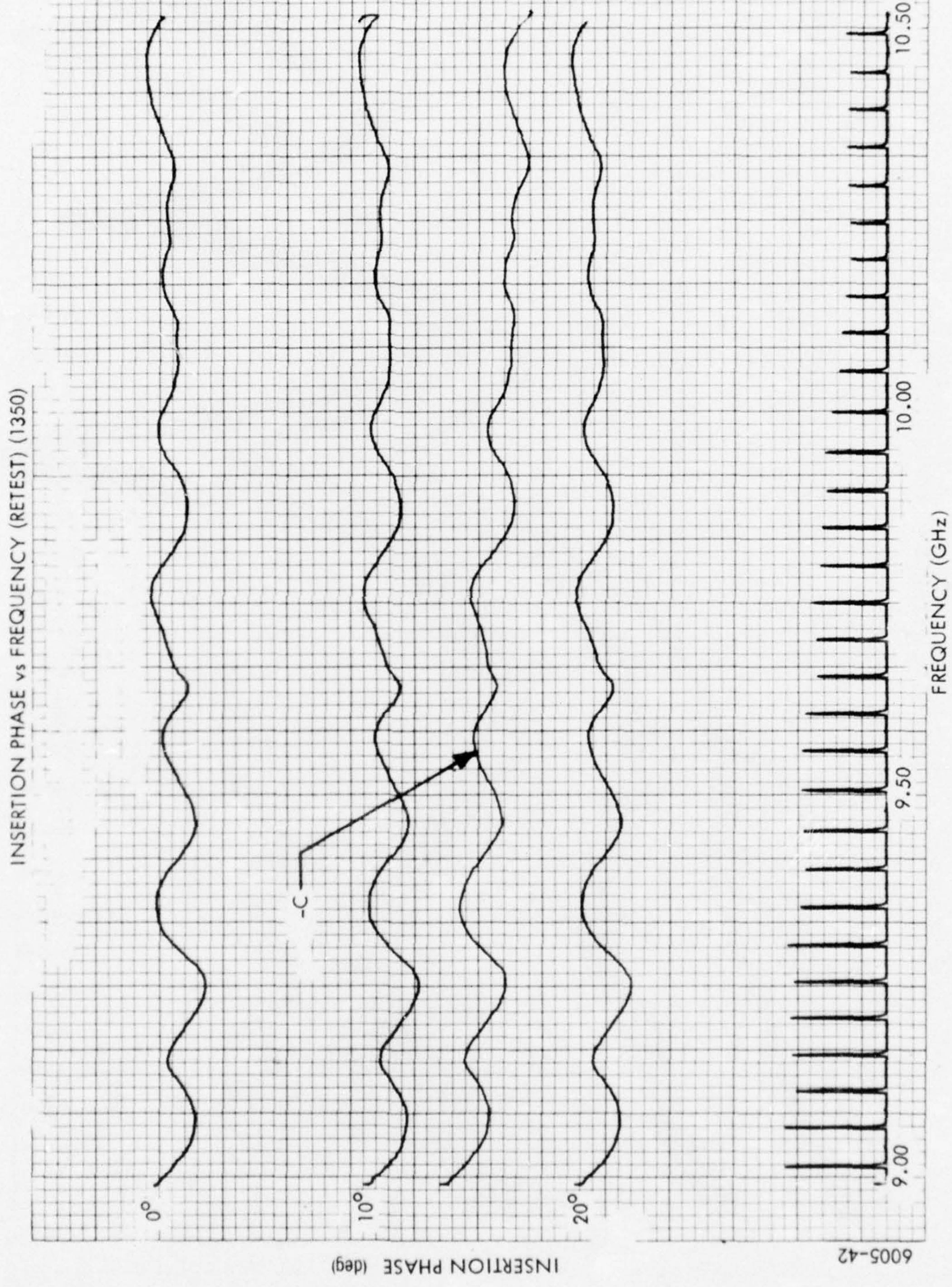


Figure 28. Phase Randomization Block

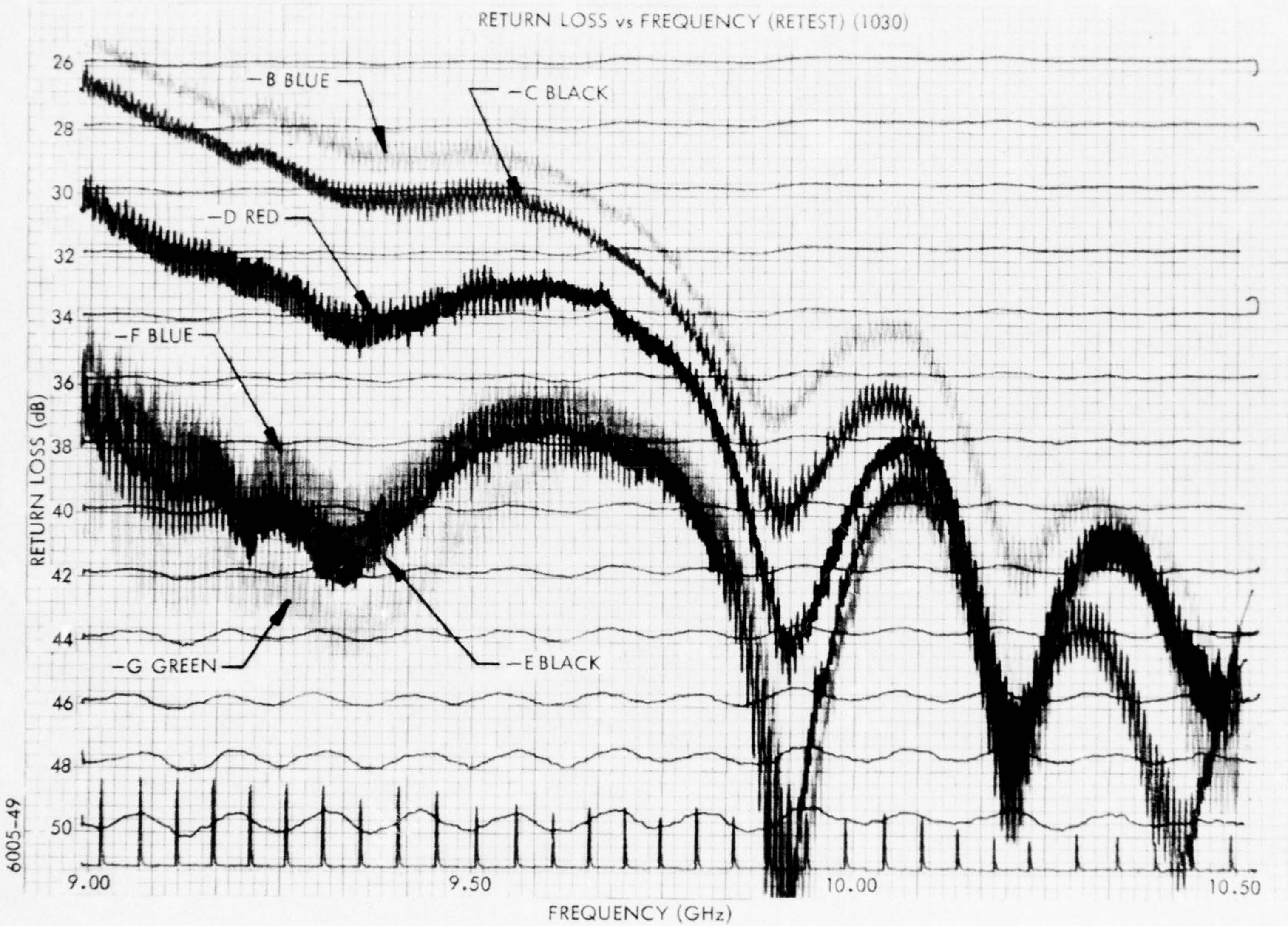


Figure 29. Phase Randomization Block

2.5 Diode Phase Shifter

The ARBAT antenna uses digitally controlled diode phase shifters to phase the energy radiated by the horizontal array elements in accordance with computer/software controlled logic. Phase shifter control in the ARBAT antenna permits control of the pencil beam over the range of ±35 degrees in elevation with respect to beam normal. The ARBAT antenna requires 167 phase shifters which have been supplied as Government Furnished Equipment.

The reciprocal phase shifters provide four-bit phase control over the range of 9300 to 10,000 MHz. A total of 16 phase states may be set by the logic control resulting in a phase state range of 0 to 337.5 degrees in 22.5 degree increments.

The phase shifter unit package includes a driver circuit and space for a logic decoding package. The input to each phase shifter package comes from a beam steering buffer unit. The control logic for the array (167 phase shifters) functions in a serial mode and, the decoding process is similar to signal progression through a long shift register. Each phase shifter contains two four-bit shift registers as shown in the block diagram of Figure 30. The four-bit command is clocked into the first register of phase shifter number 1 on the first shift command. A load signal transfers the four-bit command to the second register whose outputs drive the phase shifter assembly. A second shift command transfers the four-bit command to the first register of the second phase shifter where it is loaded by a load command.

The sequence described above is repeated from phase shifter to phase shifter with each decode logic assembly receiving data from the previous one (along with the bussed control commands). The output of the 167th logic assembly is fed back to the beam steering buffer for integrity verification.

The sampled output of each driver is then amplified and sent to built-in test equipment and compared to the phase-set command. A determination is made as to whether the phase shifter is receiving the correct command, and incorrect command, or if commands are reaching the unit.

The output voltages of the driver power supplies are also monitored. The outputs are compared with a predetermined reference voltage from a voltage regulator. If the output voltages vary by more than ±5 percent, an

"abnormal" condition is indicated. Phase shifter logic control organization is illustrated in Figure 30. Phase shifter position in relationship to the 90 degree twist waveguide section is shown in the assembled antenna in the photograph, Figure 31.

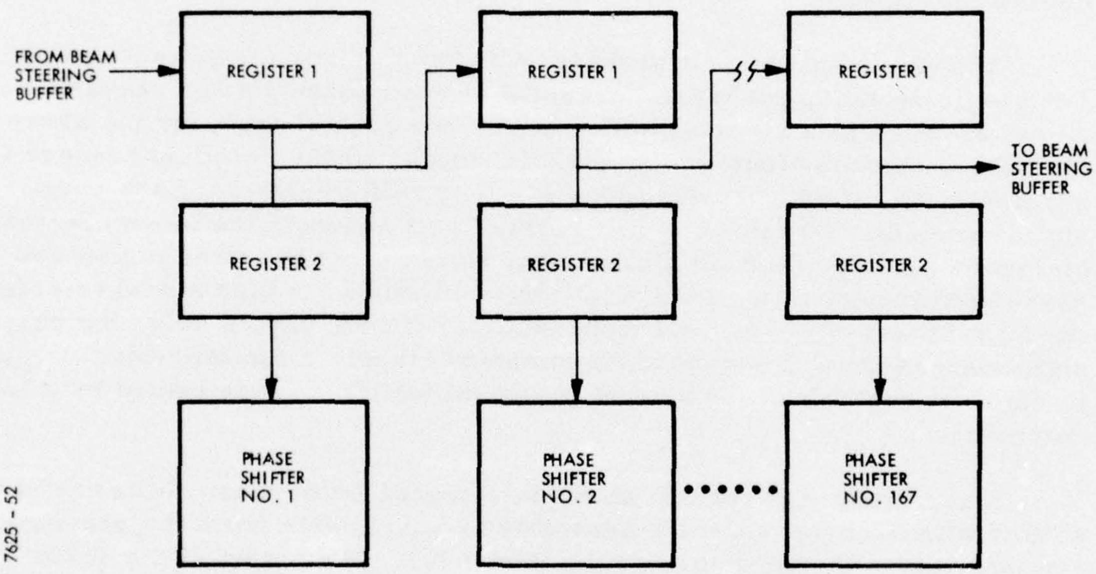


Figure 30. Phase Shifter Decode Logic Organization

Figure 31. Phase Shifter Position in Assembled Antenna

2.6 ARBAT Antenna Performance Monitor Concept

The purpose of the performance monitoring features incorporated into the ARBAT antenna design is to provide a dynamic checking capability on the operability and performance of the overall antenna subsystem. In addition to the latter basic function, the monitor capability facilitates the location of defective components or components operating in a degraded mode.

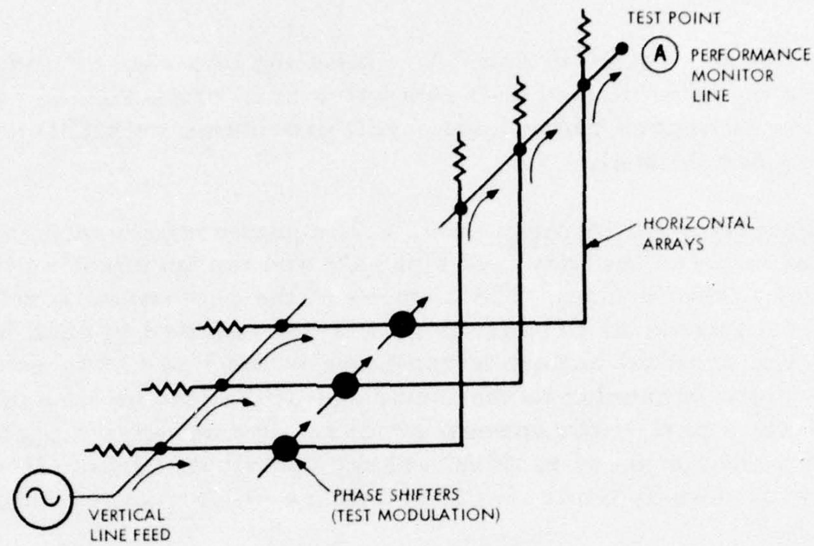
The performance monitoring function in the ARBAT antenna is accomplished by the inclusion of the performance monitor line and monitor line couplers described in the following section (2.6.1). The additional components required to monitor the signal detected at the output of the vertical monitor line are not parts of the antenna and are not described in this report.

In operation, overall general antenna performance may be ascertained by observing the pattern presentation on a monitor display. If the observed display is abnormal indicating degraded performance, a special diagnostic routine generated by the CPU may be initiated which supplies logic commands to the phase shifter control circuitry. By means of these diagnostic commands, the cause of the abnormal display may be localized to the individual horizontal array element and/or phase shifter in the individual array section that is responsible for the indication.

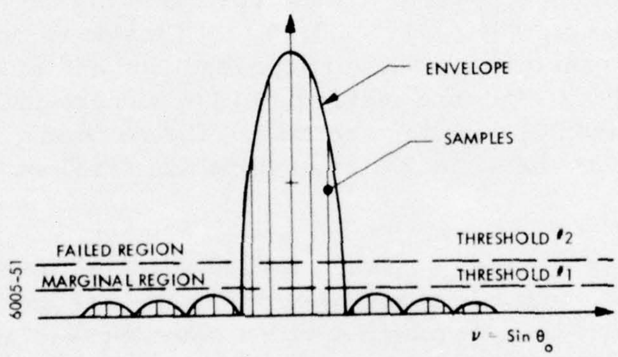
The sketches in Figure 32 (Performance Monitoring Concept) illustrate the fault detection process.

Point A of the antenna fault detection approach schematic is the location of a single ended mixer. At this point, a signal from a good antenna would be similar to the second illustration when the phase shifters are programmed through a standard scan. If the antenna has component failures affecting the elevation pattern, overall system performance will be degraded, and the sidelobe pattern will be distorted as in the third figure.

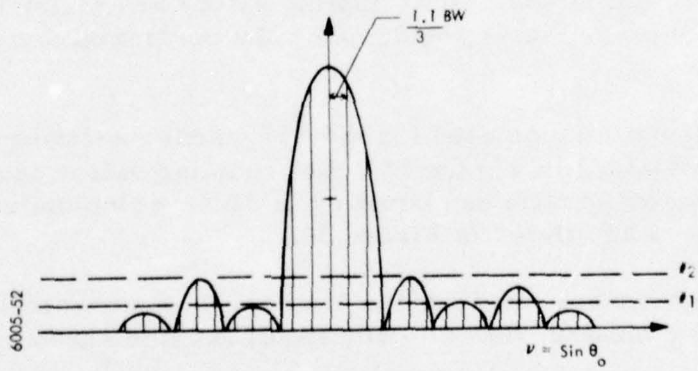
To localize the particular waveguide/phase shifter element, each phase shifter may be separately cycled linearly in phase. In a good system the amplitude waveform at point A will go through a negative zero crossing as the phase is cycled through the 90 degree phase shifter point.



Fault Detection Approach Schematic



Monitored Signal for Antenna without Failures



Monitored Signal for Antenna with Failures

Figure 32. Performance Monitoring Concept

A circuit coupled to point A, consisting of a gate seeking coincidence between a pulse generated at the negative zero crossing and another generated at the 90 degree phase instant,will provide an output if the element conditions are normal.

2.6.1 Performance Monitor Line. - The performance monitor line is connected between the last dual slot pair and the terminating load in each horizontal array section. The purpose of the performance monitor line is to collect the residual RF energy that is not radiated in each horizontal array. The residual energy is combined in the line and is detected by a diode detector connected to the lower end of the line by a coaxial line which is not a part of the antenna proper. The detected signal resulting from the combination of residual energy contributed from all elements is used to provide a dynamic check on antenna performance/status during operation.

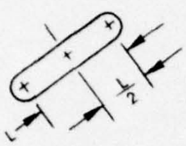
The performance monitor line is fabricated in three separate sections using precision waveguide (0.400 x 0.900 inch inside dimension by 0.500 x 1.000 outside dimension) for the vertical feed line and smaller precision waveguide (0.400 x 0.750 inch inside by 0.476 x 0.826 inch outside dimension) for the horizontal coupling sections. The couplers, as will be noted are fabricated from the same material (type and size) as the horizontal array elements.

The coupling sections contain a milled nondirectional four port slot which couples the short horizontal sections to the vertical monitor line. Each coupling section is terminated with a matched loading block. The coupling coefficients of the sections are adjusted carefully to match the Taylor excitation generated by the vertical feed line. The coupling value is a function of slot length. The coupling values are maintained low in view of the low energy level required for the performance monitoring function.

The slot dimensions used for the 167 coupler sections in the ARBAT antenna are contained in Figure 33. Slot coupling values in voltage amplitude, coupling power ratio and coupling in dB on which the slot configurations were based are listed in Figure 34.

The performance monitor line is shown in the assembled antenna in Figure 35 and a closeup view of a section of the line shows mounting details (Figure 36).

SLOT WIDTH = 0.062 +.002
FREQUENCY= 9.65000GHZ
A DIMENSION = 0.90000 IN.
B DIMENSION = 0.40000 IN.
POWER INTO LOAD = 0.60000 (
LENGTH OF SLOT IS GIVEN AS 1/2 LENGTH



1	0.15634	43	0.15936	85	0.16267	127	0.16636
2	0.15641	44	0.15943	86	0.16275	128 40	0.16645
3	0.15648	45	0.15951	87	0.16283	129	0.16654
4	0.15655	46	0.15958	88 80	0.16292	130	0.16664
5	0.15662	47	0.15966	89	0.16300	131	0.16673
6	0.15669	48	0.15973	90	0.16309	132	0.16683
7	0.15676	49	0.15981	91	0.16317	133	0.16692
8	0.15683	50	0.15988	92	0.16325	134	0.16702
9	0.15689	51	0.15996	93	0.16334	135	0.16711
10	0.15696	52	0.16004	94	0.16342	136	0.16721
11	0.15703	53	0.16011	95	0.16351	137	0.16730
12	0.15711	54	0.16019	96	0.16359	138 30	0.16740
13	0.15718	55 113	0.16027	97	0.16368	139	0.16749
14	0.15725	56	0.16035	98 70	0.16377	140	0.16759
15	0.15732	57	0.16042	99	0.16385	141	0.16769
16	0.15739	58 110	0.16050	100	0.16394	142	0.16778
17	0.15746	59	0.16058	101 67	0.16402	143	0.16788
18	0.15753	60	0.16066	102	0.16411	144 24	0.16798
19	0.15760	61	0.16073	103	0.16420	145	0.16808
20	0.15767	62	0.16081	104	0.16428	146	0.16818
21	0.15774	63	0.16089	105	0.16437	147	0.16827
22	0.15781	64	0.16097	106	0.16446	148 20	0.16837
23	0.15789	65	0.16105	107	0.16455	149	0.16847
24	0.15796	66	0.16113	108 60	0.16464	150	0.16857
25	0.15803	67	0.16121	109	0.16472	151	0.16867
26	0.15810	68 100	0.16129	110	0.16481	152	0.16877
27	0.15817	69	0.16137	111	0.16490	153	0.16887 .399
28	0.15825	70	0.16145	112	0.16499	154	0.16897
29	0.15832	71	0.16153	113	0.16508	155	0.16908
30	0.15839	72	0.16161	114	0.16517	156	0.16918
31	0.15847	73	0.16169	115	0.16526	157	0.16928
32	0.15854	74	0.16177	116	0.16535	158 10	0.16938
33	0.15861	75	0.16185	117	0.16544	159	0.16948
34	0.15869	76	0.16193	118 50	0.16553	160	0.16959
35	0.15876	77 91	0.16201	119	0.16562	161	0.16969
36	0.15883	78 90	0.16209	120	0.16571	162	0.16979
37	0.15891	79	0.16217	121	0.16580	163	0.16990
38	0.15898	80	0.16226	122	0.16589	164	0.17000
39	0.15906	81	0.16234	123 —	0.16599	165	0.17011
40	0.15913	82	0.16242	124	0.16608	166	0.17021
41	0.15921	83	0.16250	125	0.16617	167 1	0.17032 .402
42	0.15928	84	0.16259	126	0.16626		

.374

0.382
92 THRU 112

0.386
68 THRU 91

0.390
46 THRU 67

0.394
25 THRU 45

1 THRU 24

FREQUENCY = 9.65000 GHZ
W.G. A DIMENSION= 0.90000IN
W.G. B DIMENSION= 0.40000IN
ELEMENT SPACING= 0.72000IN
TE MODE(N,M) = 1.00000 0.00000
WAVEGUIDE LOSSES = 0.00255 DB

6005-47

Figure 33. Performance Monitor Slot Dimensions

ELEMENTS =167.
FREQ = 9.65000
A = 0.90000
B = 0.40000
SPACE = 0.72000
SERPENTINE SPACING = 0.00000
POWER INTO LOAD = 0.60000
WAVEGUIDE LOSSES = 0.00000
TOTAL LOSSES = 0.67023

	AMPLITUDE (V)	C (PWR RATIO)	C(dB)								
1	0.04389	0.00192	-27.14919	57	0.04389	0.00223	-26.50159	113	0.04389	0.00265	-25.76705
2	0.04389	0.00193	-27.13825	58	0.04389	0.00224	-26.48931	114	0.04389	0.00265	-25.75297
3	0.04389	0.00193	-27.12730	59	0.04389	0.00225	-26.47700	115	0.04389	0.00266	-25.73886
4	0.04389	0.00194	-27.11633	60	0.04389	0.00225	-26.46466	116	0.04389	0.00267	-25.72471
5	0.04389	0.00194	-27.10533	61	0.04389	0.00226	-26.45230	117	0.04389	0.00268	-25.71052
6	0.04389	0.00195	-27.09432	62	0.04389	0.00226	-26.43991	118	0.04389	0.00269	-25.69629
7	0.04389	0.00195	-27.08328	63	0.04389	0.00227	-26.42749	119	0.04389	0.00270	-25.68203
8	0.04389	0.00196	-27.07222	64	0.04389	0.00228	-26.41504	120	0.04389	0.00271	-25.66772
9	0.04389	0.00196	-27.06114	65	0.04389	0.00228	-26.40256	121	0.04389	0.00272	-25.65338
10	0.04389	0.00197	-27.05004	66	0.04389	0.00229	-26.39006	122	0.04389	0.00272	-25.63900
11	0.04389	0.00197	-27.03891	67	0.04389	0.00230	-26.37752	123	0.04389	0.00273	-25.62458
12	0.04389	0.00198	-27.02776	68	0.04389	0.00230	-26.36496	124	0.04389	0.00274	-25.61011
13	0.04389	0.00198	-27.01659	69	0.04389	0.00231	-26.35237	125	0.04389	0.00275	-25.59561
14	0.04389	0.00199	-27.00540	70	0.04389	0.00232	-26.33975	126	0.04389	0.00276	-25.58107
15	0.04389	0.00199	-26.99419	71	0.04389	0.00232	-26.32710	127	0.04389	0.00277	-25.56649
16	0.04389	0.00200	-26.98295	72	0.04389	0.00233	-26.31442	128	0.04389	0.00278	-25.55187
17	0.04389	0.00200	-26.97169	73	0.04389	0.00234	-26.30171	129	0.04389	0.00279	-25.53721
18	0.04389	0.00201	-26.96041	74	0.04389	0.00235	-26.28897	130	0.04389	0.00280	-25.52251
19	0.04389	0.00201	-26.94911	75	0.04389	0.00235	-26.27620	131	0.04389	0.00281	-25.50776
20	0.04389	0.00202	-26.93778	76	0.04389	0.00236	-26.26340	132	0.04389	0.00282	-25.49297
21	0.04389	0.00202	-26.92643	77	0.04389	0.00237	-26.25057	133	0.04389	0.00283	-25.47814
22	0.04389	0.00203	-26.91506	78	0.04389	0.00237	-26.23771	134	0.04389	0.00284	-25.46327
23	0.04389	0.00204	-26.90366	79	0.04389	0.00238	-26.22482	135	0.04389	0.00285	-25.44836
24	0.04389	0.00204	-26.89224	80	0.04389	0.00239	-26.21189	136	0.04389	0.00286	-25.43341
25	0.04389	0.00205	-26.88080	81	0.04389	0.00239	-26.19894	137	0.04389	0.00287	-25.41841
26	0.04389	0.00205	-26.86933	82	0.04389	0.00240	-26.18596	138	0.04389	0.00288	-25.40337
27	0.04389	0.00206	-26.85784	83	0.04389	0.00241	-26.17294	139	0.04389	0.00289	-25.38828
28	0.04389	0.00206	-26.84633	84	0.04389	0.00242	-26.15990	140	0.04389	0.00290	-25.37316
29	0.04389	0.00207	-26.83479	85	0.04389	0.00242	-26.14682	141	0.04389	0.00291	-25.35798
30	0.04389	0.00207	-26.82323	86	0.04389	0.00243	-26.13371	142	0.04389	0.00292	-25.34277
31	0.04389	0.00208	-26.81164	87	0.04389	0.00244	-26.12057	143	0.04389	0.00293	-25.32751
32	0.04389	0.00208	-26.80003	88	0.04389	0.00245	-26.10739	144	0.04389	0.00294	-25.31220
33	0.04389	0.00209	-26.78840	89	0.04389	0.00245	-26.09419	145	0.04389	0.00295	-25.29685
34	0.04389	0.00210	-26.77674	90	0.04389	0.00246	-26.08095	146	0.04389	0.00296	-25.28145
35	0.04389	0.00210	-26.76506	91	0.04389	0.00247	-26.06768	147	0.04389	0.00297	-25.26601
36	0.04389	0.00211	-26.75335	92	0.04389	0.00248	-26.05437	148	0.04389	0.00298	-25.25053
37	0.04389	0.00211	-26.74162	93	0.04389	0.00248	-26.04103	149	0.04389	0.00299	-25.23499
38	0.04389	0.00212	-26.72986	94	0.04389	0.00249	-26.02766	150	0.04389	0.00300	-25.21941
39	0.04389	0.00212	-26.71808	95	0.04389	0.00250	-26.01426	151	0.04389	0.00301	-25.20378
40	0.04389	0.00213	-26.70627	96	0.04389	0.00251	-26.00082	152	0.04389	0.00302	-25.18811
41	0.04389	0.00214	-26.69444	97	0.04389	0.00251	-25.98735	153	0.04389	0.00303	-25.17239
42	0.04389	0.00214	-26.68258	98	0.04389	0.00252	-25.97385	154	0.04389	0.00305	-25.15662
43	0.04389	0.00215	-26.67070	99	0.04389	0.00253	-25.96030	155	0.04389	0.00306	-25.14080
44	0.04389	0.00215	-26.65879	100	0.04389	0.00254	-25.94673	156	0.04389	0.00307	-25.12493
45	0.04389	0.00216	-26.64686	101	0.04389	0.00255	-25.93312	157	0.04389	0.00308	-25.10902
46	0.04389	0.00217	-26.63490	102	0.04389	0.00255	-25.91948	158	0.04389	0.00309	-25.09305
47	0.04389	0.00217	-26.62291	103	0.04389	0.00256	-25.90580	159	0.04389	0.00310	-25.07704
48	0.04389	0.00218	-26.61090	104	0.04389	0.00257	-25.89208	160	0.04389	0.00311	-25.06097
49	0.04389	0.00218	-26.59886	105	0.04389	0.00258	-25.87834	161	0.04389	0.00312	-25.04486
50	0.04389	0.00219	-26.58679	106	0.04389	0.00259	-25.86455	162	0.04389	0.00314	-25.02869
51	0.04389	0.00220	-26.57470	107	0.04389	0.00259	-25.85073	163	0.04389	0.00315	-25.01248
52	0.04389	0.00220	-26.56259	108	0.04389	0.00260	-25.83688	164	0.04389	0.00316	-24.99621
53	0.04389	0.00221	-26.55044	109	0.04389	0.00261	-25.82299	165	0.04389	0.00317	-24.97989
54	0.04389	0.00221	-26.53827	110	0.04389	0.00262	-25.80906	166	0.04389	0.00318	-24.96352
55	0.04389	0.00222	-26.52607	111	0.04389	0.00263	-25.79509	167	0.04389	0.00320	-24.94710
56	0.04389	0.00223	-26.51384	112	0.04389	0.00264	-25.78109				

1 - 24	.399
25 - 45	0.394 (.393 - .395)
46 - 67	.390 (.389 TO .391)
68 to 91	.386 (.385 - 387)
92 - 112	.382

6005-48

Figure 34. Slot Coupling Values

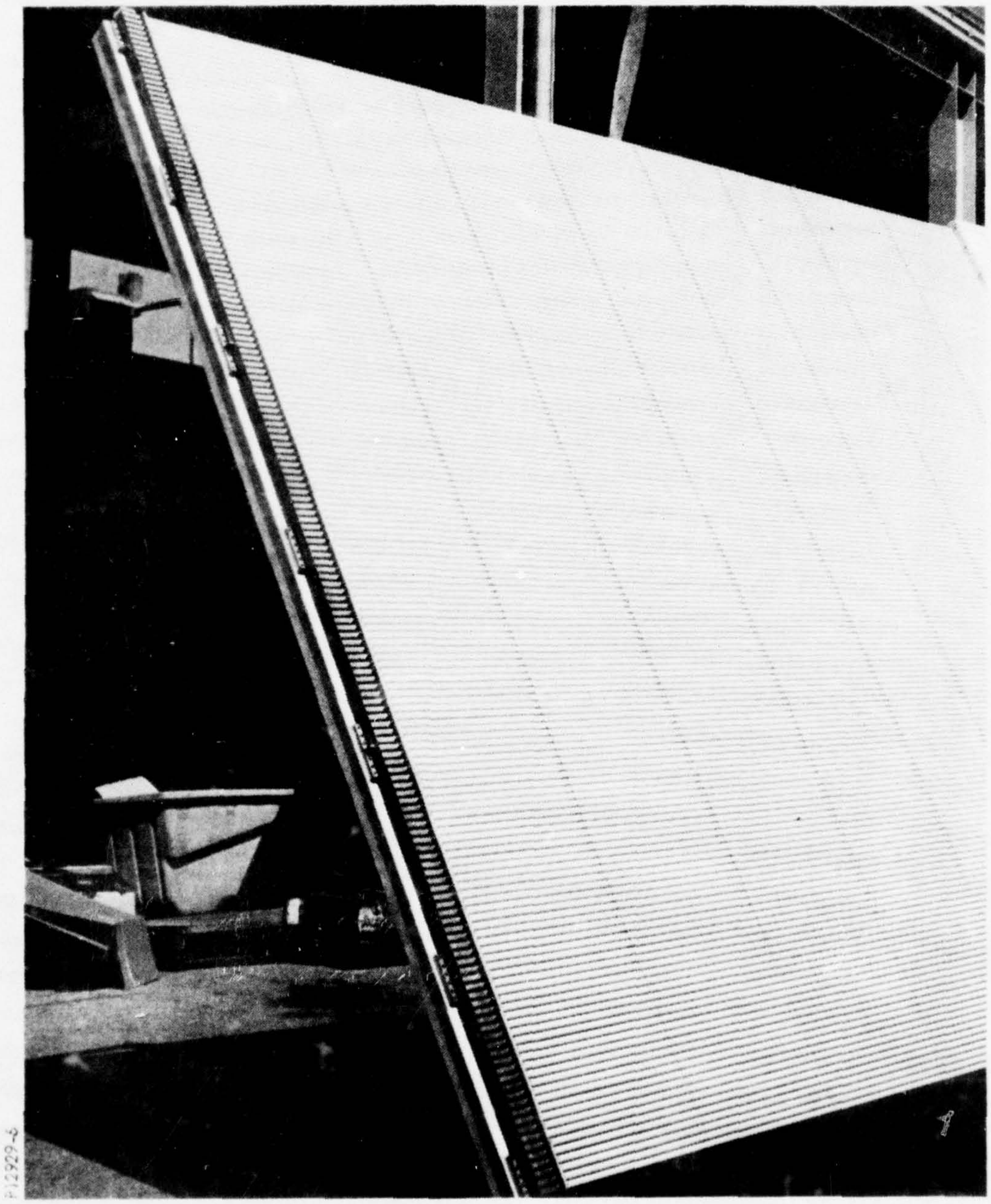


Figure 35. Performance Monitor Line in Assembled Antenna

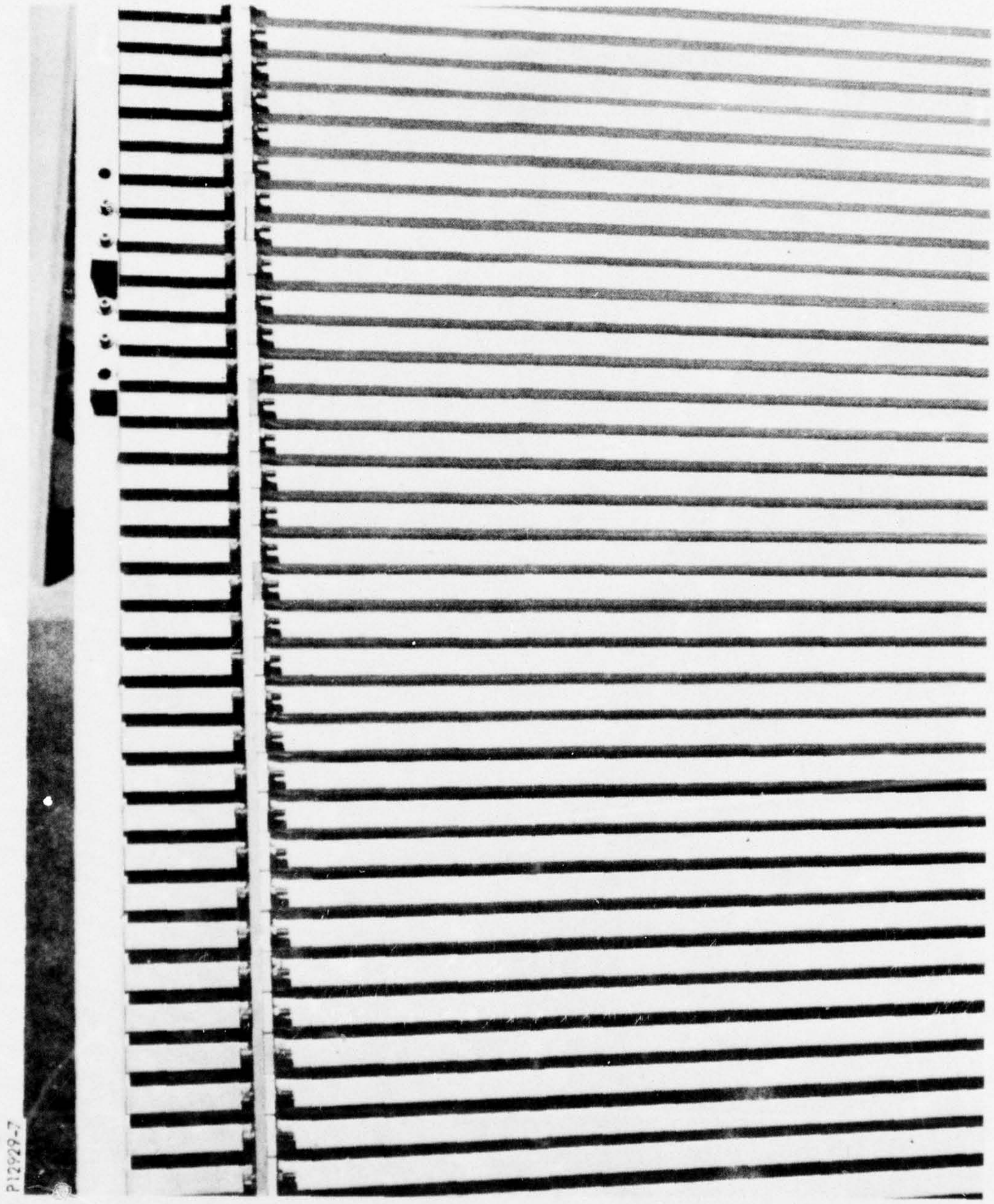


Figure 36. Performance Monitor Line (Close-Up View)

2.6.2 Loads: Performance Monitor Line. - Equalizing termination loads are required to terminate the horizontal array RF signal path, which in the ARBAT antenna is the extreme end of each coupling section attached to the performance monitor line. The performance monitor line loads are fabricated from material identical to that used for fabrication of the vertical line feed load elements, however the design and method of installation differs radically. These load elements are of uniform dimensions for all 167 elements. Oversize loads are molded from ECCOSORB 17 compound using an appropriate catalyst and milled to final dimensions. The load elements are chamfered at each edge of the surface contacting the wide dimension of the waveguide. In installation the load element is pressed into the waveguide together with a precut section of foam material the width of the load element and of a height to fully fill the space between the top of the element and the top inside wall of the waveguide above the load. The foam block holds the load firmly in place and epoxy adhesive is injected into the openings produced by the champfer at each corner of the waveguide.

For detailed design of the load element see Drawing 140325, Load, Monitor (available at Picatinny Arsenal).

Load Tests. - Tests to ascertain the return loss (VSWR) of the final load design were run throughout the antenna operating frequency range. Results of the tests are shown in Figure 37.

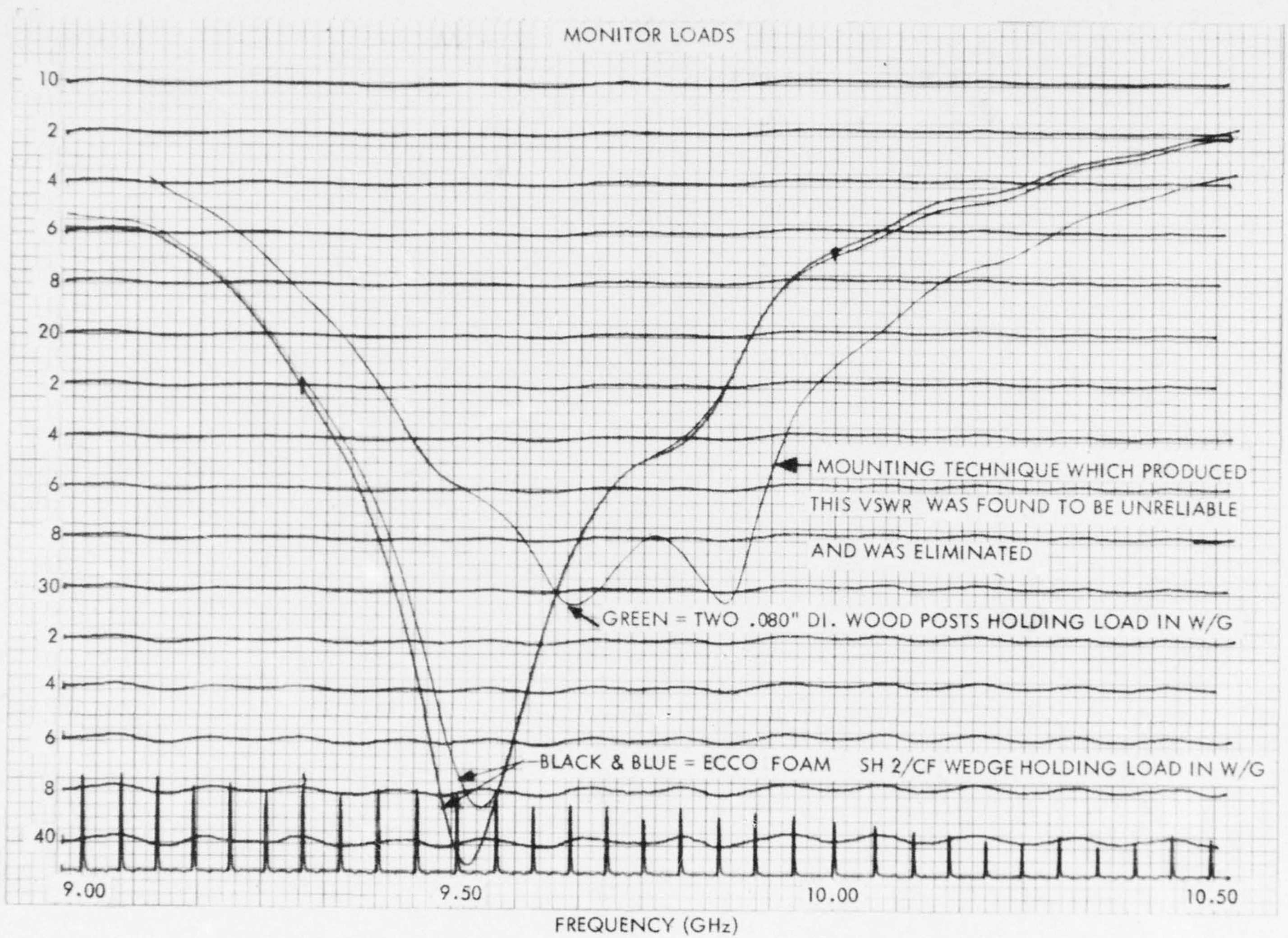


Figure 37. Load Block VSWR Measurement

3. TEST PROGRAM

Antenna Pattern Measurements

A major part of the ARBAT antenna development phase was the fabrication, testing, modification and retest of critical elements comprising the antenna subsystem. The procedure, which followed the paper design and computer analyses, was based on intermediate test results of single components followed by three* array range tests. On completion of these tests and after incorporation of changes determined necessary to optimize component design, a nine element test array was assembled using the optimized components. The nine element array configuration was selected as the minimum number of elements capable of producing patterns that reliably reflect the validity of the component designs, providing a confident prediction of the complete array performance.

3.1 Short Array (3 Section) Tests.

The 3 section array tests were made using a single excited horizontal array section between two "dummy" array sections positioned to provide a realistic environment for the active element. Short comb sections were used to maintain the relative positions of the three elements. The 3 section array was assembled and tested in the Van Nuys plant RF test chanber for insertion loss, VSWR (return loss) and phase error. The results of these tests are contained in the following figures. The last illustration is a computed pattern prediction based on the 3 element array phase and amplitude excitation measurements.

Figure 38. Horizontal Array Element Insertion Loss
Figure 39. Horizontal Array Element Return Loss
Figure 40. Horizontal Array Element Return Loss (Expanded D2 RL)
Figure 41. Predicted Pattern (3 Element Test)

---

*One Excited Array and Two Dummy Arrays

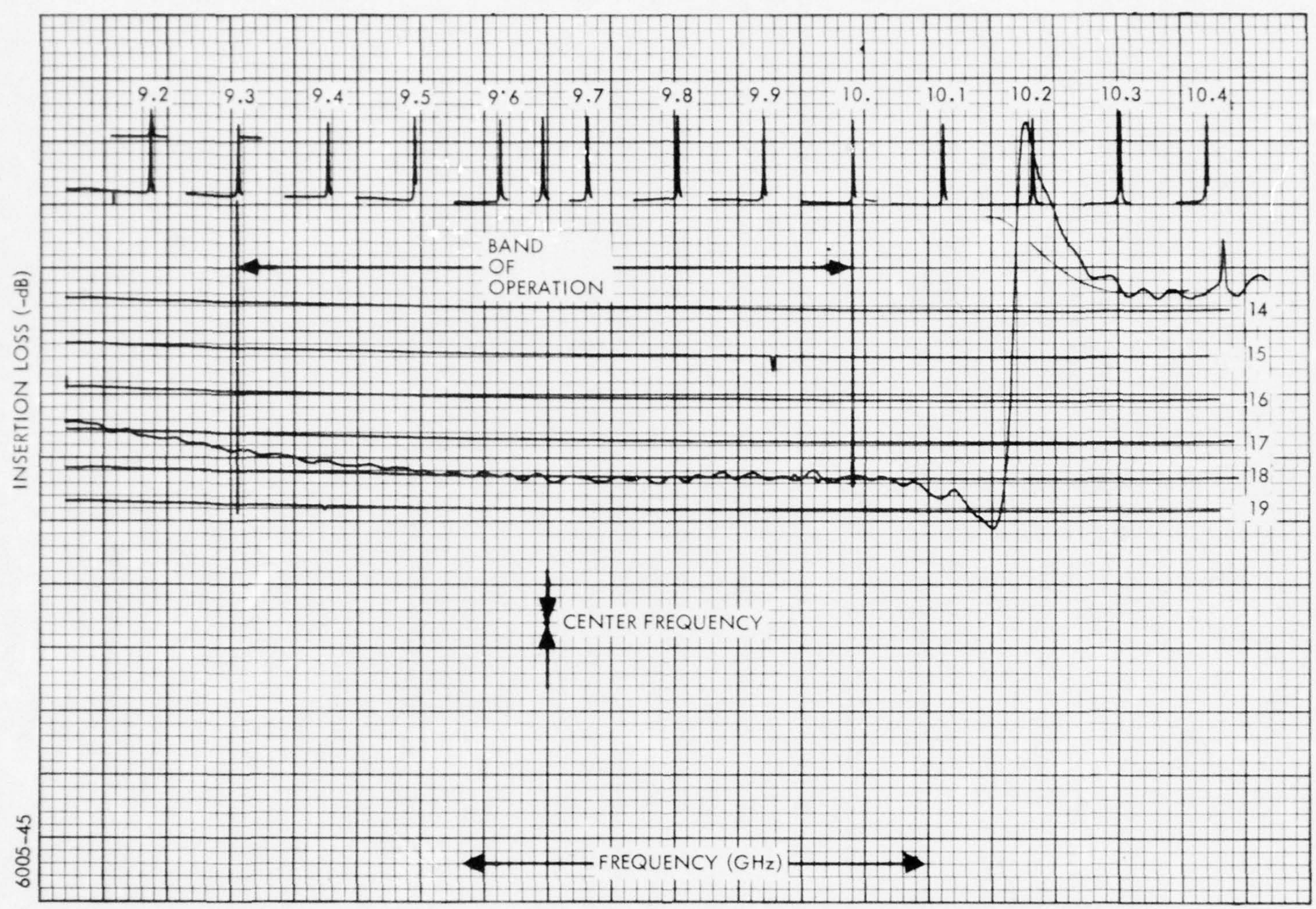


Figure 38. Horizontal Array Element Insertion Loss (Dual Slot Radiators)

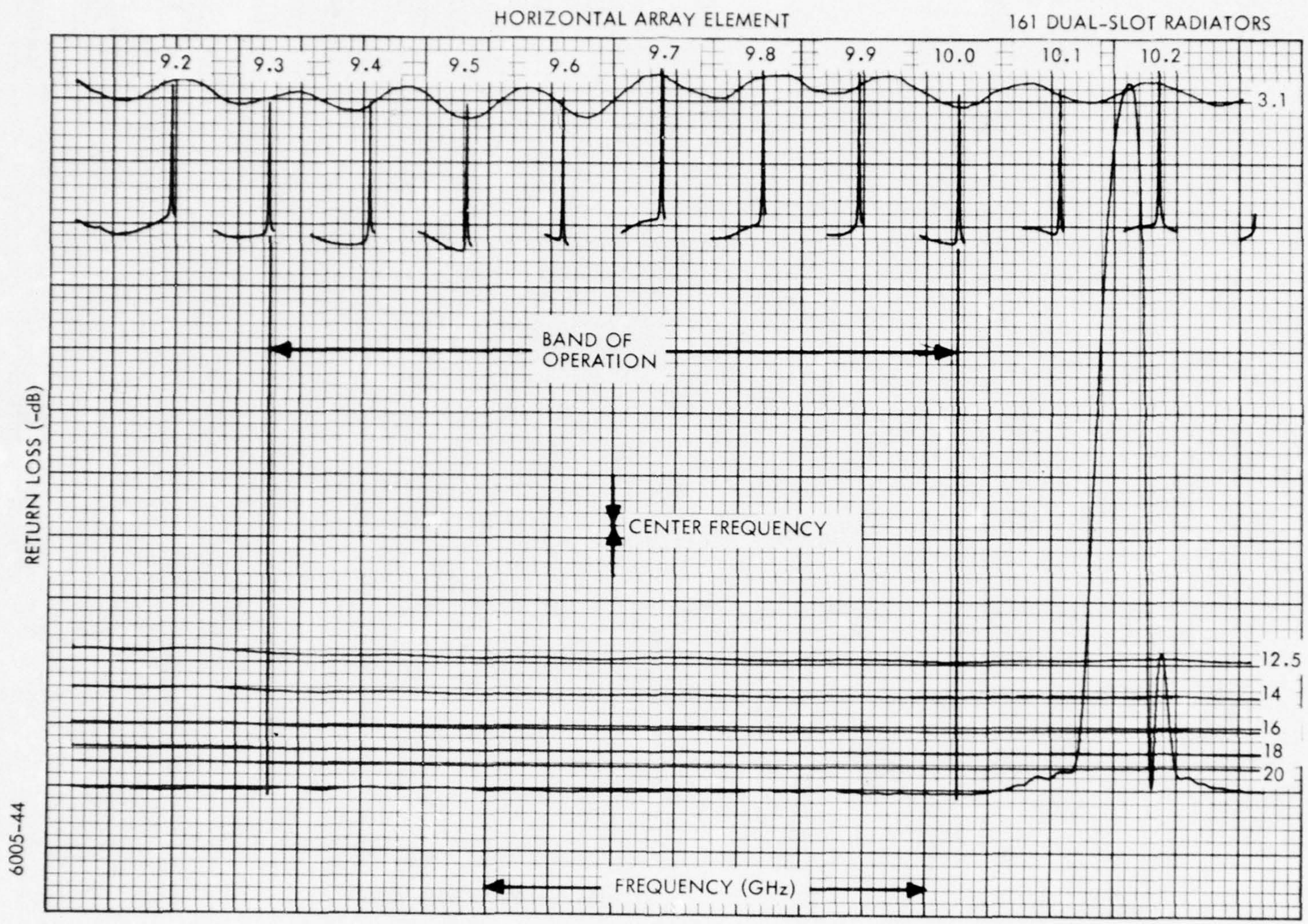


Figure 39. Horizontal Array Element Return Loss (Dual Slot Radiators)

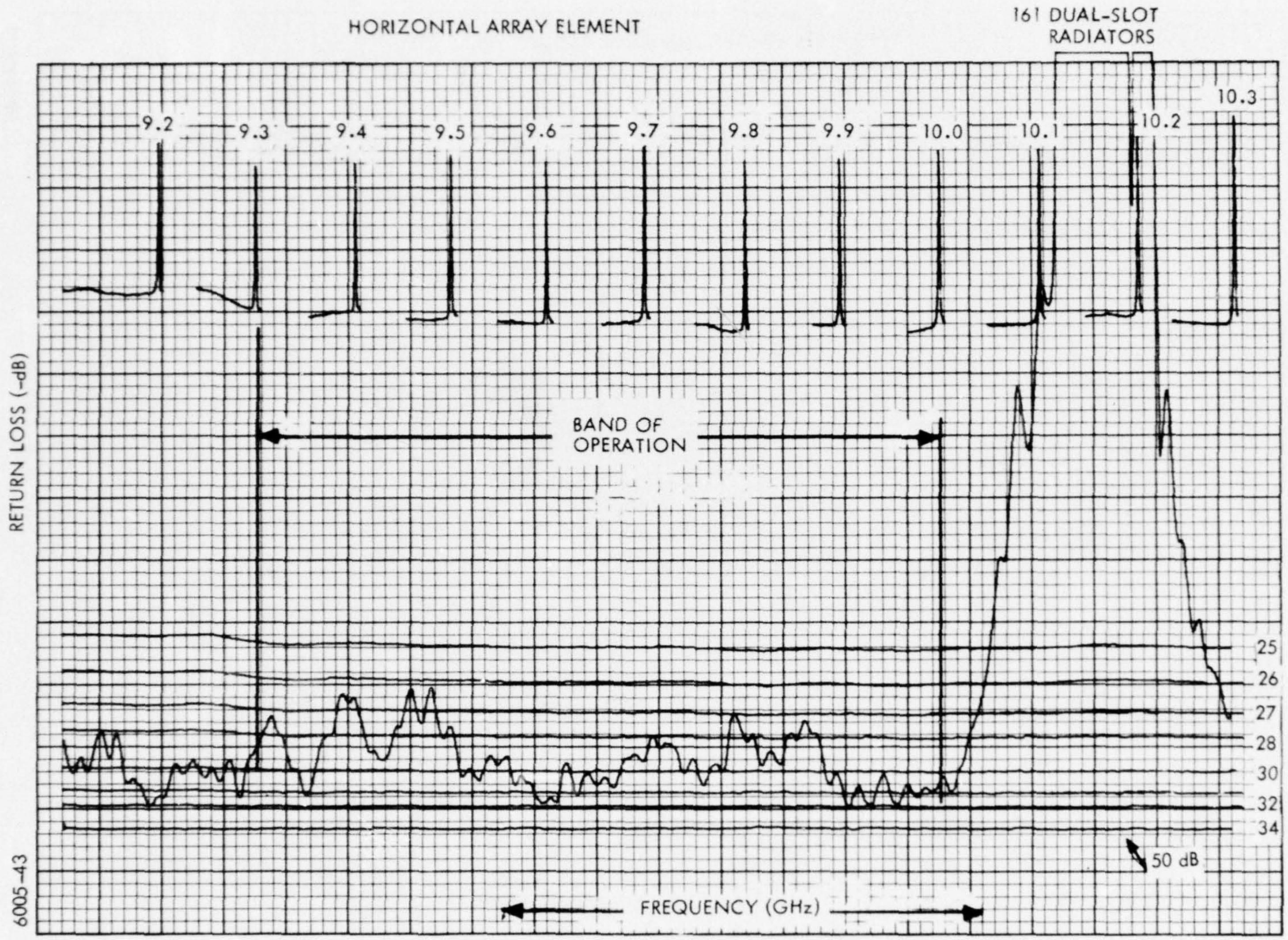


Figure 40. D-2 Horizontal Array Element Return Loss (Expanded D2 RL)

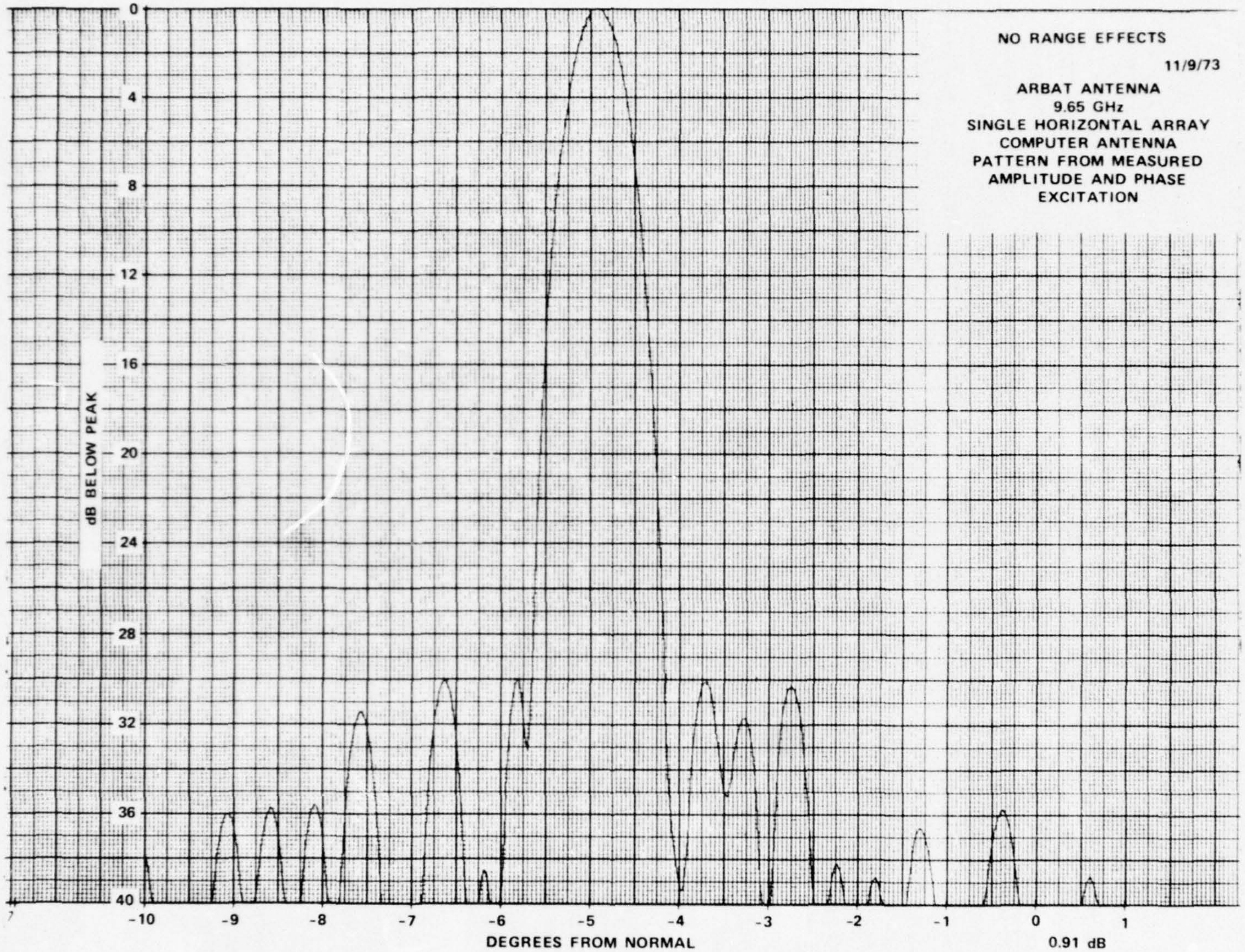


Figure 41. Predicted Pattern (3 Element Test)

3.2 Nine-Element Test Array

The nine-element range tests were designed to determine the validity of all previous tests and modifications resulting from intermediate single element testing and the three element tests in the preceding section. For the purpose of these tests it was necessary to introduce phase changes in each horizontal array input by means of small waveguide sections containing Rexolite phase shift blocks in lieu of the diode phase shifters which were not available. The phase shifting elements fabricated for these tests duplicate the electrical function of the phase shifters and insure that the results obtained are transferable to the same array if excited via the phase shifters which will be used in the operational system. Mechanically, the Rexolite block phase shift devices differed significantly from the actual diode phase shifter, as will be noted in the test array sketch, Figure 43, largely in that an "in-line" configuration was used in the test device assembly, whereas the diode phase shifters contain a 90 degree bend at the point at which the connection to the horizontal array is made. A quarter wave transformer was inserted between the phase shift test device and the horizontal array elements.

Horizontal array elements for the nine-element test array included one array element fabricated during the earlier tests in which a single array was tested singly and mounted between two "dummy" elements to form a three-array assembly. In order to provide a realistic electrical environment for the nine-element array, a "dummy" horizontal element was positioned on the outside of the first and last excited elements in the test assembly.

A short vertical feed line was fabricated for use with the test array assembly. The nine-element test array pictorial schematic is shown in Figure 42. The test array is shown mounted on a test fixture during range tests in Figure 43.

After alignment of the test array with the transmitting antenna, tests were conducted to determine elevation scan angles versus phase shift increments and azimuth patterns at beam normal, mid scan, and at scan limits. All tests were repeated at 9.3, 9.65 and 10.0 GHz.

3.2.1 Test Patterns

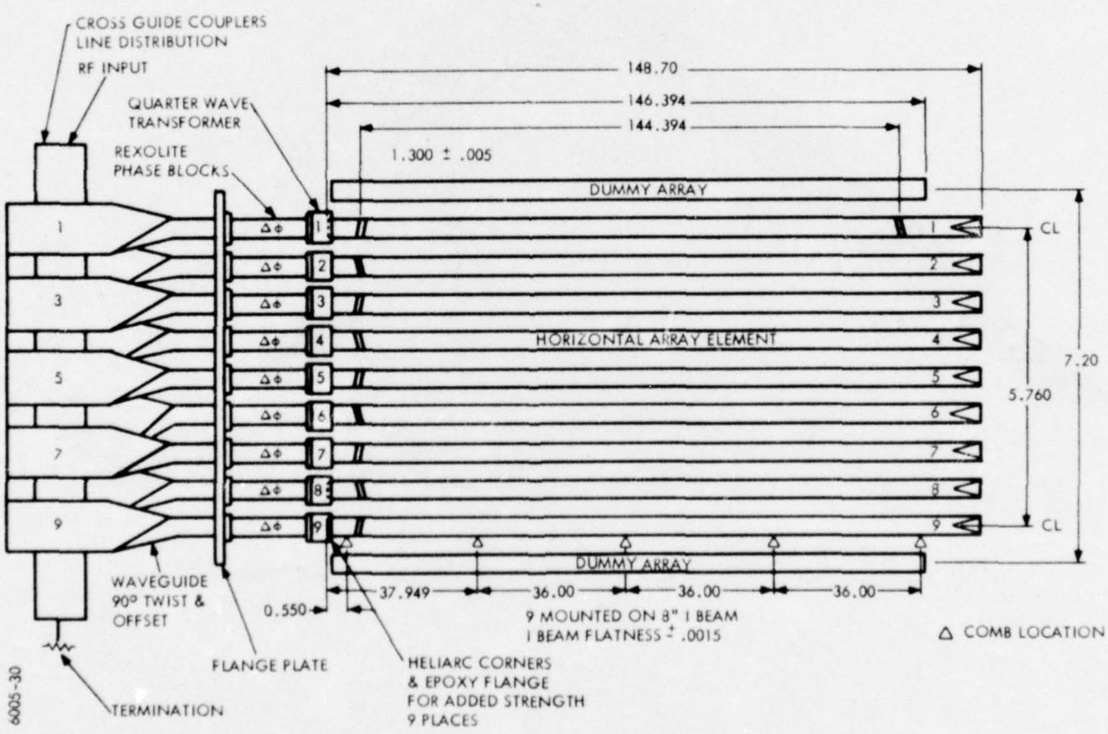
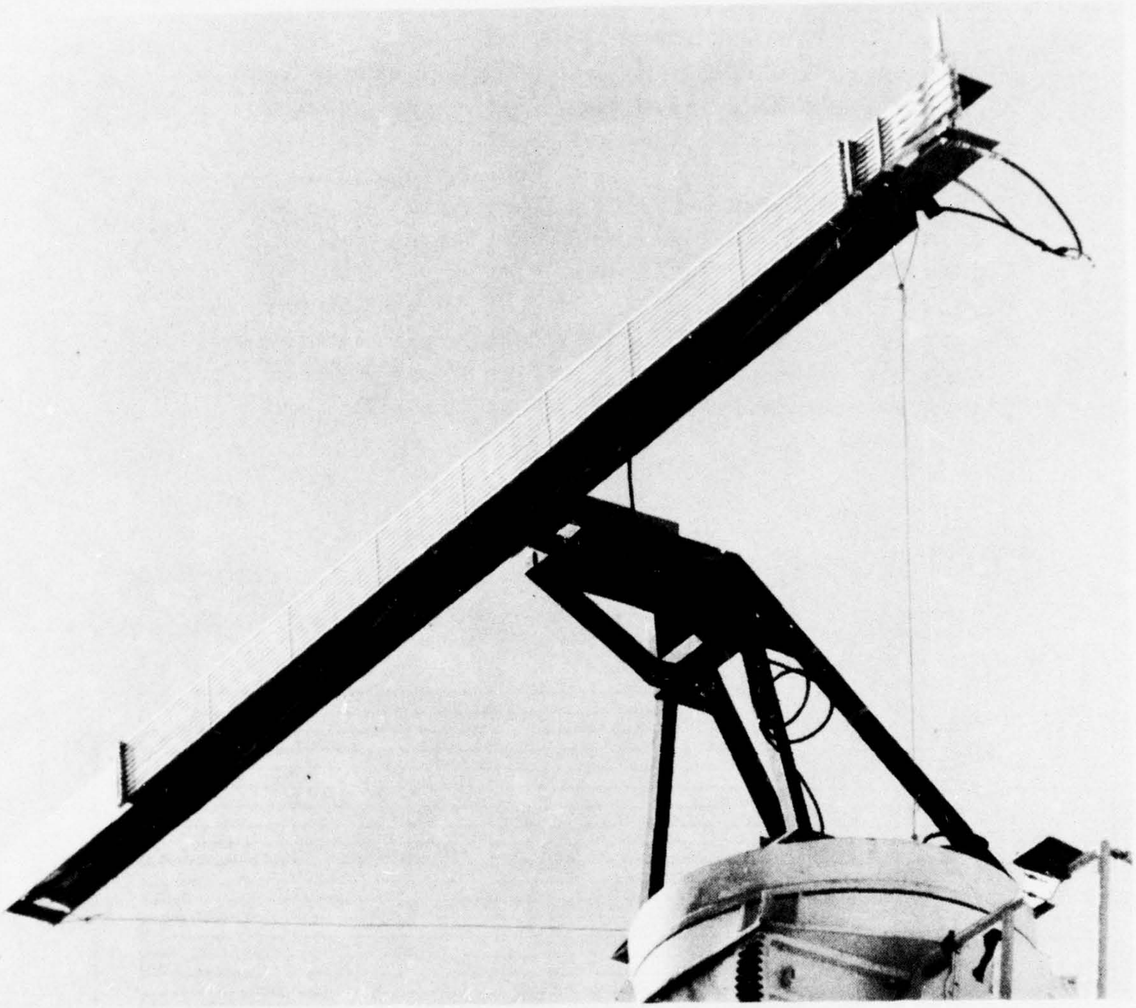


Figure 42. Nine-Element Test Array Assembly



P12663-9

Figure 43. Nine-Element Test Array Assembled

ITEM	SCAN ANGLE ELEVATION (DEG)	FREQ GHZ	Ø BLOCKS	
1	0.0	9.3	1. 0.0	6. 180
			2. 45	7. 225
			3. 67.5	8. 247.5
			4. 112.5	9. 292.5
			5. 135	
2	0.0	9.65	1. 0	6. 135
			2. 22.5	7. 157.5
			3. 45	8. 180
			4. 67.5	9. 202.5
			5. 90	
3	0.0	10.0	1. 0.0	6. 67.5
			2. 22.5	7. 90
			3. 22.5	8. 112.5
			4. 45	9. 112.5
			5. 67.5	
4	-17.5	9.3	1. 0	6. 225
			2. 337.5	7. 202.5
			3. 315	8. 180
			4. 292.5	9. 157.5
			5. 247.5	
5	-17.5	9.65	1. 0.0	6. 157.5
			2. 315	7. 135
			3. 292.5	8. 90
			4. 247.5	9. 45
			5. 202.5	
6	-17.5	10.0	1. 0	6. 112.5
			2. 315	7. 45
			3. 270	8. 0
			4. 202.5	9. 315
			5. 157.5	
7	-35	9.3	1. 0	6. 315
			2. 270	7. 225
			3. 202.5	8. 157.5
			4. 112.5	9. 67.5
			5. 45	
8	-35	9.65	1. 0	6. 247.5
			2. 270	7. 135
			3. 157.5	8. 45
			4. 67.5	9. 315
			5. 337.5	
9	-35	10.0	1. 0	6. 157.5
			2. 247.5	7. 45
			3. 135	8. 292.5
			4. 22.5	9. 180
			5. 270	

Figure 44. Nine-Element Test Array Elevation Scan

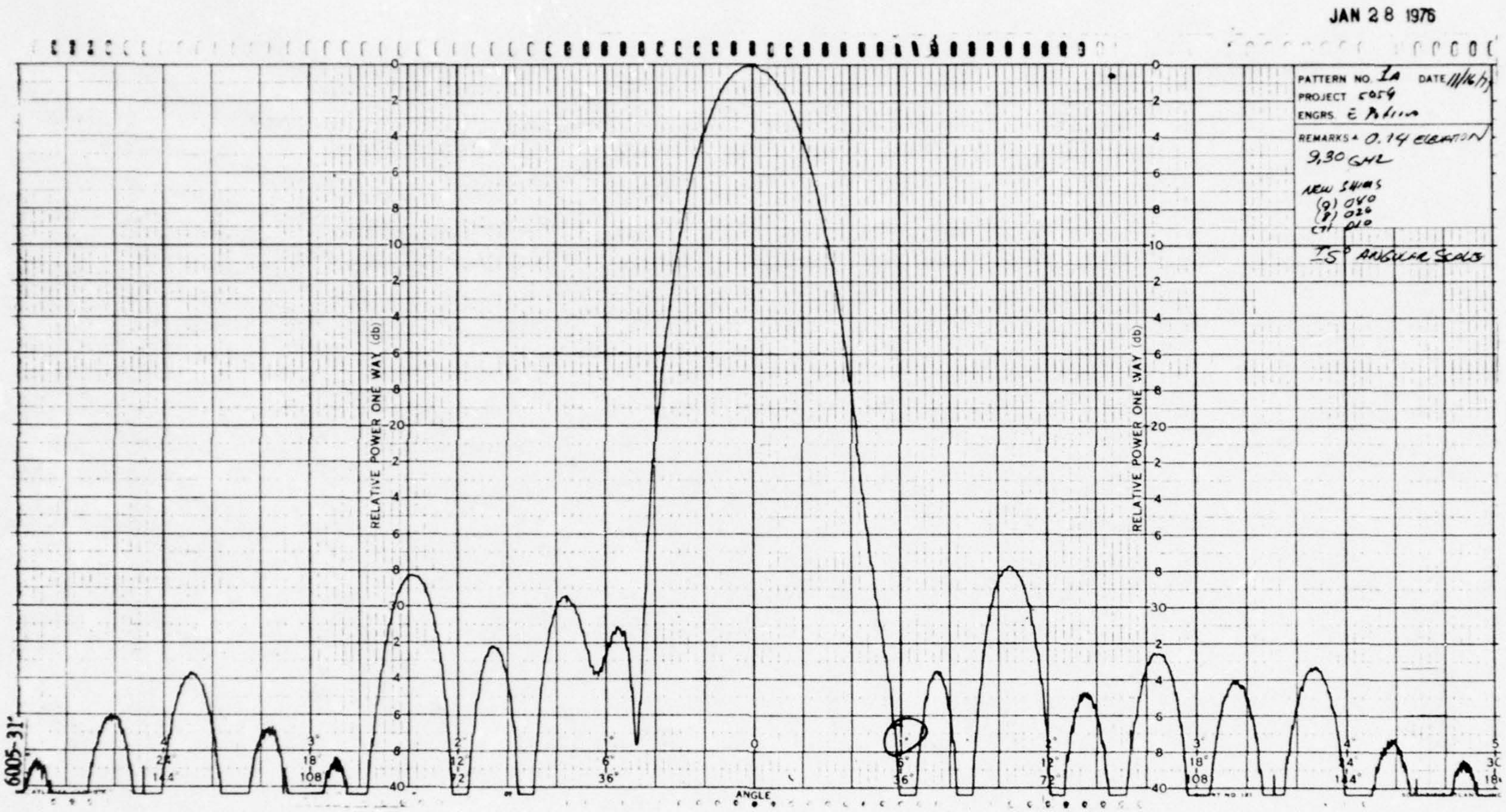


Figure 45. ARBAT 9-Element Test Array Pattern (Beam Normal) (9.30 GHz)

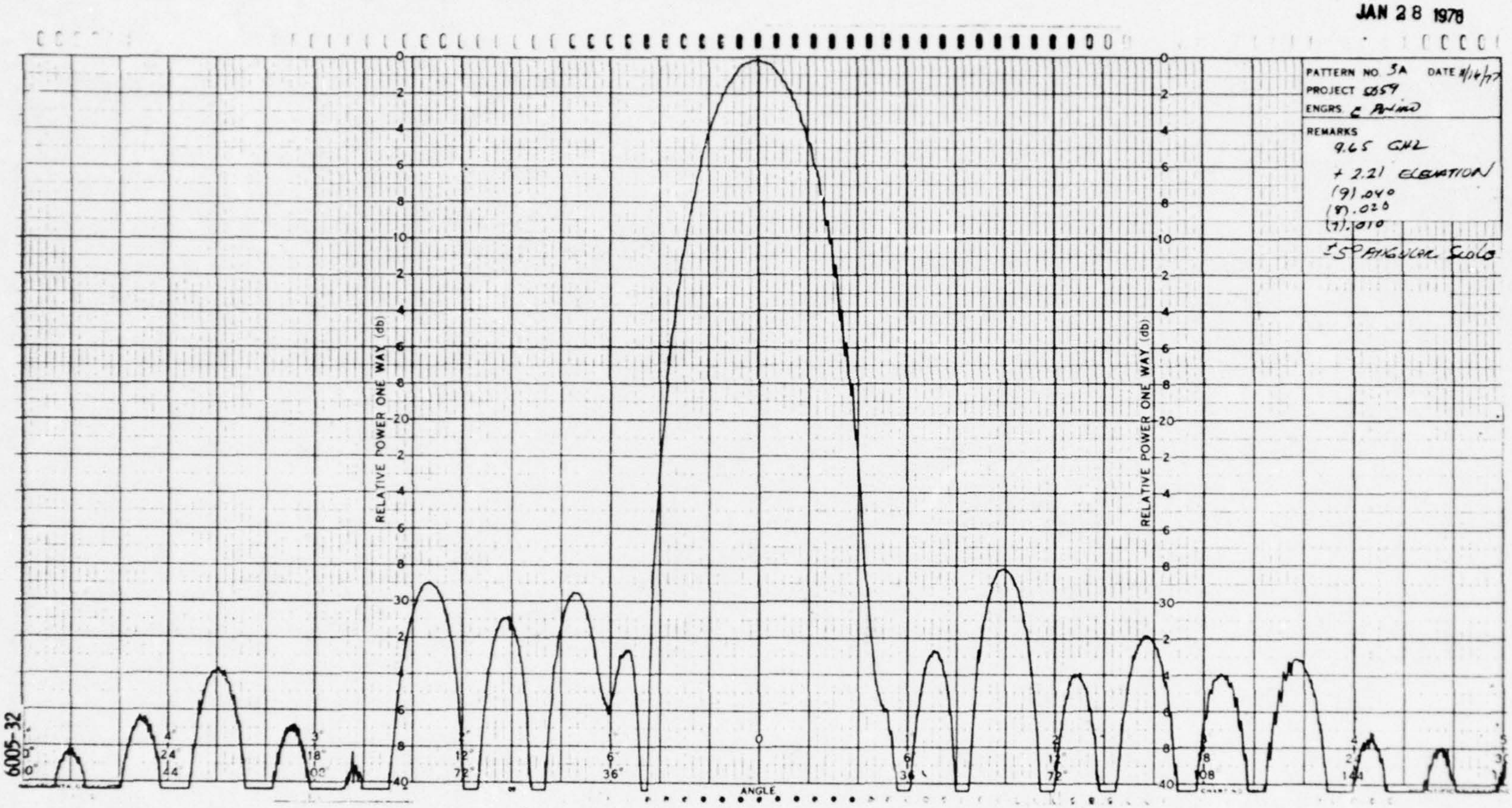


Figure 46. ARBAT 9-Element Test Array Pattern (Beam Normal) (9.65 GHz)

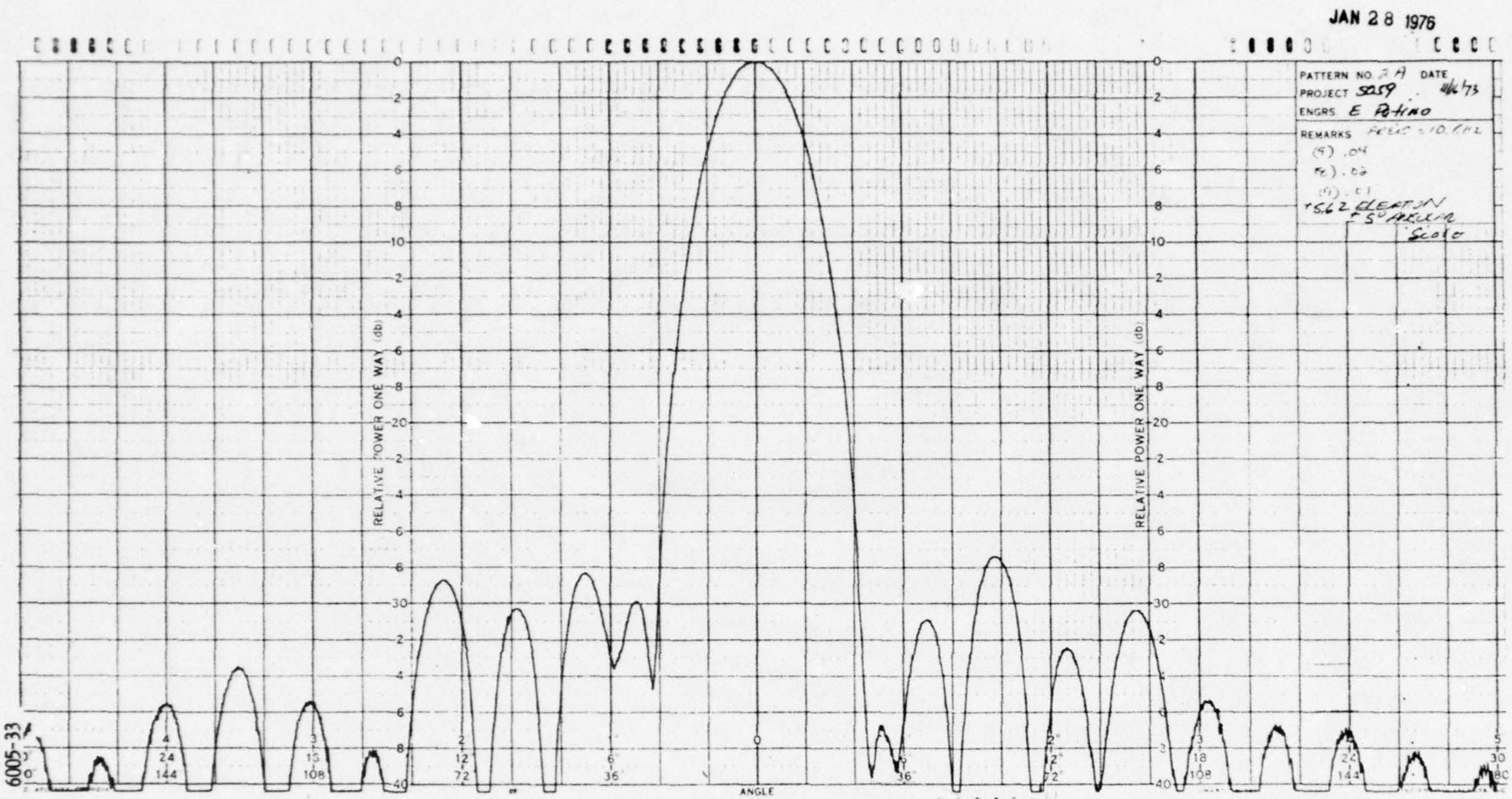


Figure 47. ARBAT 9-Element Test Array Pattern (Beam Normal) (10.0 GHz)

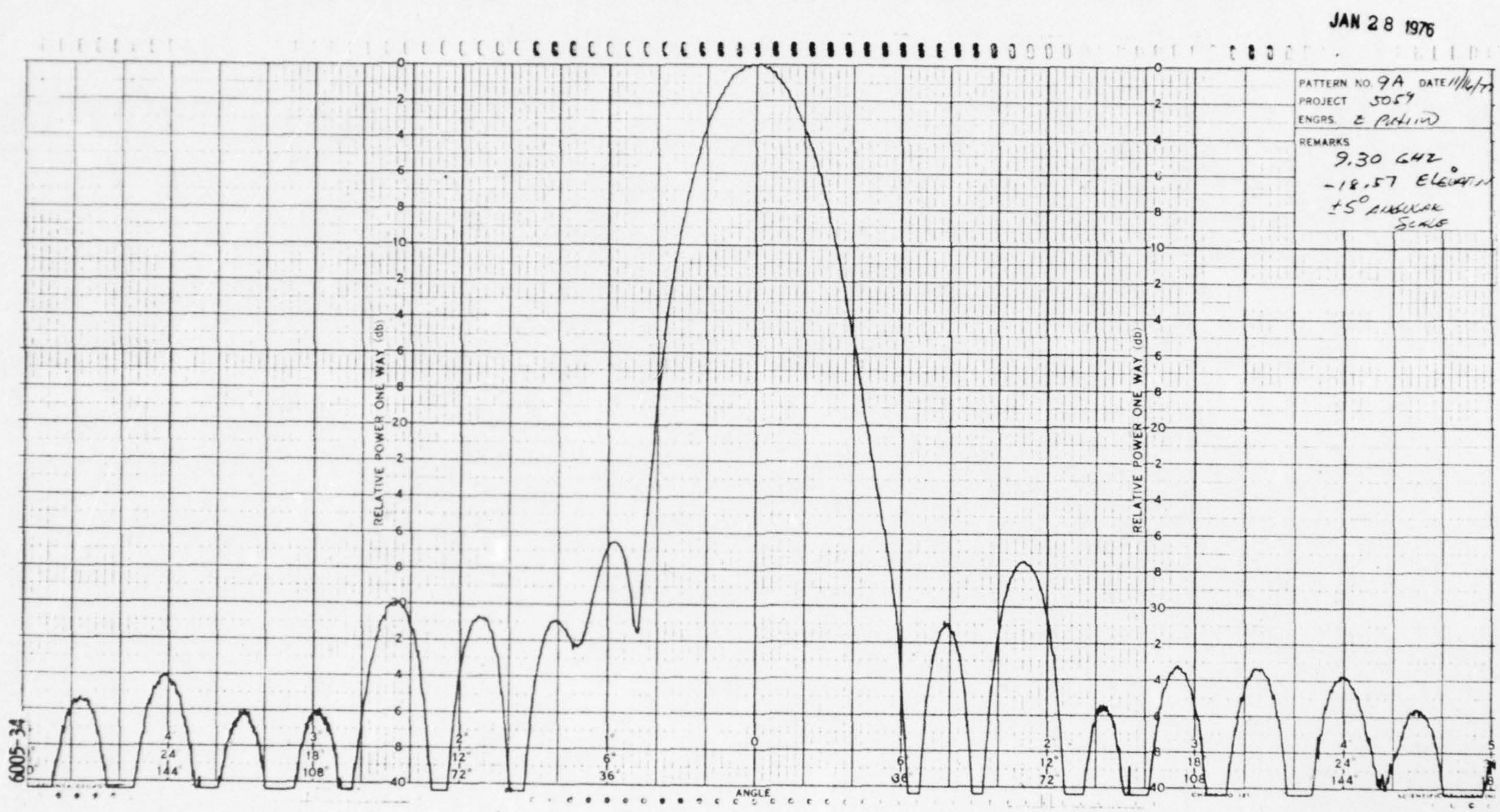


Figure 48. ARBAT 9-Element Test Array Pattern (Mid-Scan) (9.3 GHz)

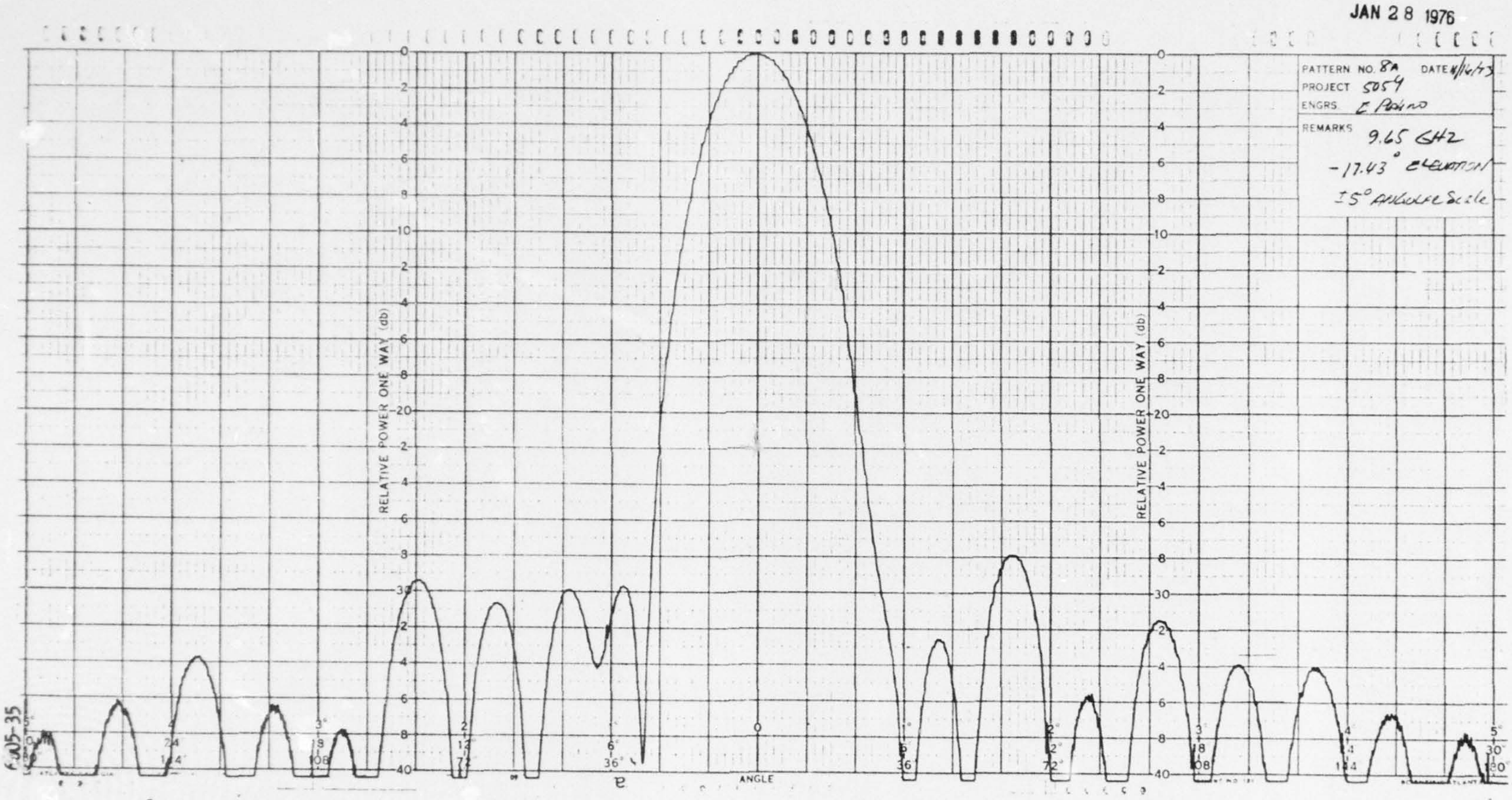


Figure 49. ARBAT 9-Element Test Array Pattern (Mid-Scan) (9.65 GHz)

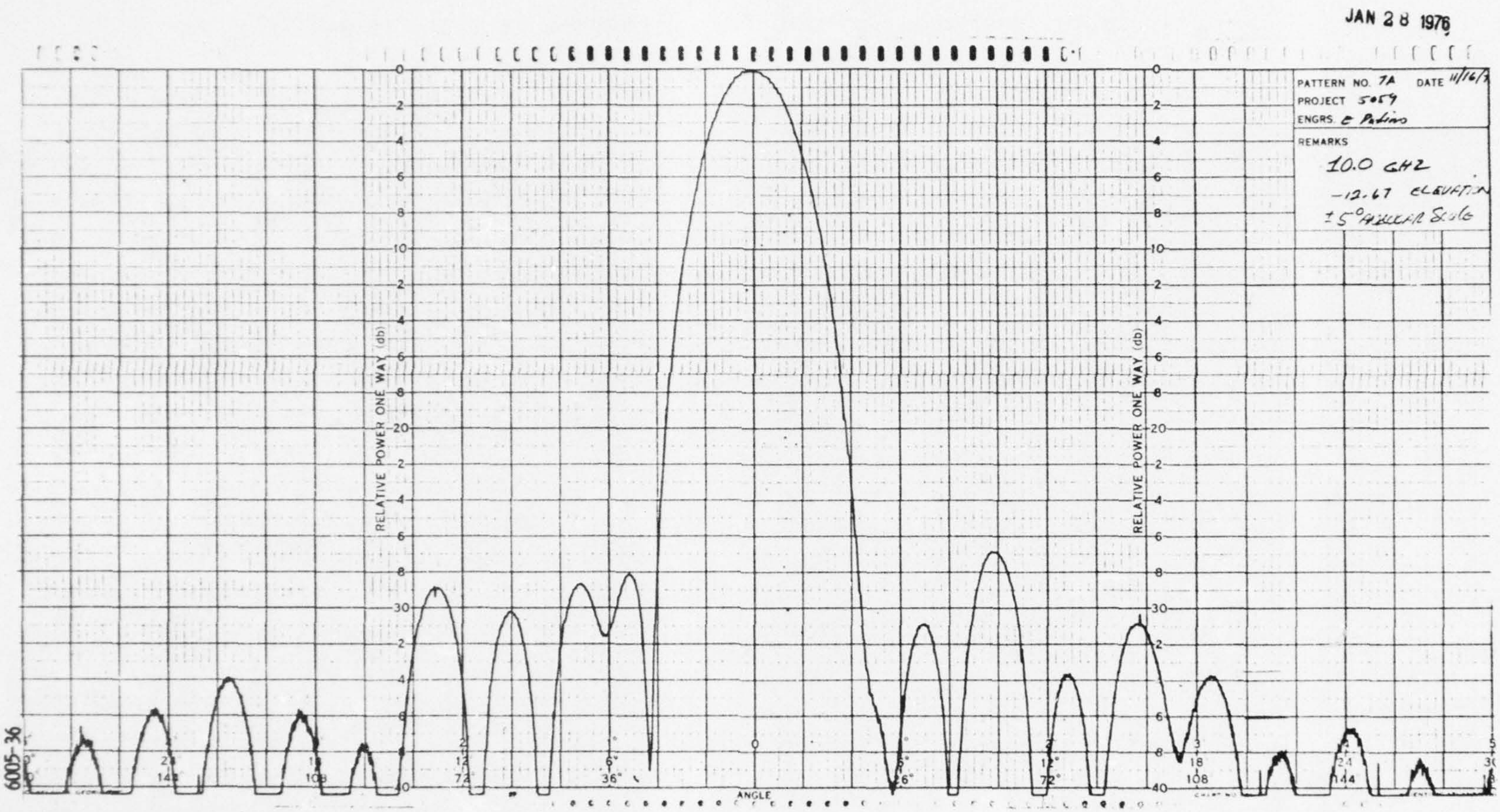


Figure 50. ARBAT 9-Element Test Array Pattern (Mid-Scan) (10.0 GHz)

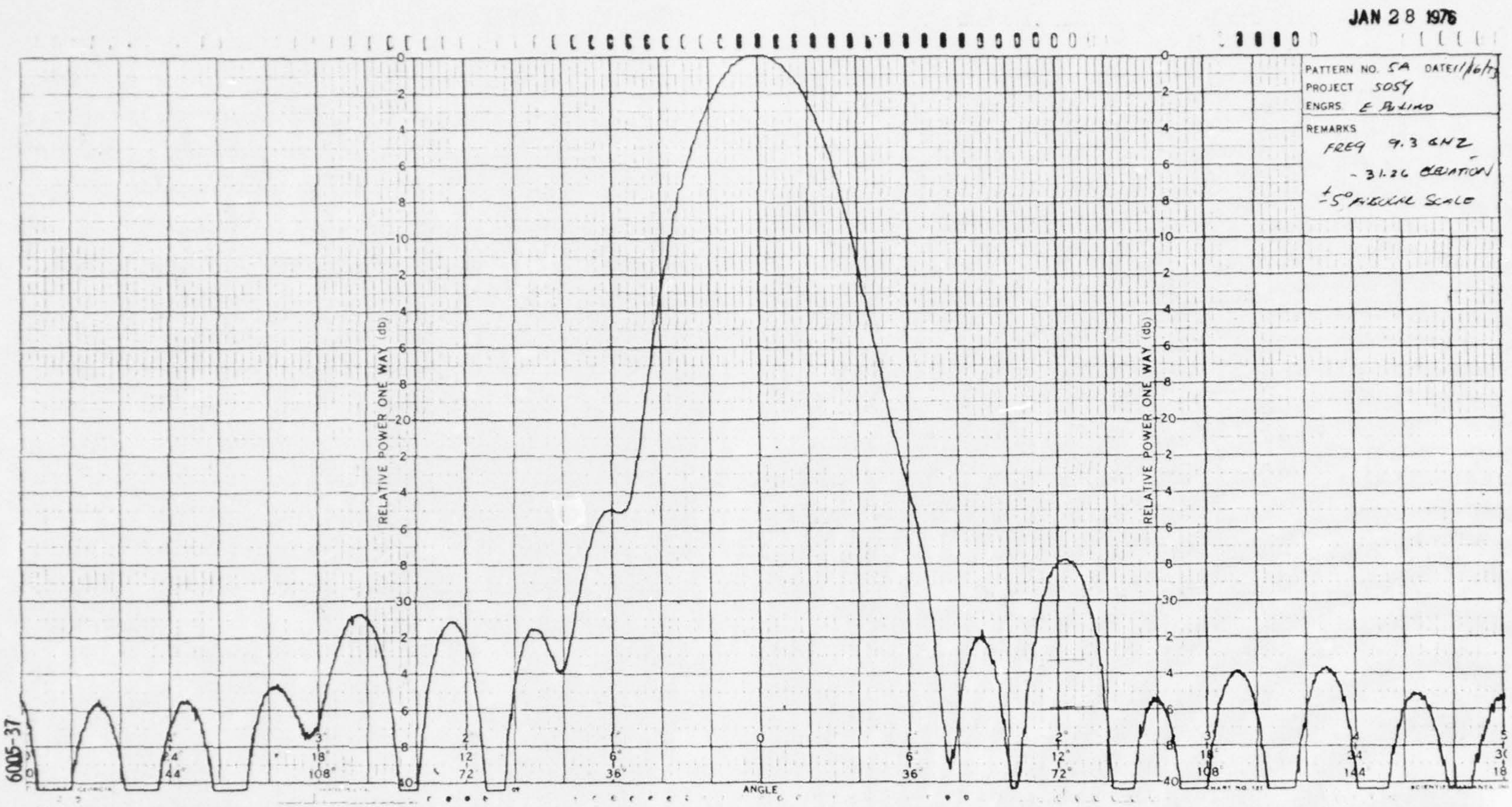


Figure 51. ARBAT 9-Element Test Array Pattern (Scan Limit) (9.3 GHz)

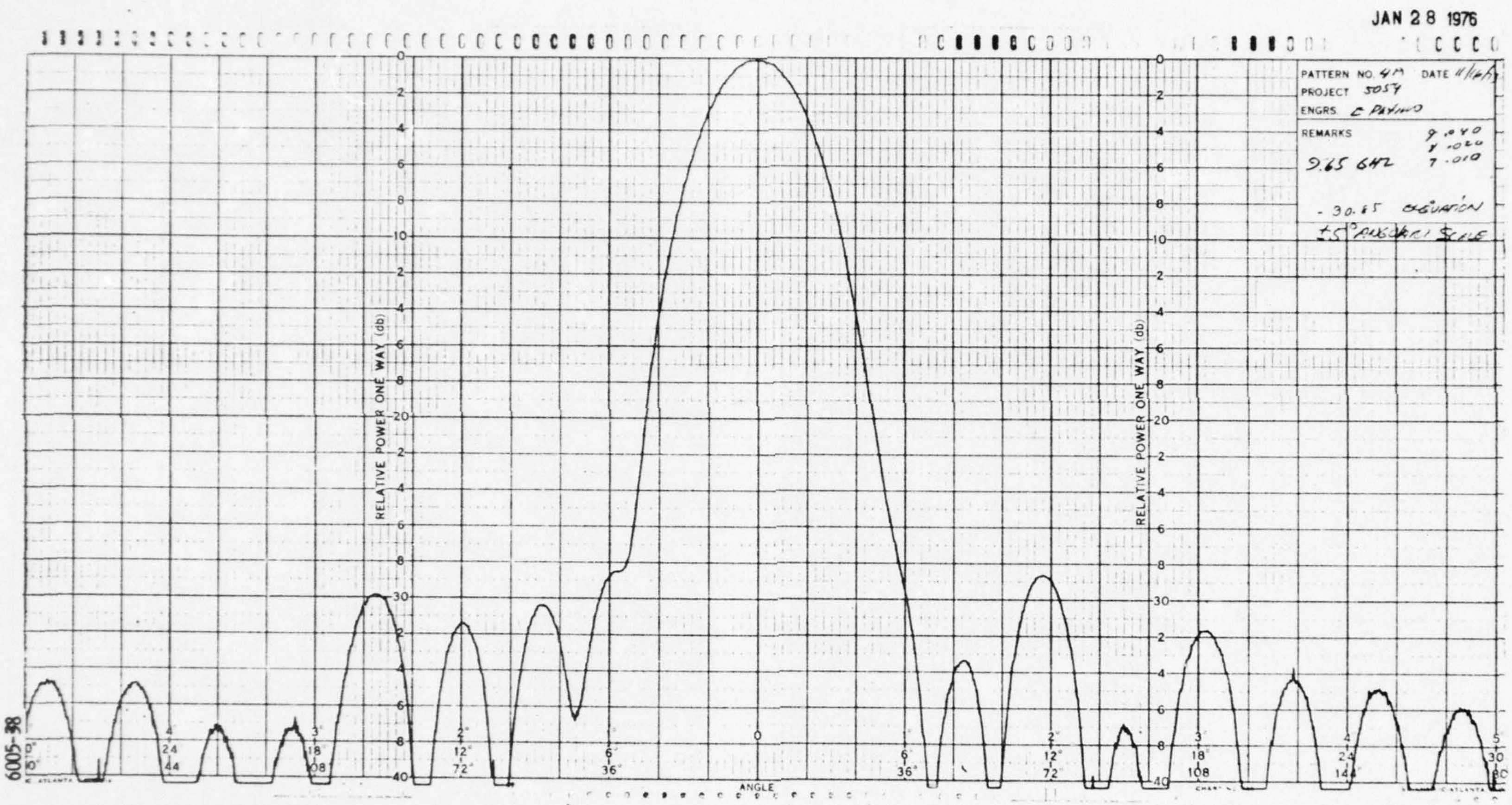


Figure 52. ARBAT 9-Element Test Array Pattern (Scan Limit) (9.65 GHz)

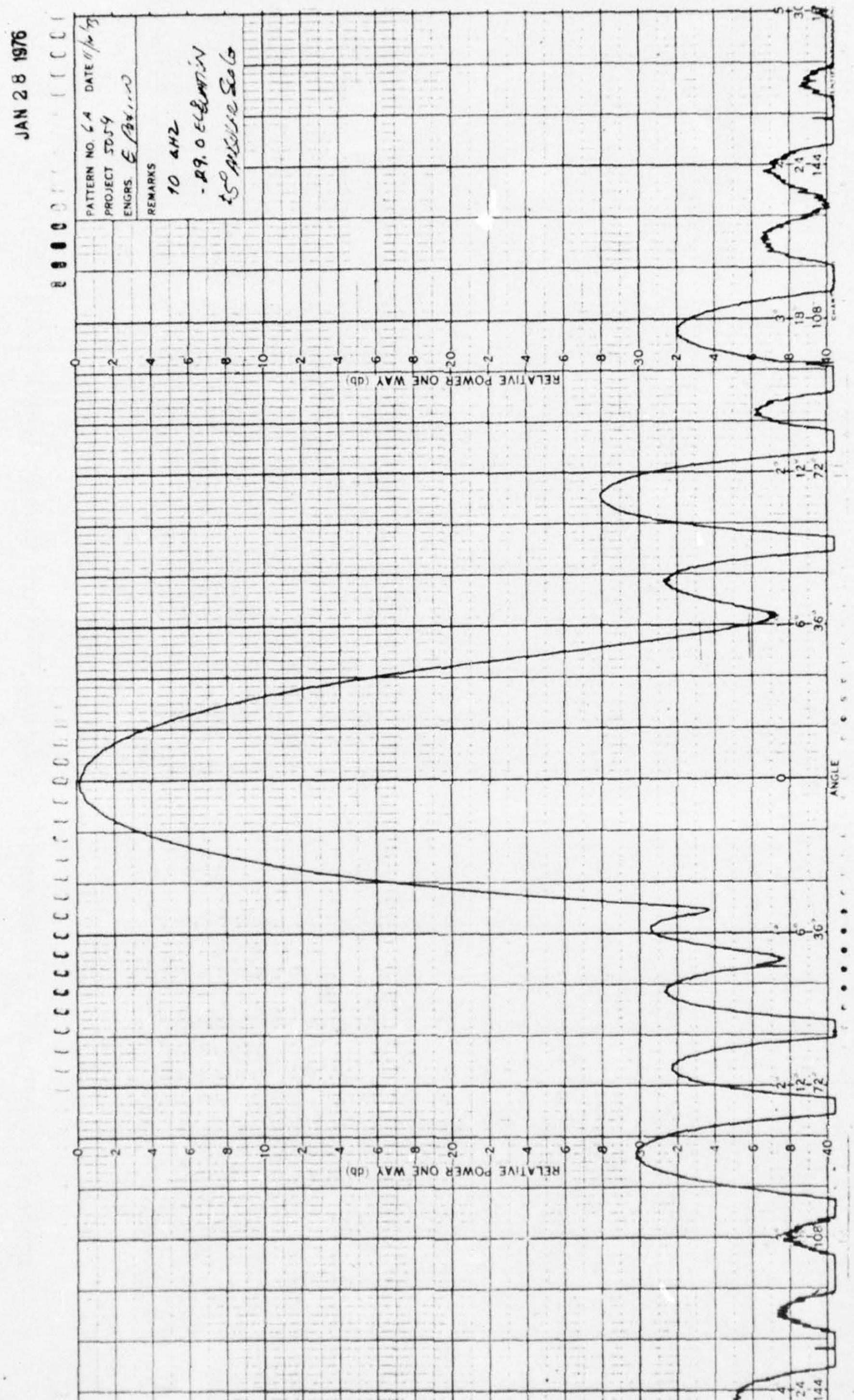


Figure 53. ARBAT 9-Element Test Array Pattern (Scan Limit) (10.0 GHz)

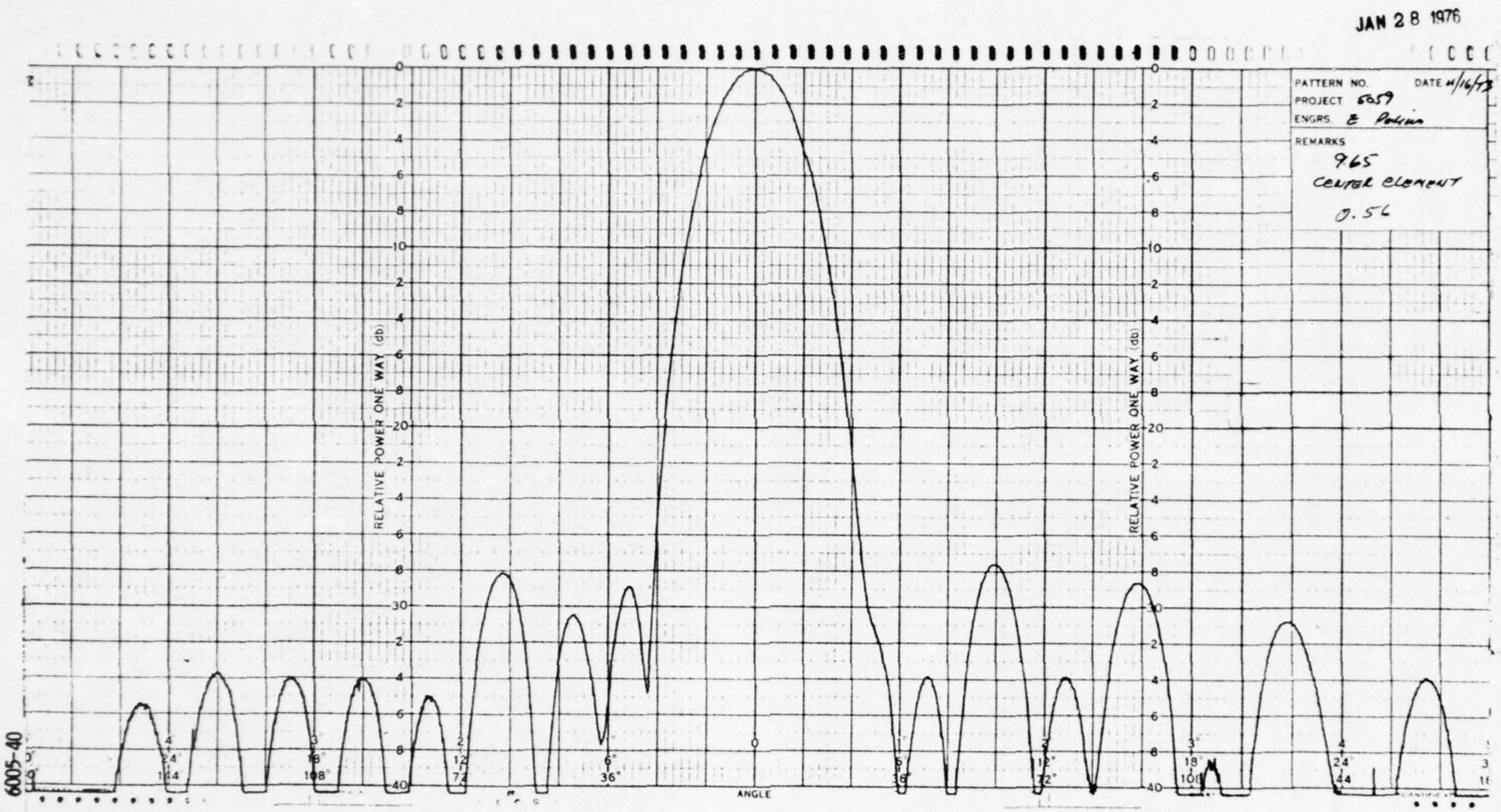


Figure 54. ARBAT 9-Element Test Array Pattern (Center Element Broadside) (9.65 GHz)

4. SUMMARY OF TEST RESULTS

Test results throughout the ARBAT antenna development program have been consistent with the design goals and with the performance of both component parts tested individually and as partial arrays.

Scan coverage and radiation patterns demonstrated in the nine-element test array range testing program were in accordance with the design requirement and predicted performance.

Based on extensive experience in the development of similar antenna subsystems, the results from the 9-element tests can be assumed to be reliably indicative of the full (167 element) array performance with the operational phase shifters.

APPENDIX A

STRUCTURES ANALYSIS

	NAME	DATE	ITT Gilfillan Inc.	SHEET 1 OF
PREPARED	APD	1/30/73		
CHECKED			TITLE PROJECTILE TRACKING RADAR STRUCTURES ANALYSIS	SKETCH NO.
APPROVED				

TRAILER MOUNTED ANTENNA DESIGN PARAMETERS

1. ERROR (a) TOTAL BUDGET ERROR $(\mathcal{E}_t) = 2.0$ MILLI RADIAN

(b) ASSUMED MECHANICAL ERROR FROM ANTENNA TO DATA TAKE-OFF = 25% OF TOTAL $(\mathcal{E}_m) = 0.50$ MR.

THIS IS THE SUM OF THE ERRORS OF ANTENNA REFLECT. STRUCTURES, TORQUE TUBE, AZIMUTH BRG, & DATA TAKE-OFF BOX.

(c) TRAILER & JACK SYSTEM ERROR

$(\mathcal{E}_{j+t_r}) = 0.25$ M.R.

2. TEMPERATURE

(a) $T_{MAX} = 165°F$, $T_{MIN} = -65°F$ } EQUIPMENT SHALL OPERATE

(b) $T_{MAX} = 120°F$, $T_{MIN} = -20°F$ } EQUIPMENT SHALL OPERATE WITH ACCURACY REQUIREMENTS BEING MAINTAINED

3. WIND LOADS

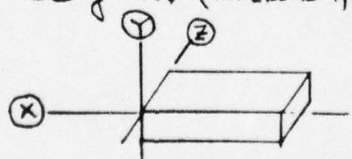
(a) $V_o = 30$ MPH @ $-20°F$ $q_o = .0028 V_o^2 = 2.52$ PSF (OPERATING)

(b) $V_s = 75$ MPH @ $-65°F$ $q_s = .00335 V_s^2 = 18.85$ PSF (SURVIVAL)

4. SHOCK

(a) n_x, n_y & $n_z = 10$ g's (TRUCK TRANSPORT MODE)

(b) n_x & $n_y = 20$ g's MAX (RAILROAD HUMPING IMPACT)



NORMAL TRANSPORT COORDINATE SYSTEM

"X" AXIS – FORE & AFT

Z AXIS – CURBSIDE & ROADSIDE

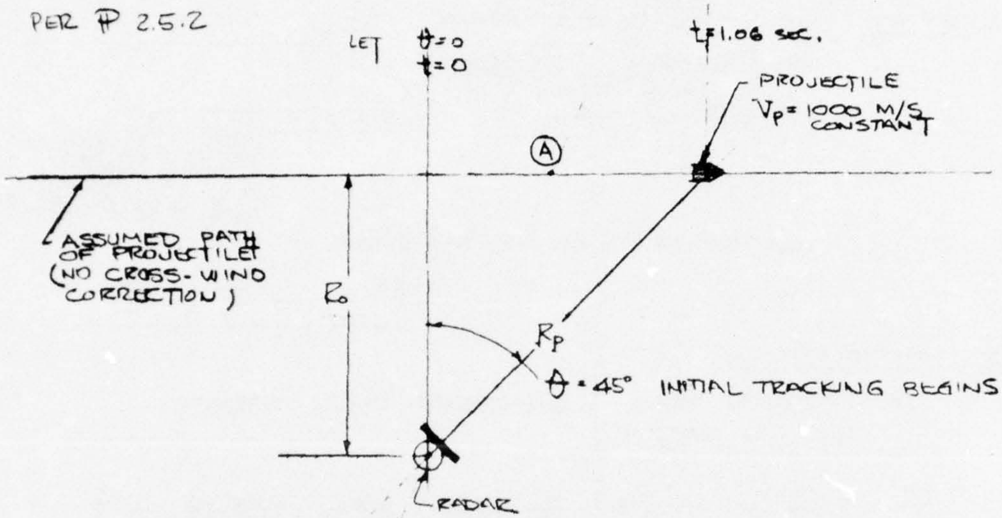
FORM 118 – (5-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 2 OF
PREPARED	APD	1/30/73	TITLE PROJECTILE TRACKING RADAR STRUCTURES ANALYSIS	SKETCH NO.
CHECKED				
APPROVED				

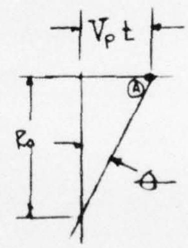
5. AZIMUTH TRACKING - REQUIREMENTS

ANGULAR VELOCITY & ACCELERATION ANALYSIS

PER ¶ 2.5.2



CONSIDER PROJECTILE AT ANY TIME "t"



BY DEFINITION $R_o = R_p \cos 45°$

$$\therefore \tan\theta = \frac{V_p t}{R_o}$$

$$\theta = \tan^{-1}\frac{V_p t}{R_o} \quad \text{——} (1)$$

$$\frac{d\theta}{dt} = \frac{V_p/R_o}{1+\left(\frac{V_p t}{R_o}\right)^2} \quad \text{——} (2)$$

$$\frac{d^2\theta}{dt^2} = \frac{-2\left(V_p/R_o\right)^3 t}{\left[1+\left(\frac{V_p t}{R_o}\right)^2\right]^2} \quad \text{——} (3)$$

FORM 118 - (5-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 3 OF
PREPARED	APD	1/30/73	TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
CHECKED				
APPROVED			STRUCTURES ANALYSIS	

AZIMUTH TRACKING

ANGULAR VELOCITY & ACCELERATION (CONT'D)

SOLVE FOR INITIAL STARTING TIME t_i @ $\theta = 45°$

$$\therefore \quad \tan 45° = 1.0 = \frac{V_p t_i}{R_o}$$

$$t_i = \frac{R_o}{V_p} = \frac{R_p \cos 45°}{V_p} \quad \text{LET } R_p = 1500 \text{ M}$$

$$= \frac{1500 \times .707}{1000}$$

$$\boxed{t_i = 1.06 \text{ SEC.}}$$

PER ¶ 2.1 REQUIREMENTS

WITH ELECTRONIC SCAN @ ± 3.5°/SEC.

$$\dot{\theta} = 40°/\text{SEC} = 0.70 \text{ RAD/SEC}$$

$$\ddot{\theta} = 40°/\text{SEC}^2 = 0.70 \text{ RAD/SEC}^2$$

SOLVE FOR MINIMUM R_p TO SATISFY BOTH CONDITION @ 45° ORIENTATION

$$\dot{\theta} = \frac{V_p}{2R_p \cos 45°} = 0.70 \text{ RAD/SEC}$$

$\boxed{R_p = 1010 \text{ METERS}}$ BUT $\ddot{\theta}_{@t=0} = 0.98 \text{ RAD/SEC}^2$

$t_i = .714$ SEC

SOLVE EQN (3) FOR R_p FOR $\ddot{\theta} = 0.70$ RAD/SEC^2.

$$\ddot{\theta} = \frac{-2\left(V_p/R_p \cos 45°\right)^3 t_i}{\left[1 + \left(\frac{V_p t_i}{R_p \cos 45°}\right)^2\right]^2} = 0.70$$

$R_p = 1200$ METERS

$\ddot{\theta} = 33.8°/\text{SEC} = 0.6$ RAD/SEC

$t_i = .8484$ SECS.

FORM 118 – (5-67)

PREPARED	NAME APD	DATE 1/30/73	ITT Gilfillan Inc.	SHEET 4 OF
CHECKED			TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
APPROVED			STRUCTURES ANALYSIS	

ANTENNA SYSTEM

INTRODUCTION: THE ANTENNA SYSTEM WILL BE MOUNTED ON A VEHICLE BED WITH JACK PAD PROVISIONS TO LIFT THE ENTIRE OR PORTION OF THE SPRUNG MASS OF THE VEHICLE-ANTENNA SYSTEM. THE ANTENNA WILL BE OF ARRAY WITH PHASE SHIFTER TYPE DESIGN ATTACHED TO A CENTER MAIN STRONG BACK STRUCTURE WHICH SERVES AS A TORQUE TUBE AS WELL AS A CANTILEVER BEAM FOR ELEVATION BENDING MOMENT.

THE ANTENNA WILL HAVE A MAXIMUM TILT OF 25° WITH THE VERTICAL AXIS. THE TRANSCEIVER ASSEMBLY WILL BE MOUNTED TO THE MAIN BACK STRUCTURE SO POSITIONED FOR MINIMUM MASS MOMENT OF INERTIA EFFECT ABOUT THE AZIMUTHAL AXIS.

THE ANTENNA SYSTEM WILL BE ASSEMBLED TO A PEDESTAL WHICH HOUSES THE BULL GEAR - BEARING ASSEMBLY, DRIVE MOTOR, GEAR BOX & DATA TAKE-OFF. EXISTING AN/SPS-48 PEDESTAL CAN EASILY BE ADAPTED IN THIS DESIGN. THE PEDESTAL IN TURN IS PERMANENTLY BOLTED TO THE TRAILER BED. THE TRAILER IN THE JACKED POSITION SHALL BE SO DESIGNED TO ACT AS NEARLY RIGID FOR SUDDENLY APPLIED TORSIONAL LOAD AT THE PEDESTAL BASE. THE JACK-PADS WILL REST ON A PREPARED ON-SITE GROUND FOOTING. THE 8 HOURS SET UP TIME CAN BE ACHIEVED. THE JACK ASSEMBLY LATERAL DEFLECTION (WHICH INCLUDES ANY ATTACHMENT TO THE TRAILER BODY) SHALL BE HELD TO AN ACCEPTABLE LIMIT UNDER OPERATING CONDITION.

FORM 118 - (5-67)

PREPARED	NAME APD	DATE 1/30/73	ITT Gilfillan Inc.	SHEET 5 OF
CHECKED			TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
APPROVED			STRUCTURES ANALYSIS	

ANTENNA SYSTEM WEIGHTS

WEIGHT ANALYSIS - "X" BAND RADAR

COMPONENTS

(1)	BASIC W.G. ARRAYS 2004 FT @ .12#/FT	= 240 LBS
(2)	W.G. FLANGES (167) & HARDWARES	= 30 LBS
(3)	PHASE SHIFTERS (167 @ .9# EA)	= 150 LBS
(4)	LINE FEED W.G. + BENT TRANSITION	= 25 LBS
(5)	BUFFER BEAM, STEERING	= 25 LBS
(6)	POWER SUPPLY	= 50 LBS
(7)	CABLE, BUS BAR, DEHYDRATOR, ETC	= 30 LBS
(8)	TRANSCEIVER ASSY	= 375 LBS
(9)	COOLING FANS	= 15 LBS
	SUB-TOTAL (1)	= 940 LBS

STRUCTURES & HOUSINGS

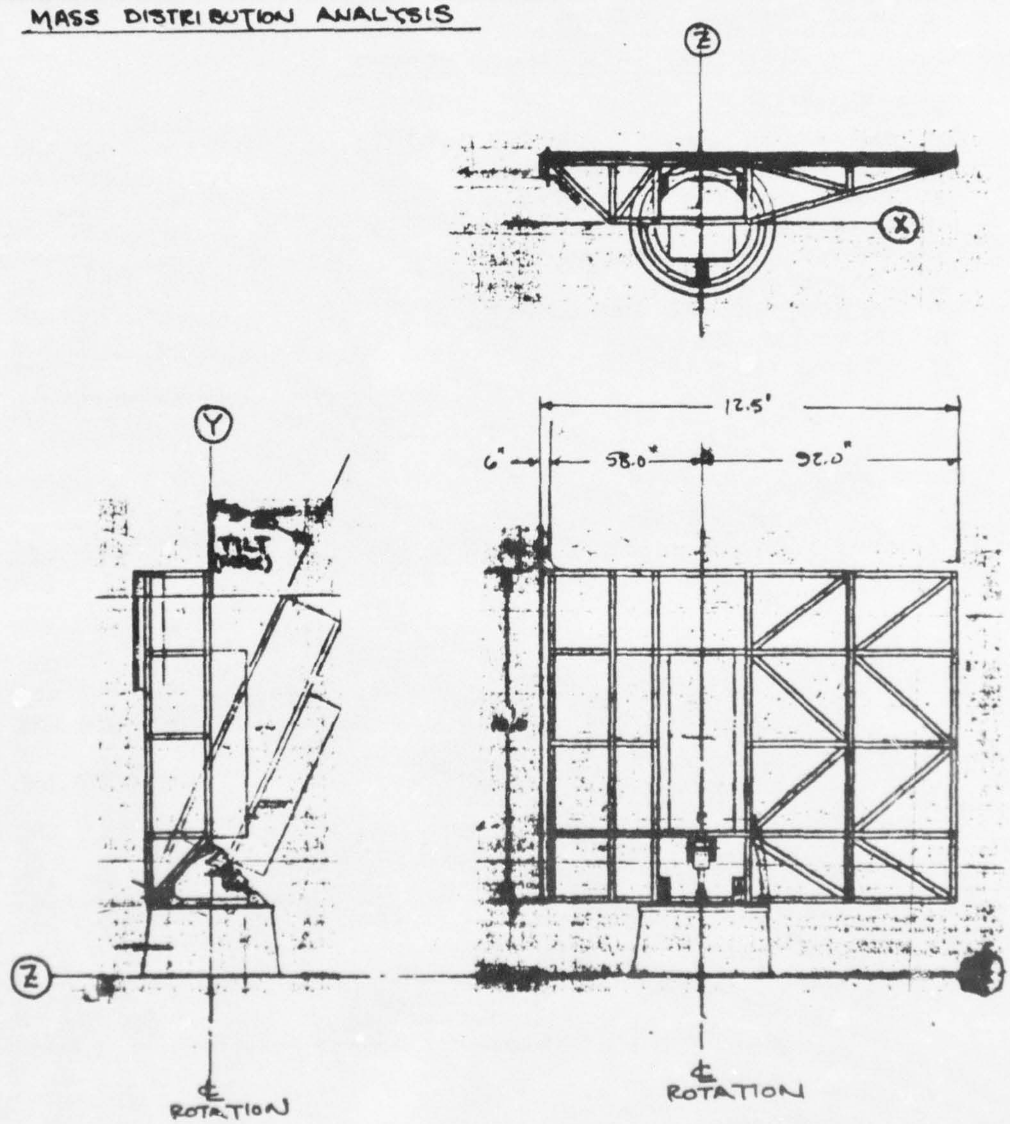
(1)	USING AN/SPS-48 PEDESTAL (ROTATING MASS ONLY)	
	(a) TOP PLATE ADAPTER (D_o = 46.0 IN, D_i = 24.0 IN) + CLEVISES	= 120 LBS
	(b) INNER BRG RACE $A = 5.0\ IN^2$ $D_{AV} = 37.0\ IN$	= 170 LBS
	SUB-TOTAL (2)	= 290 LBS
(2)	PHASE SHIFTER HOUSING + TRANSITION PLATE	= 50 LBS
(3)	COMPONENT ITEMS 5 6 & 7 HOUSING	= 20 LBS
(4)	CENTER MAIN TORQUE-BOX BEAM TUBE t = 0.25, 24.0 x 32.0	= 350 LBS
(5)	TRUSS MEMBERS 275 FT @ 1.31 #/FT	= 360 LBS
(6)	10 TON ACTUATOR #1810	= 60 LBS
	SUB-TOTAL (3)	= 840 LBS

TOTAL WEIGHT ROTATING MASS = 2070 LBS

FORM 118 - (5-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 6 OF
PREPARED	HPD	1/30/73	TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
CHECKED				
APPROVED			STRUCTURES ANALYSIS	

MASS DISTRIBUTION ANALYSIS



PEDESTAL-ANTENNA ASSEMBLY CONFIGURATION

FORM 118 - (5-67)

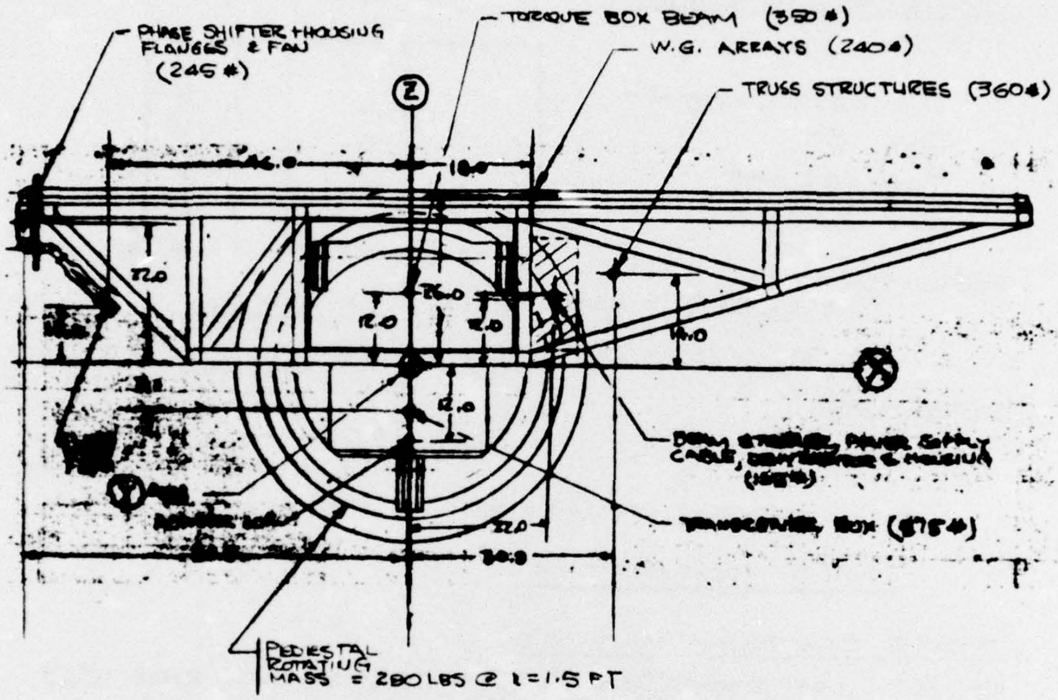
AD-A033 605 ITT GILFILLAN INC VAN NUYS CALIF F/G 17/9
MM AND TE-APPLICATION OF RADAR TO BALLISTIC ACCEPTANCE TESTING --ETC(U)
SEP 76 C BARFIELD DAAA21-73-C-0664
UNCLASSIFIED ITTG-50598 NL

2 OF 2
AD
A033605

END
DATE
FILMED
2-77

	NAME	DATE	ITT Gilfillan Inc.	SHEET 7 OF
PREPARED	ARD	1/30/73	TITLE PROJECTILE TRACKING RADAR STRUCTURES ANALYSIS	SKETCH NO.
CHECKED				
APPROVED				

MASS DISTRIBUTION ANALYSIS (CONT'D)



PLAN VIEW - MASS DISTRIBUTION

$$\bar{X} = \frac{-245\times60-25\times46+240\times18+360\times30+125\times22.0}{2070} = \frac{2020}{2070} = \underline{0.97\ \text{IN}}$$

$$\bar{Z} = \frac{245\times22.0+25\times10+240\times26.0+350\times12.0+360\times14+125\times12.0-375\times7.0-60\times12.0}{2070}$$

$$R = \sqrt{Z^2+X^2} \qquad = \frac{19270}{2070} = \underline{9.30\ \text{IN}}$$

$$I_M)_{YY} = \frac{1}{32.2}\left[245(63.9)^2+25(47)^2+60(12.0)^2+375(7.0)^2+350(12)^2+290(18)^2 + 125(25)^2+\frac{360}{12}(144)^2+360(33)^2+\frac{240}{12}(150)^2+240(31.5)^2\right]\frac{1}{144} = \frac{3.012\times10^6}{32.2\times144}$$

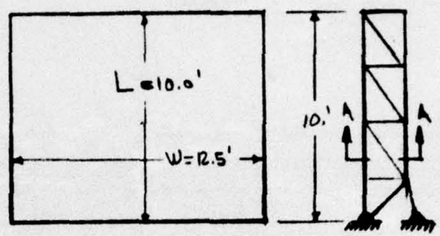
$$\underline{I_M)_{YY} = 650.0\ \#\text{-FT SEC}^2}$$

FORM 118 - (5-67)

PREPARED	NAME APD	DATE 1/31/73	ITT Gilfillan Inc. TITLE PROJECTILE TRACKING RADAR	SHEET 8 OF
CHECKED				SKETCH NO.
APPROVED			STRUCTURES ANALYSIS	

STRUCTURES ANALYSIS

WIND LOAD



$A = 12.5 \times 10.0 = 125 \text{ FT}^2$

$C_D = 1.30$

$q_o = 2.52$ PSF

$q_s = 18.85$ PSF

DRAG LOAD

$F_o = C_D q_o A = 1.30 \times 2.52 \times 125 = \underline{\underline{410 \text{ LBS}}}$

$F_s = C_D q_s A = 1.30 \times 18.85 \times 125 = \underline{\underline{3070 \text{ LBS}}}$

TORQUE LOAD

$T_{WL} = C_E W q A$ where $C_E = 0.15$, $q_o = 2.52$ PSF @ 30 MPH

$= 0.15 \times 12.5 \times 2.52 \times 125$

$T_{WL} = 590.0$ FT-#

TORQUE BOX-BEAM ANALYSIS

REF P(1) LET ERROR TORQUE TUBE ≦ 25% OF MECH. ERROR (E_m)

(a) $E_{tt} \leqq .25 \times .50 = .125$ M.R

(b) $\alpha = 0.70$ RAD/SEC²

(c) $I_m)_y = 650.0$ #-FT SEC²

TOTAL TORQUE LOAD ON TUBE

(455)

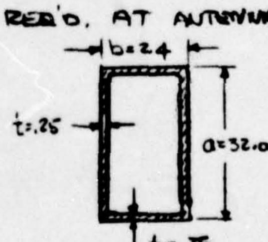
$T_T = I_m \alpha + T_{WL} = 0.70 \times 650 + 590.0$

$T_T = 1045.0$ FT-# MAXIMUM TORQUE REQ'D. AT ANTENNA

TORSIONAL STIFFNESS (K) OF TUBE

CLOSED RECTANGULAR SECTION $K = \dfrac{2 t b^2 a^2}{(a+b)} = \dfrac{2 \times .25 (24)^2 (32)^2}{(24+32)}$

$K = 5266.0 \text{ IN}^4$



SECTION A-A

FORM 118 - (5-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 9 OF
PREPARED	AFD	1/31/73		SKETCH NO.
CHECKED			TITLE PROJECTILE TRACKING RADAR	
APPROVED			STRUCTURES ANALYSIS	

TORQUE BOX-BEAM ANALYSIS (CONT'D)

SOLVE FOR ANGULAR TWIST "θ_{tt}"

$$\theta_{tt} = \frac{T_T L}{KG}$$

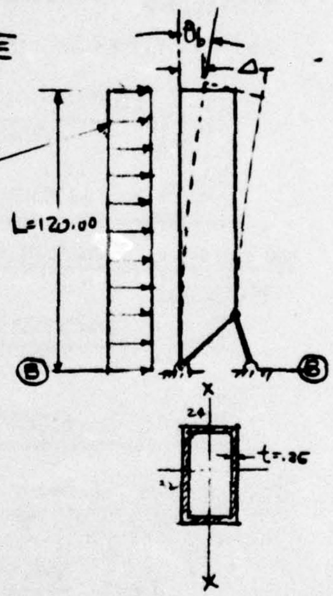
where: $T_T = 1045 \times 12$ IN-#
$G = 3.8 \times 10^6$ psi (AL ALLOY)
$L = 120.0$ IN
$K = 5266.0$ IN^4

$$= \frac{1045 \times 12 \times 120}{5266.0 \times 3.8 \times 10^6}$$

$$\varepsilon_{tt} = \underline{\theta_{tt}} = 0.075 \times 10^{-3} \text{ RAD} = \underline{0.075 \text{ M.R.}} \ll \varepsilon_{tt} = .125 \text{ OK}$$

BENDING DEFLECTION & ROTATION OF TUBE

AT 30 MPH WIND
CONSIDER TUBE CANTILEVERED @ (B)-(B)
UNIFORMLY LOADED



$$\Delta_T = \frac{WL^3}{8EI_{xx}} = \frac{410(120)^3}{8 \times 10^7 \times 2800}$$

$$\underline{\Delta_T = 0.0032 \text{ IN}}$$

ANGULAR ROTATION θ_b

$$\theta_b = \varepsilon_b = \frac{WL^2}{6EI} = \frac{410(120)^2}{6 \times 10^7 \times 2800}$$

$$\underline{\varepsilon_b = 0.035 \text{ M.R.}}$$

$$I_{xx} = \frac{1}{12}\left[24^3 \times 32 - 23.5^3 \times 31.5\right]$$

$$\underline{I_{xx} = 2800 \text{ IN}^4}$$

TILTING SCREW ACTUATOR ANALYSIS

THE ACTUATOR WILL BE A DUFF-NORTON SCREW ACTUATOR MODEL # 1810 RATED AT 10 TON. THE LIFTING SCREW IS A 2.00 INCH DIA. WITH A .50 INCH PITCH SQUARE THREAD. THE ERECTED LENGTH OF THE SCREW IS

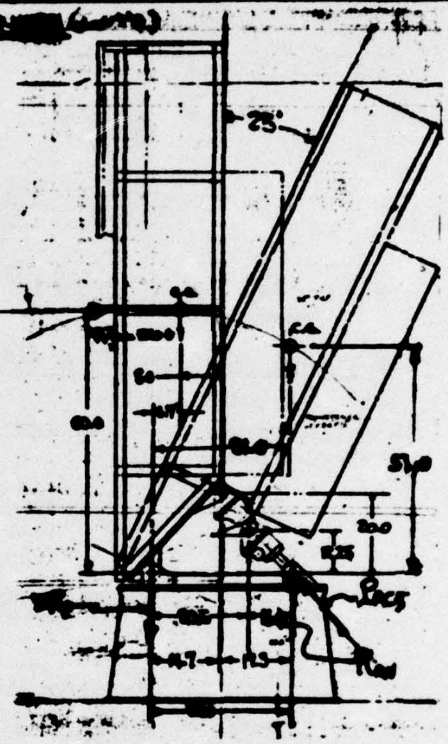
$$L_{eff} = 19.50 \text{ INCHES}$$

CALCULATE LOADS ON ACTUATOR & TRUNNIONS

FORM 118 - (5-67)

PREPARED	NAME: APD	DATE: 1/31/73	ITT Gilfillan Inc.	SHEET 10 OF
CHECKED			TITLE: PROJECTILE TRACKING RADAR	SKETCH NO.
APPROVED			STRUCTURES ANALYSIS	

ANTENNA TRUNNION PIVOT & ACTUATOR AN[illegible]



THE TRUNNION PIVOTS & ACTUATOR ARE ANALYZED FOR LOAD AS FOLLOWS:

(a) WIND LOAD (ERECT CONDITION) $F_o = 410$ # (OPERATING)
$F_S = 3070$ # (SURVIVAL)

(b) RAILROAD IMPACT LOAD AT $n_y = n_z = 20$ g's

OPERATING CONDITION

$$\Sigma M_{R_P} = 0$$

$$60 F_o + 1720 \times 6.7 = 32.0 \left[\frac{20.0 P_{ACT})_o}{(20.0 + 17.3)} \right]$$

$$P_{ACT})_o = \frac{(60 \times 410 + 1720 \times 6.7)\, 26.44}{32.0 \times 20.0}$$

$$P_{ACT})_o = 1500 \text{ LBS}$$

SURVIVAL CONDITION

$$\Sigma M_{R_P} = 0$$

$$P_{ACT})_S = \frac{(60 \times 3070 + 1720 \times 6.7)(26.44)}{32.0 \times 20.0}$$

$$P_{ACT})_S = 8090 \text{ LBS}$$

RAILROAD IMPACT LOAD $n_z = n_y = 20$ g's (25° TILT)

$n_z = 20$ g's $\quad P_{ACT} = 0.0$

$$R_P = \frac{W_n \times 51 (n_z)}{24.0} = \frac{1720 \times 51 \times 20}{24.0} = 73{,}000 \text{ LBS}$$

$n_y = 20$ g's

$$P_{ACT}) = \frac{31.0 \times W_n\, n_y}{32.0 \times 12.25} (11.45 + 12.25) = \frac{31.0 \times 1720 \times 20 \times 16.76}{32.0 \times 12.25}$$

$$* P_{ACT}) = 45{,}600 \text{ LBS}$$

* BASED ON THESE CALCULATED LOADS ON TRUNNION & ACTUATOR, STOWAGE BARS ARE REQUIRED DURING RAIL ROAD SHIPMENT OF ANTENNA ASSEMBLY.

FORM 118 - (5-67)

PREPARED	AHD	1/31/73	ITT Gilfillan Inc.	SHEET 11 OF
CHECKED			TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
APPROVED			STRUCTURES ANALYSIS	

SCREW ACTUATOR ELONGATION OR CONTRACTION

ACTUATOR SCREW, SQUARE THREAD

$D_o = 2.00$ IN

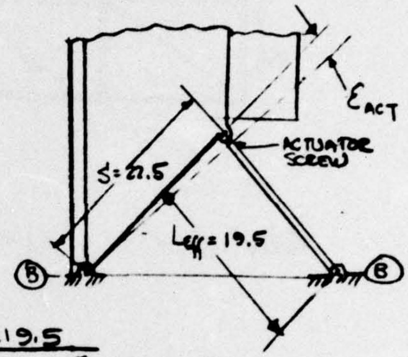
$D_R = 1.612$ IN

$L_{eff} = 19.5$ IN

$E = 29 \times 10^6$ psi

$P_{ACT})_o = 1500$ LBS

$A_R = \frac{\pi}{4}(1.612)^2 = 2.05\ IN^2$



ANGULAR ERROR (ε_{ACT}) ELEVATION

OPERATING CONDITION

$$\Delta_{ACT} = \frac{P_{ACT})_o L_{eff}}{A_R E} = \frac{1500 \times 19.5}{2.05 \times 29 \times 10^6}$$

$$\Delta_{ACT} = .00048 \text{ IN}$$

$$\underline{\varepsilon_{ACT}} = \frac{\Delta_{ACT}}{S} = \frac{.00048}{22.5} = \underline{0.02 \text{ M.R.}}$$

CHECK BUCKLING

CONSIDER SCREW LENGTH FIXED AT ONE END

$$P_{CR} = \frac{\pi^2 E A_R}{4\left(\frac{L_{eff}}{r}\right)^2} \quad \text{where } r = \frac{D_R}{4} = 1.612/4 = .403$$

$$\underline{P_{CR}} = \frac{(3.14)^2 \times 29 \times 10^6 \times 2.05}{4\left(\frac{19.5}{.403}\right)^2} = \underline{62{,}600 \text{ LBS}} \ \underline{\text{OK}}$$

AZIMUTH BEARING ANGULAR ROTATION (ELEV) (ε_{BRG})

$$k_{brg} = 5.5 \times 10^8 \text{ IN-\# /RADIAN}$$

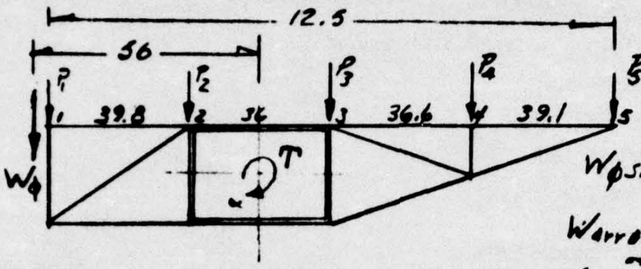
$$M_{BB} = F_o \times 60 = 410 \times 60 = 24600 \text{ IN-\#}$$

$$\varepsilon_{BRG} = \frac{M_{BB}}{k_{brg}} = \frac{24{,}600}{5.5 \times 10^8} = 45.0 \times 10^{-6} \text{ RADIAN}$$

$$\underline{\varepsilon_{BRG} = 0.045 \text{ M.R.}}$$

FORM 118 - (5-67)

PREPARED / CHECKED / APPROVED	NAME	DATE	ITT Gilfillan Inc.	SHEET 12 OF
PREPARED	D Lee	7/25/73	TITLE ARBAT COMBINED STRUCTURAL LOADING	SKETCH NO. PHASE B
CHECKED				
APPROVED				



$W_{\phi shifter} = \frac{322}{3'} = 107\ lb$

$W_{array} = \frac{270}{3(12.5)} = 7.5\ \#/FT$

$W_{struct} = \frac{420}{3(12.5)} = 11.7\ \#/FT$

Wind load – $F_o = 410\ lb$ OPERATING
$F_s = 3070$ SURVIVAL $\quad F_s/F_o = 7.5$

$$w_0 = \frac{F_0}{3}\left(\frac{1}{12.5}\right) = \frac{410}{3}\,\frac{1}{12.5} = 11\ \#/ft$$

JOINT LOADS DUE TO WIND

$$P_1 = \frac{3}{2}(11) = \underline{16.5\ \#}$$

$$P_2 = P_3 = P_4 = 3(11) = \underline{33\ \#}$$

$$P_5 = \frac{3}{2}(11) = \underline{16.5\ \#}$$

JOINT LOADS DUE TO ACCELERATION $\quad \alpha = .7\ rad/sec^2$

$$F = ma = \frac{W}{g} r\alpha = .02174\, W r$$

$$F_1 = \left[W r + (25 + 11.7)\left(\frac{3}{2}\right)52\right]\frac{.02174}{12} = \left[107\overset{6000}{(56)} + 19.5\overset{1520}{(1.5)}52\right]\frac{.02174}{12} = \underline{13.6\ \#}$$

$$F_4 = 19.2(3)\left(\frac{.02174}{12}\right)52 = \underline{5.4\ \#}$$

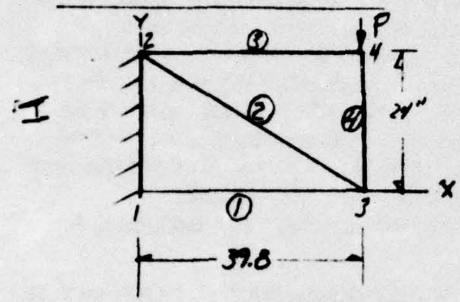
$$F_5 = 19.2\left(\frac{3}{2}\right)\left(\frac{.02174}{12}\right)88 = \underline{3.58\ \#}$$

FORM 118 – (8-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 13 OF
PREPARED	S. Roe	7/25/73	TITLE COMPUTER MODEL FOR STRUPAK ANALYSIS	SKETCH NO. PHASE B
CHECKED				
APPROVED				

COMPUTER MODELS STRUPAK PROGRAM 2DTSAP

I



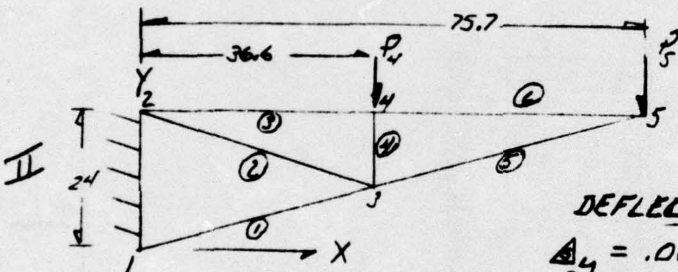
$P_4 = 16.5 + 13.6 = \underline{30.1 \text{ lb}}$

DEFLECTION RESULTS

$\Delta_y = .000979$ IN

$\epsilon_{H_B} = \frac{.000979}{39.8} \times 1000 = \underline{\underline{.025 \text{ mr}}}$

II



$P_4 = 33 + 5.4 = \underline{38.4 \text{ lb}}$

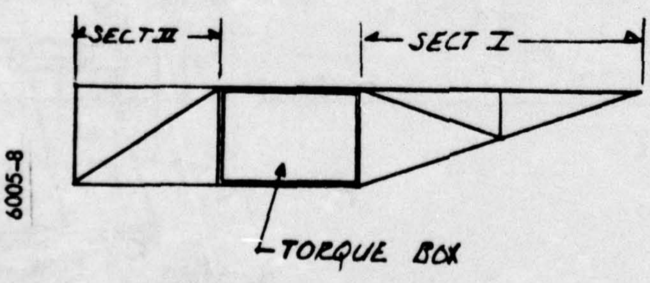
$P_5 = 16.5 + 3.6 = \underline{20.1 \text{ lb}}$

DEFLECTION RESULTS

$\Delta_y = .004122$ IN

$\epsilon_{H_S} = \frac{.004122(1000)}{75.7} = \underline{\underline{.054 \text{ mr}}}$

ASSUME CENTER SECTION TORQUE BOX TO BE RIGID & DEFLECTIONS ARE DUE TO BENDING OF TRUSS STRUCTURE ONLY



6005-8

FORM 118 - (5-67)

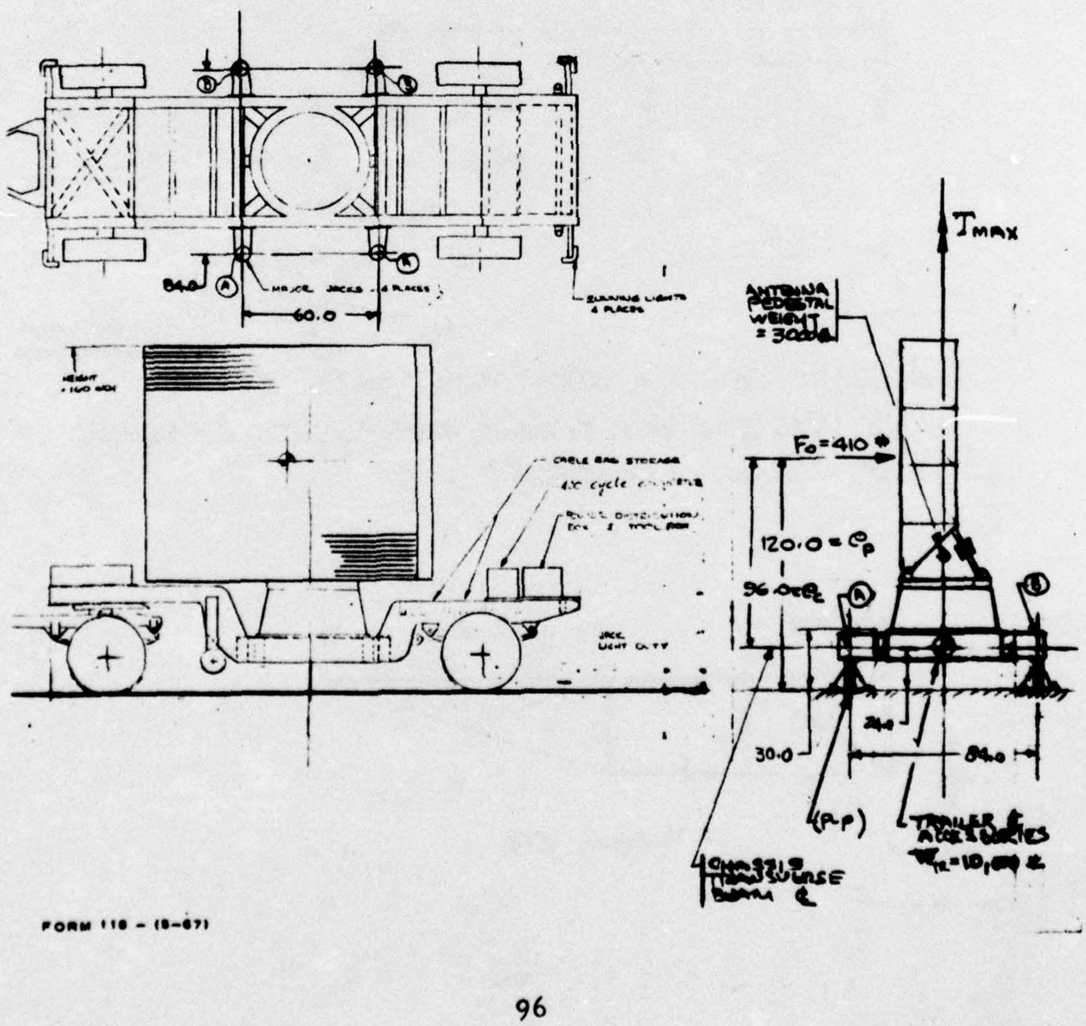
PREPARED	NAME APD	DATE 2/1/73	ITT Gilfillan Inc.	SHEET 15 OF
CHECKED			TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
APPROVED			STRUCTURES ANALYSIS	

ANTENNA-VEHICLE STRUCTURES ANALYSIS

INTRODUCTION: THE ANTENNA-PEDESTAL ASSEMBLY WEIGHING APPROX. 3000 LBS WILL BE MOUNTED RIGIDLY TO THE CENTER TRAILER CHASSIS AS SHOWN BELOW. FOUR (4) MAIN JACKS WILL RAISE THE SPRUNG MASS OF THE ANTENNA VEHICLE ASSEMBLY. A FIFTH JACK FOR ADDED STABILITY IS LOCATED AT AT THE TAIL END OF TRAILER.

THE DESIGN CRITERIA IS A ROTATIONAL OR A BENDING ANGULAR DEVIATION OF

$$\varepsilon_{(j+t_c)} = 0.25 \text{ MILLIRADIAN}$$ (REF. SHT 1)



FORM 118 - (8-67)

PREPARED	NAME APD	DATE 2/1/73	ITT Gilfillan Inc.	SHEET 16 OF
CHECKED			TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
APPROVED			STRUCTURES ANALYSIS	

ANTENNA-VEHICLE STRUCTURES ANALYSIS (CONT'D)

ANALYSIS PARAMETERS

$q_0 = 2.52$ PSF @ 30 MPH (OPERATING)

$q_S = 18.85$ PSF @ 75 MPH (SURVIVAL)

$C_D = 1.30$

$A_{ANT} = 125\ FT^2$

$F_0 = C_D q_0 A = 1.30 \times 2.52 \times 125$

$\boxed{F_0 = 410\ LBS}$

$F_S = C_D q_S A = 1.30 \times 18.85 \times 125$

$\boxed{F_S = 3070\ LBS}$

$T_T = T_{MAX} = 1045.$ FT-#

$\varepsilon_{j+tri} = 0.25$ MILLIRADIAN

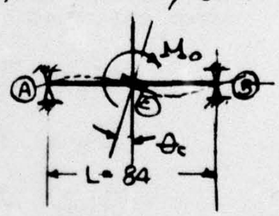
CHASSIS-TRANSVERSE BEAM STIFFNESS DETERMINATION

INCLUDING JACK EXTENTION BEAM

$M_0/_{BEAM} = F_0 \times e_C/2 = 410 \times \frac{96}{2} = 19,680$ IN-# /BEAM

$\theta_c \doteq \varepsilon_{(j+tri)} = 0.25 \times 10^{-3} = \frac{ML}{12EI}$

$I = \frac{19,680 \times 84}{12 \times .25 \times 10^{-3} \times 30 \times 10^6} = 18.40\ IN^4$



USE AISC 6.0x3.0 RECT. TUBING $t = 3/8$

$E = 30 \times 10^6$ psi STEEL

CHECK FOR STRESS AT SURVIVAL

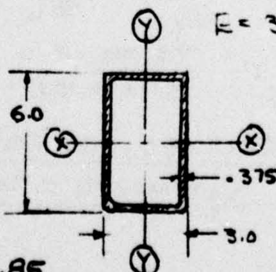
$M_{LL} = M/_{BEAM} = F_S e_{c/2} = 3070\left(\frac{96}{2}\right)$

$= 147,400$ IN-#

$\sigma_b = \frac{Mc}{I_{xx}} = \frac{147,400 \times 3.0}{22.7}$

$\sigma_b = 19,480$ psi

$MS)_y = \frac{36,000}{19,480} - 1.0 = +0.85$ (OK)



$I_{xx} = 22.7\ IN^4$

$I_{YY} = 7.51\ IN^4$

$F_{TY} = 36$ KSI

REF: AISC MANUAL 7TH EDITION P. 3.47

FORM 118 - (8-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 14 OF
PREPARED	APD	2/1/73	TITLE PROJECTILE TRACKING RADAR STRUCTURES ANALYSIS	SKETCH NO.
CHECKED				
APPROVED				

FRONT TRUNNION PIVOT ANALYSIS

THE TRUNNIONS ARE DESIGNED FOR LOADS UNDER RAILROAD IMPACT LOAD. THE LOAD PER TRUNNION (REF. SHEET 10) WAS PREVIOUSLY CALCULATED TO BE

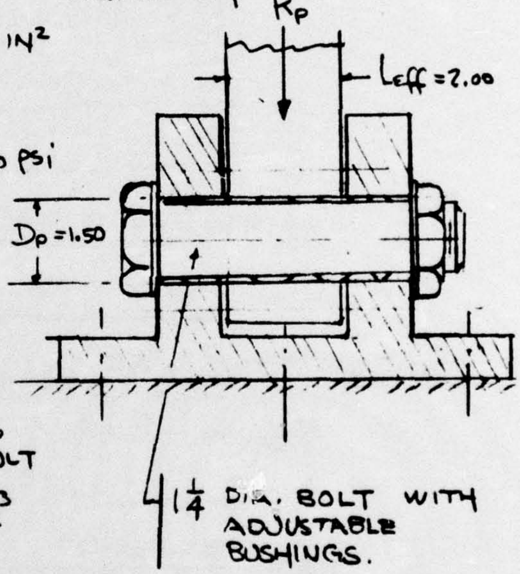
$$R_P = 73{,}000 \text{ LBS}$$

PRE-LIMINARY DESIGN

LET $D_P = 1.50$ IN BASIC PIN DIAMETER INCLUDING BRG. BUSHINGS

$L_{eff} = 2.00$ IN BRG. LENGTH

$A_{BRG} = 3.00 \text{ IN}^2$



BEARING STRESS

$$\sigma_{BRG} = \frac{R_P}{A_{BRG}} = \frac{73{,}000}{3.00} = 24{,}300 \text{ psi}$$

FOR 6061-T6 CLEVIS BLOCK

$$F_{BRY} = 50{,}000 \text{ PSI}$$

$$MS = \frac{50{,}000}{24{,}300} - 1.0 = \underline{+1.14}$$

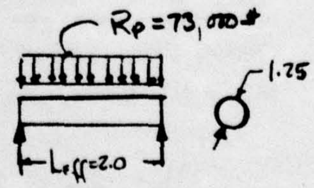
BENDING STRESS ON BOLT

ASSUMED UNIFORMLY DISTRIBUTED LOAD ON 2.00 IN SPAN $1\frac{1}{4}$ IN BOLT

$$S_b = \frac{\pi D_b^3}{32.0} = \frac{3.14\,(1.25)^3}{32.0}$$

$$S_b = 0.192 \text{ IN}^3$$

$$\sigma_b = \frac{M}{S_b} = \frac{R_P L/8}{S_b}$$



$$\underline{\sigma_b} = \frac{73{,}000 \times 2.0}{8.0 \times 0.192} = 95{,}000 \text{ psi}$$

USE 160-180,000 psi BOLT ULTIMATE STRENGTH

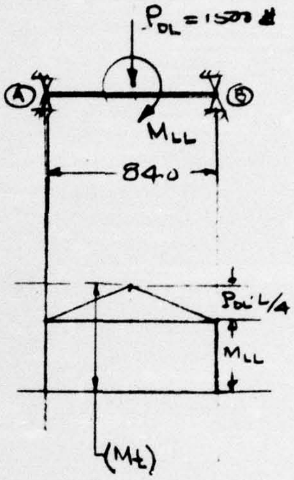
FORM 118 - (5-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 17 OF
PREPARED	APD	2/1/73	TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
CHECKED			STRUCTURES ANALYSIS	
APPROVED				

ANTENNA-VEHICLE STRUCTURES ANALYSIS

CHASSIS TRANSVERSE BEAM (CONT'D)

INCLUDE DL = 3000#/2 = 1500#
ASSUMED CONC. AT CENTER



$M_{DL} = 1500 \times 84/4 = 31{,}500$ IN-#

$M_{LL} = F_S\, e_C/2 = 147{,}000$ IN-#

$M_T = 178{,}500$ IN-#

$$\sigma_{b_{max}} = \frac{M_T \cdot c}{I_{xx}} = \frac{178{,}500 \times 3.0}{22.7}$$

$\sigma_b)_{max} = 23{,}600$ PSI < F_{TY} OK

DYNAMIC LOADING ON FRAME

$n = 10$ g's

$\therefore\ M_{DL} = 1500 \times 84/4 \times 10 = 315{,}000$ IN-#

$$\sigma_b)_{max} = \frac{315{,}000 \times 2.5}{15.5} = 50{,}800 \text{ psi} \gg F_{TY}$$

HIGH (NG)

FOR $F.S = 1.50,\ \sigma_b)_{all} = \dfrac{36{,}000}{1.5} = 24{,}000$

$I_{REQ} = \dfrac{315{,}000 \times 3.0}{24{,}000} = 39.4\ \text{IN}^4$ FOR 6.0" SQ TUBING

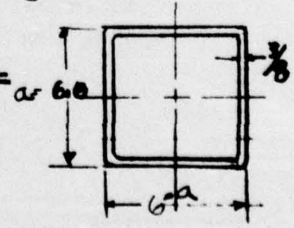
USE AISC $\boxed{6 \times 6 \times \tfrac{3}{8} \text{ SQ. STRUCTURAL TUBING}}$

$I_{xx} = I_{yy} = 40.5\ \text{IN}^4$

$$\therefore\ \theta_c = (\varepsilon_{t_L}) = \frac{M_0 L}{12EI} = \frac{19{,}680 \times 84}{12 \times 40.5 \times 30 \times 10^6} = .000113 \text{ RAD}$$

$(\varepsilon_{t_L}) = 0.113$ MILLIRADIAN

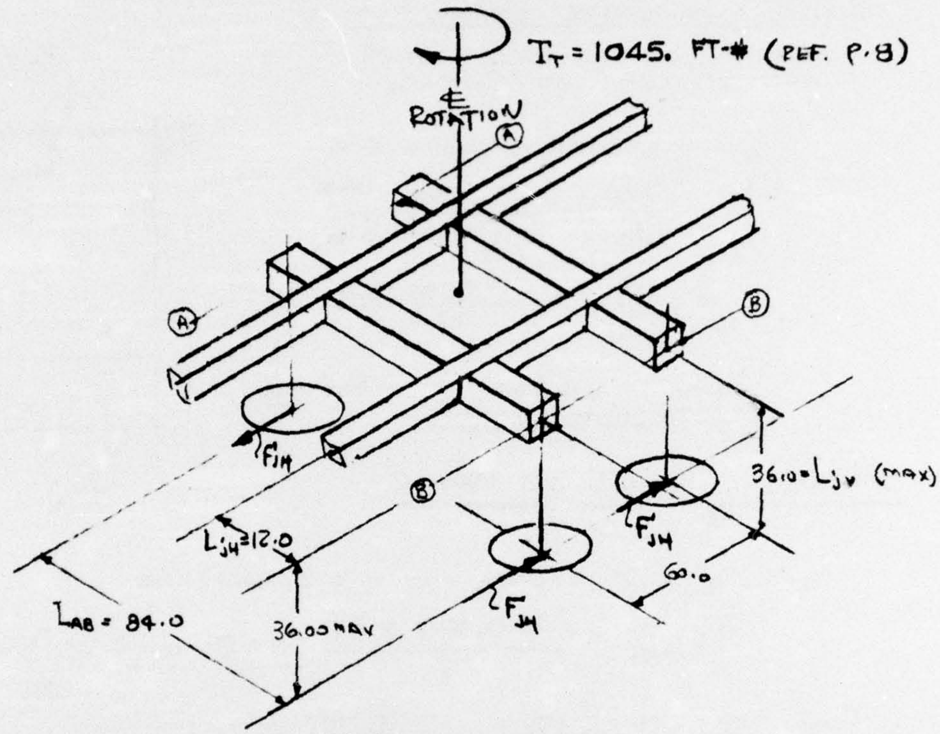
(ELEVATION DIRECTION)



FORM 118 – (5-67)

NAME		DATE	ITT Gilfillan Inc.	SHEET 18 OF
PREPARED	APD	2/1/73	TITLE PROJECTILE TRACKING RADAR STRUCTURES ANALYSIS	SKETCH NO.
CHECKED				
APPROVED				

JACK STRUCTURE TORSIONAL & BENDING ROTATION



JACK SHEAR REACTION (F_{JH}) (OPERATING CONDITION)

$$\underline{F_{JH}} = \frac{T_T}{2L_{AB}} = \frac{1045 \times 12}{2 \times 84} = \underline{75.0 \text{ LBS}}$$

CHASSIS TRANSVERSE BEAM (A-B) WAS PREVIOUSLY SIZED TO BE $6 \times 6 \times 3/8$ AISC TUBING.

SOLVE FOR TORSIONAL STIFFNESS OF LENGTH (L_{JH})

$a = 6.00$ IN
$t = 3/8$ IN

$$K_j = a^3 t = 6^3 \times 3/8$$

$$\underline{\underline{K_j = 81.00 \text{ IN}^4}}$$

POLAR MOMENT OF INERTIA $\approx I_{XX} + I_{YY}$

FORM 118 - (8-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 19 OF
PREPARED	APD	2/1/73	TITLE PROJECTILE TRACKING RADAR	SKETCH NO.
CHECKED				
APPROVED			STRUCTURES ANALYSIS	

JACK STRUCTURES TORSIONAL & BENDING ROTATION (CONT'D)

CONSIDER ONE JACK SUPPORT

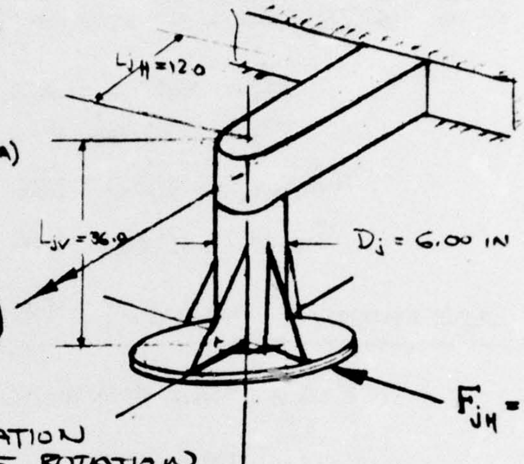
$T_j = F_{jH} \times L_{jV} = 75 \times 36.0$

$T_j = 2700.00$ IN-#

LET $D_j = 6.00$ IN (DIA)

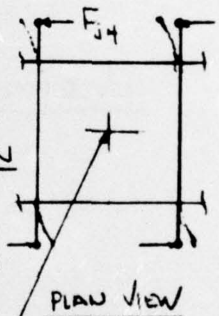
$t = 3/8$ IN

$I_j = \frac{\pi D^3 t}{8} = 31.8$ IN^4



THE TOTAL ANGULAR DEVIATION ABOUT THE CENTER OF ROTATION IS GIVEN BY

$$\boxed{\Phi = \mathcal{E}_{J+TR} = \frac{\Delta L_{jH} + \overbrace{\Delta L_{jV} + \Phi_{jH} \times L_{jV}}^{\Delta_j}}{L_{AB}/2}}$$



$$\Delta_{L_{jH}} = \frac{F_{jH} L_{jH}^3}{3EI} = \frac{75.0(12)^3}{3\times30\times10^6\times40.5} = \underline{.00003 \text{ IN}}$$

$(I = 40.5\ \text{IN}^4)$

$$\Delta_{LjV} = \frac{F_{jH} L_{jV}^3}{3EI_j} = \frac{75.0(36)^3}{3\times30\times10^6\times31.8} = .00122 \text{ IN}$$

$(I = 31.8\ \text{IN}^4)$

$$\Delta_j = \frac{T_j L_{jH}}{K_j G} \times L_{jV} = \frac{2700\times12.0\times36.0}{81.0\times11.5\times10^6} = .00124 \text{ IN}$$

$G = 11.5\times10^6$ psi

$$\Delta_j\Big]_{TOTAL} = \underline{.00249 \text{ IN}}$$

(AZIMUTH DIRECTION)

$$(\mathcal{E}_{j+tr}) = \Phi = \frac{.00249}{84/2} \times 1000 = \underline{0.059} \text{ MILLIRADIAN} \ll \mathcal{E}_{AL} = 0.25 \text{ MR}$$

FROM THE ABOVE RESULTS A DIAMETRAL CLEARANCE (SLOP) ON THE JACK CAN BE TOLERATED TO A MAXIMUM OF

$$\underline{\Delta D} = (0.00025 - .000059)\,42 = \underline{0.0080 \text{ IN}}$$

$\therefore\ \mathcal{E}_{jcL} = 0.200$ M.R.

FORM 118 - (5-67)

	NAME	DATE	ITT Gilfillan Inc.	SHEET 20 OF
PREPARED	APD	2/1/73	TITLE PROJECTILE TRACKING RADAR STRUCTURES ANALYSIS	SKETCH NO.
CHECKED				
APPROVED				

ANTENNA-VEHICLE SYSTEM STABILITY - SURVIVAL COND.

REFERRING TO SKETCH ON P.14 AND LOAD F_S ON P. 15 AND TAKING MOMENT ABOUT (P-P)

$$F_S = 3070.0 \text{ LBS}$$
$$e_P = 120.00 \text{ IN}$$
$$W_{ANT-PED} = 3000 \text{ LBS}$$
$$W_{TR+AC} \approx 10{,}000 \text{ LBS}$$

RESTRAINING MOMENT (RM)

$$RM = (W_{A-P} + W_{TR+AC})\, L_{AB}/2$$
$$= 13{,}000 \times 42$$
$$RM = 546{,}000 \text{ IN-\#} = 45{,}500 \text{ FT-\#}$$

OVERTURNING MOMENT -(OM)

$$OM = F_S \times e_P$$
$$= 3070 \times 120$$
$$OM = 368{,}400 \text{ IN-\#} = 30{,}700 \text{ FT-\#}$$

$$\frac{RM}{OM} = \frac{546{,}000}{368{,}400} = 1.48$$

FOR A 13,000 LB ANTENNA-VEHICLE WEIGHT THE SYSTEM THEREFORE IS STABLE AND NEEDS NO EXTERNAL STOWAGE PROVISION.

FORM 118 - (5-67)

PREPARED	NAME: APD	DATE: 2/1/73	ITT Gilfillan Inc.	SHEET 21 OF
CHECKED			TITLE: PROJECTILE TRACKING RADAR STRUCTURES ANALYSIS	SKETCH NO.
APPROVED				

JACK PAD BEARING LOAD ANALYSIS

* USE SURVIVAL LOAD (F_S) ON ANTENNA

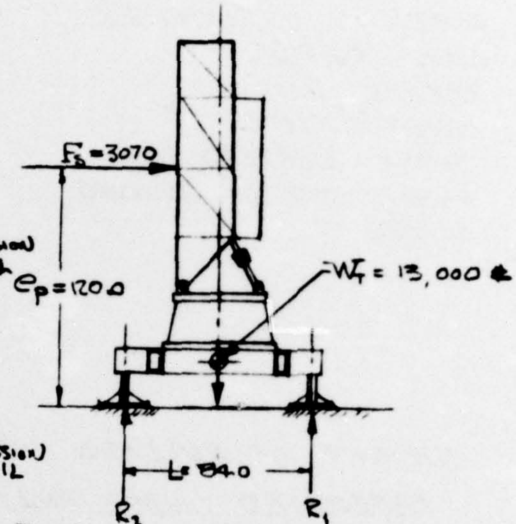
$\Sigma M_{R_1} = 0$

$$R_2 = \frac{F_S\, e_P}{2L} - \frac{W_T}{4}$$

$$= \frac{3070 \times 120}{2 \times 84} - \frac{13{,}000}{4}$$

$$= 2190 - 3250$$

$$\boxed{R_2 = -1060 \text{ LBS}}$$ COMPRESSION ON SOIL



$\Sigma M_{R_2} = 0$

$$R_1 = -2190 - 3250$$

$$\boxed{R_1 = -5440 \text{ LBS}}$$ COMPRESSION ON SOIL

DESIGN JACK PAD FOOT PRINT BASE ON MAX. OPERATING BEARING LOAD OF * $P_{BRG} = 5000$ LBS

* DESIGN JACK FOR 5 TON OR 10,000 LBS CAPACITY.

ASSUMPTION

(1) USE MODULUS OF SUBGRADE REACTION $K_u = 100$ PSI/IN

(2) LET MAXIMUM BRG. LOAD$)_{ALL}$ = 1500 PSF — WHICH WILL ALLOW THE SYSTEM TO OPERATE ON SOIL SUCH AS SOFT CLAY, CLAY LOAM, POORLY COMPACTED SAND, CLAY CONTAINING LARGE AMOUNT OF SILT & WATER STANDS DURING WET SEASON.

$$A_{PAD} = \frac{P_{BRG}}{F_{BRG})_{AL}} = \frac{5000}{1500} = 3.33 \text{ FT}^2 \qquad (A_{PAD} = 3.14 \text{ FT}^2)$$

$$D_{PAD} = \sqrt{\frac{4 \times 3.3}{\pi}} = 2.06 \text{ FT} \quad \text{OR} \quad (D_{PAD} \simeq 24.00 \text{ IN})$$

THE DIFFERENTIAL BEARING LIVE LOAD $\Delta P_{LL} = 2190$ LBS

$$\therefore \quad \Delta_{DIFF} = \frac{\Delta P_{LL} / A_{PAD}}{K_u} = \frac{2190/(3.14 \times 144)}{100} = 0.048 \text{ IN}$$

$$\varepsilon_{PAD} = \frac{\Delta_{DIFF}}{L} \times 1000 = \frac{.0480}{84.0} \times 1000$$

$$\boxed{\varepsilon_{PAD} = 0.570 \text{ MILLI RADIAN}}$$

FORM 118 - (5-67)

PREPARED	B. ROE	10/5/76	ITT Gilfillan	SHEET 1 OF 1
CHECKED			TITLE PHASE B ANTENNA WEIGHTS	SKETCH NO.
APPROVED				

ANTENNA STRUCTURE	722.0
LINE FEED	45.5
ARRAYS (167)	235.5
MONITOR LINE	22.4
PHASE SHIFTERS (167)	167.0
PHASE SHIFTER HOUSING	45.3
COMBS	26.0
	1263.7 lb

WEIGHT OF ANTENNA SYSTEM DESIGNED & FABRICATED UNDER PHASE B. THESE WEIGHTS WILL BE UTILIZED IN PHASE C FOR ANALYSIS & DESIGN OF SERVO DRIVE SYSTEM.

FORM 118 - (8-73)

REPORT DISTRIBUTION

Required Distribution	Number of Copies Reports Final Tech Report DI-S-180
Commander Picatinny Arsenal ATTN:	
Technical Support Directorate	
SARPA-TS-T-S	5
SARPA-TS-1	1
Product Assurance Directorate	10
SARPA-QA-A-R	
Dover, New Jersey 07801	
Project Manager Munitions Prod Base Mod & Exp Picatinny Arsenal ATTN:	
DRCPM-PBM	1
Dover, New Jersey 07801	
Defense Documentation Center Cameron Station Alexandria, Virginia 22314	12
Commander U. S. Army Material Development & Readiness Command ATTN:	
DRCRD-WC	1
DRCRD-OS	1
DRCQA-E	1
Washington, D. C. 20315	
Commander U. S. Army Armament Command ATTN:	
DRSAR-QAE	3
DRSAR-RD	1
DRSAR-AS	1
Rock Island, Illinois 61201	

Commander
U. S. Army Electronics Command
ATTN:
DRSEL-CT-R 3
Fort Monmouth, N.J. 07703

Commander
U. S. Army Test & Eval. Command
ATTN:
DRSTE-RU 1
Aberdeen, Maryland 21005

Commander
U. S. Army Missile Command
ATTN:
Technical Library 1
Redstone Arsenal, Alabama 35809

Commander
Ballistic Research Laboratories
ATTN:
Technical Library 1
Aberdeen Proving Ground
Maryland 21005

Commander
Harry Diamond Laboratories
ATTN:
DRXDO-TA 1
Washington, D. C. 20438

Commander
Frankford Arsenal
ATTN:
N3200 1
Philadelphia, PA. 19137

Commander
Aberdeen Proving Ground
ATTN:
STEAP-MT-G 1
Aberdeen Proving Ground, Maryland
21005

Commander
Yuma Proving Ground
ATTN:
STEYP-MTS 1
Yuma, Arizona 85634

Commander
White Sands Missile Range
ATTN:
Technical Library 1
New Mexico 88002

Commander
Jefferson Proving Ground
ATTN:
STEJP-MTM 1
Madison, Indiana 47521

Commander
Naval Ordnance Systems Command
ATTN:
Code ORD-0462D 1
Washington, D. C. 20362

Director
Naval Research Laboratories
ATTN:
Technical Library 1
Washington, D. C. 20390

Commander
U. S. Naval Weapons Laboratory
ATTN:
Technical Library 1
Dahlgren, Virginia 22488

Commander
U. S. Naval Ordnance Test Station
ATTN:
Technical Library 1
China Lake, California 93555

Commander Marine Corps
Hq., U. S. Marine Corps
ATTN:
Code A04C 1
Washington, D. C. 20380

Commander
Wright Air Development Division
Wright-Patterson Air Force Base
ATTN:
Technical Library 1
Ohio 45433

Commander
Rome Air Development Command
Griffiss Air Force Base
ATTN:
Technical Library 1
New York 13440

Commander
Air Force Rocket Propulsion Lab (AFSC)
ATTN:
Mr. L. Meyers (RPMMA) 1
Edwards Air Force Base
California 93523

Commander
ADTC (ADLEG)
ATTN:
Mr. J. Howanick 1
Eglin Air Force Base
Florida 32542

Commander
Service Engineering Division (MME)
ATTN:
Mr. D. Hebdon (MMECL) 1
Hill Air Force Base, Utah 84401

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE

READ INSTRUCTIONS BEFORE COMPLETING FORM

1. REPORT NUMBER and 14 ITTG-5059B

2. GOVT ACCESSION NO.

3. RECIPIENT'S CATALOG NUMBER

4. TITLE (and Subtitle) 6

MM&TE-Application Of Radar To Ballistic Acceptance Testing of Ammunition (ARBAT). Phase B: Antenna Development/Fabrication.

5. TYPE OF REPORT & PERIOD COVERED 9

Final Report

6. PERFORMING ORG. REPORT NUMBER

5059B

7. AUTHOR(s) 10

C. Barfield

8. CONTRACT OR GRANT NUMBER(s) 15

DAAA21-73-C-0664 NEW

9. PERFORMING ORGANIZATION NAME AND ADDRESS

International Telephone & Telegraph Corporation
Gilfillan Division
7821 Orion Street, Van Nuys, CA. 91409

10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS

MM&TE Project 5704139

11. CONTROLLING OFFICE NAME AND ADDRESS

Picatinny Arsenal, Dover, N.J. 07801

12. REPORT DATE 11

30 Sep[redacted]76

13. NUMBER OF PAGES 12

113p.

14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)

15. SECURITY CLASS. (of this report)

Unclassified

15a. DECLASSIFICATION/DOWNGRADING SCHEDULE

N/A

16. DISTRIBUTION STATEMENT (of this Report)

Unlimited

17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)

18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Ammunition Testing
Ballistic Trajectory
Electronic Elevation Scanning
Dual Slot Radiators
Projectile Tracking Radar
Antenna Performance Monitor
Phase/Frequency/Mechanical Scanning
Low Sidelobe Amplitude
Planar Array Antenna

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Antenna design analyses performed in an earlier program phase (ARBAT System Design Study) were validated and used in the final development and fabrication of an "X" band phase/frequency mechanical scanning radar antenna to be incorporated in a radar system for ballistic ammunition acceptance testing. The antenna is a 10 by 12 ft aperture planar array. Elevation scanning is accomplished by phase changes produced by digitally controlled 4 bit diode phase shifters. Scanning in azimuth is by frequency variation and mechanical — over

DD FORM 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED 388 599

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

bpg

Block No. 20 (Continued)

rotation of the array. Development steps included fabrication and testing of individual critical items and assemblies of critical items to estimate full array performance. A 9 element partial array was range tested prior to fabrication of the required 167 horizontal array elements and associated microwave elements. The mechanical and electrical design is discussed and test results are summarized.